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TABLICE
DO RACHUNKÓW TRYGONOMETRYCZNYCH NA ELIPSOIDZIE BESSEL'A

przez

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TABLES
FOR TRIGONOMETRICAL COMPUTATIONS ON BESSEL'S SPHEROID

by

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Wstęp.

Poniższe tablice funkcyjne, mające służyć do rozwiązywania podstawowych zadań trygonometrji na elisoidzie obrotowej (t. zw. zadanie główne w formie zwykłej i odwróconej) przy pomocy współrzędnych geograficznych, opracowane zostały w oparciu o następujące założenia: 1) dokładność rachunku ma wynosić:

± 0"0001 dla współrzędnych geograficznych (φ, λ)

± 0.001m: dla iloczynów długości linji geodezyjnej przez cos i sin. azymutu.

2) długości linji geodezyjnych nie przekraczają 100 klm.

3) zakres stosowalności tablic rozciąga się od φ=48° do φ=56°. *)

Schemat pracy przy obliczeniu wartości funkcji podanych w tablicach był pokrótce następujący:

a) Wartości funkcji, odpowiadające wartościom argumentu równym całkowitej liczbie stopni kątowych, obliczano wzorami ścisłymi **) z wyższą od założonej dokładnością.

b) zagęszczanie otrzymanych tak tablic funkcyjnych odbywało się w drodze interpolacji bezpośredniej - t. zn. przez operowanie bezpośrednio wartościami funkcji a nie ich różnic - przy takim oczywiście obraniu rzędu interpolacji, aby spełnić założenia (1).

Jakkolwiek takie postępowanie powodowało konieczność stosowania w niektórych wypadkach nawet interpolacji 7 rzędu było jednak ekonomiczniejsze od obliczenia funkcji wzorami ścisłymi. Wynikało to ze skomplikowanej formy algebraicznej obliczanych funkcji, oraz - zwłaszcza przy obliczaniu współczynników „zadania odwrotnego" - z małej zbieżności odnośnych szeregów.

Wartości współczynników zadania wprost (t. zw. szeregi Legendre'a) brano pod postacią formalną przyjętą w Handbuch der Vermessungskunde Jordana, t. zn. z wprowadzeniem pojęcia funkcji podstawowej (Grundfunktion) $V = 1 + e'^2 \cos^2 \varphi$.

Wartości współczynników zadania odwrotnego wyrażono w funkcji współczynników zadania wprost („zagadnienie odwrócenia szeregu"), opierając się przytym częściowo również na Jordanie.

Całkowite wykorzystanie szeregów podanych przez Jordana było z uwagi na błędy algebraiczne - prawdopodobnie charakteru drukarskiego - niemożliwe.

Surowe założenia dotyczące dokładności (1.2) spowodowały konieczność nowego obliczania niektórych potęg funkcji podstawowej V, gdyż oparcie się o odnośne wartości podane u Jordana w formie logarytmicznej nie dałoby gwarancji spełnienia omawianych założeń.

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*) Przyjęcie zakresu stosowalności tablic w granicach szerokościowych obecnych od φ=49° do φ=54° prowadziłoby do przekreślenia dorobku geodezyjnego lat 1918 - 1939 i zmusiło do traktowania fragmentarycznego jednolitych koncepcji matematycznych, jakiemi są sieci triangulacyjne.

**) Dla podkreślenia konwencjonalnego charakteru rozróżnienia wzoru „ścisłego" od interpolacyjnego użyliśmy cudzysłowu. Różnica między obliczeniem wartości funkcji z szeregu potęgowego a z interpolacji nie polega w istocie na różnicy ścisłości, lecz na oparciu się o inne dane - w pierwszym wypadku: jedna wartość funkcji i n-1 pochodnych, w drugim: n wartości funkcji.

Na zakończenie niniejszego wstępu pozwalam sobie złożyć serdeczne podziękowanie p. Rektorowi Politechniki Warszawskiej prof. Edwardowi Warchałowskiemu za wskazówki w pracy, jak i słowa zachęty. Również p. inż. Jerzemu Szymońskiemu za współpracę przy interpolacyjnym zagęszczaniu tablic składam na tym miejscu serdeczne podziękowanie

Stefan Hausbrandt

Wskazówki dotyczące techniki wykonania obliczeń.

Przy prowadzeniu obliczeń należy pamiętać, że zasadą rachunku arytmometrycznego jest: jak najmniej zapisywać. W myśl tego nie należy więc zapisywać wartości poszczególnych iloczynów w szeregach potęgowych 2.5, a przygotować do rachunku czynniki, poczym mnożyć kolejno, jednocześnie sumując, tj nie kasować licznika rezultatów, aż do ukończenia obliczenia danej funkcji.

Przygotowując do rachunku czynniki wygodnie jest postąpić jak następuje:

Rozpocząć od wpisywania pierwszych potęg

$x=$ $y=$ względnie $\Delta\varphi=$ $\Delta\lambda=$

Następnie ustawić w liczniku nastawień pierwszą potęgę jednej ze zmiennych i pomnożyć ją przez wartość zapisaną poczym zapisać rezultat, pomnożyć przez wartość ostatnio zapisaną, zapisać rezultat, pomnożyć przez wartość ostatnio zapisaną, zapisać rezultat i t d.

Otrzymamy w ten sposób - nic nie kasując w liczniku nastawień - kolejne potęgi zmiennej.

x
x^2
x^3
x^4

Odczytywać stałe tesame ilości znaków dziesiętnych za przecinkiem, a więc np:

$x=-0.62152592$ lub $\Delta\varphi=-0.20324579$
$x^2=+0.38629447$ $\Delta\varphi^2=+0.04130885$
$x^3=-0.24009203$ $\Delta\varphi^3=-0.00839585$
$x^4=+0.14922342$ $\Delta\varphi^4=+0.00170642$

Dalszy przebieg obliczeń zależny jest od tego czy „czynniki tablicowe" - jak będziemy dalej nazywali wielkości ⓧ ⓨ ⓧⓨ..... względnie ⓐφ ⓐλ ⓐφⓐλ ..... - dla danego argumentu φ występować będą w zadaniu jednokrotnie, czy wielokrotnie, tj biorąc rzecz praktycznie - czy prace rachunkowe dotyczą pojedynczej linji geodezyjnej z punktem początkowym φ czy też peku linji geodezyjnych wychodzących z wierzchołka φ.

W wypadku pojedynczej linji najpraktyczniej postąpić j.n.

1) Pasek kartonu o jednym wymiarze równym szerokości tablicy, zaś drugim równym ca 1cm. położyć na tablicy, z której brać mamy czynniki tablicowe, poczym przeliniować pasek linjami pionowymi tak, aby podzielić go na kolumny o szerokościach, odpowiadających szerokościom kolumn tablicy.

2) W utworzonych tak polach paska wpisywać kolejno odpowiednie potęgi i iloczyny potęg patrząc na tytułowy wiersz tablicy i utożsamiając uprzednio tabliczkę potęg.

3) Po wypełnieniu całego paska nasunąć go na tę linję tablicy, która zawiera czynniki tablicowe dla najbliższej szerokości geograficznej z niedomiarem, poczym wykonać mnożenia i sumowania, ustawiając w liczniku nastawień liczbę napisaną na pasku i mnożąc ją przez liczbę wydrukowaną poniżej w tablicy. Po wykonaniu rachunku (uważać na znaki!) zapisać rezultat oznaczając że jest to wartość poszukiwanej funkcji dla argumentu φ (φ z niedomiarem)

4) Po skasowaniu rezultatu przesunąć pasek wiersz niżej i obliczyć analogicznie wartość poszu-

kiwanej funkcji dla argumentu φ_x (φ_x z nadmiarem).

2) Z otrzymanych wartości funkcji dla argumentu φ_- i φ_+ - oznaczmy je przez f_- i f_+ - wyinterpolować poszukiwaną wartość funkcji dla argumentu φ - oznaczmy ją f.

Najwygodniej przytem posługiwać się interpolacją bezpośrednią, to znaczy pomnożyć wartość funkcji od argumentu z niedomiarem przez spełnienie ułamka interpolacyjnego do jedności,[3] oraz wartość funkcji od argumentu z nadmiarem przez ułamek interpolacyjny i zesumować rezultaty. Działanie to, które wyraża wzór:

$$f = (1-k)f_- + kf_+$$

wykonywujemy oczywiście bezpośrednio na arytmometrze.

W wypadku pęku linji geodezyjnych wygodniej jest wyinterpolować dla szerokości geograficznej wierzchołka pęku wartości czynników tablicowych, poczym przeprowadzić jednokrotny już rachunek wzdłuż każdego z promieni pęku.

Dla wyinterpolowania wartości czynników tablicowych najlepiej przytem posługiwać się też interpolacja bezpośrednią, która sprowadzi się do wpisania na skrawku kartonu spełnienia ułamka interpolacyjnego do jedności, oraz poniżej samego ułamka interpolacyjnego i przesuwaniu tego skrawka $\boxed{\frac{1-k}{k}}$ w kierunku wierszy dla kolejnego wykonywania mnożeń $\frac{(1-k)f_-}{k\,f_+}$

Uwaga

W stosunku do wszystkich wyrazów szeregów potęgowych (2) i (5) z wyjątkiem wyrazów Ⓨ i ⓐⓚ interpolacja linjowa daje rezultaty identyczne (w granicach założonej dokładności 0."0001 i 0.001m) z interpolacja rzędów wyższych. Interpolując wartość wyrazu Ⓨ względnie ⓐⓚ przy pomocy interpolacji linjowej narazić się możemy na obniżenie dokładności rezultatu, dochodzące w krańcowym wypadku (przy 100klm. linji geodezyjnej) do 0."0003 względnie 0.001m

Jeżeli jest to niepożądane należy wprowadzić mało kłopotliwą „poprawkę interpolacyjną" sprowadzającą się do zmniejszenia wyrazu Ⓨ o wielkość p. względnie do zwiększenia wyrazu ⓐⓚ o wielkość q. Wielkość p. i q. znajdujemy z odnośnych tabliczek - z prawej strony tablicy głównej - według argumentu k (ułamka interpolacyjnego)

Można też wprowadzić poprawkę do rezultatu obliczenia t.zn. poprawić obliczony przyrost długości Δk (zadanie 1) o wielkość p.y, względnie poprawić obliczoną składową y (zadanie 2) o wielkość $q.\Delta k$.

Poprawki te są zresztą tak mało realnymi wielkościami, że i ich zupełne pomijanie miałoby logiczne uzasadnienie - tymbardziej, że linje geodezyjne długości rzędu 100klm. spotykają się wyjątkowo.

W przykładach liczbowych operujemy liniami geodezyjnymi nieco przekraczającymi 100klm. i wprowadzamy wyżej omówione poprawki interpolacyjne.

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[3] Wielkość k nazywana tu i dalej „ułamkiem interpolacyjnym" jest stosunkiem różnicy między wartością argumentu daną i tablicową z niedomiarem do różnicy między wartością argumentu tablicową z nadmiarem i z niedomiarem $k = \frac{\varphi - \varphi_-}{\varphi_+ - \varphi_-}$. Interpolując np. z naszych tablic dla $\varphi = 48°15'20"$ mieć będziemy $k = \frac{20"}{60"} = 0{,}333333\ldots$ itp.

Przykłady liczbowe.

Zadanie 1.

Dane $\begin{cases} \varphi_1 = 50^\circ 45' 10{,}2709 = 50^\circ 45{,}171182 \text{ t.z przy interpolacji } k = 0{,}171182 \quad 1-k = 0{,}828818 \\ S_1 = 103275{,}242\,m = 1{,}03275242 \text{ sk. (setek kilometrów)} \\ A_1 = 127^\circ 0' 0'' \text{ czyli } \cos A_1 = -0{,}601815024 \\ \qquad\qquad \sin A_1 = +0{,}798635508 \end{cases}$

Obliczenie składowych i ich potęg

$x = S\cos A = -0{,}62152592 \qquad y = S\sin A = +0{,}82479275$

$x^2 =$	$+0{,}38629447$	$y^2 =$ $+0{,}68028308$
$x^3 =$	$-0{,}24009203$	$y^3 =$ $+0{,}56109255$
$x^4 =$	$+0{,}14922342$	$y^4 =$ $+0{,}46278507$
$x^5 =$	$-0{,}09274622$	$y^5 =$ $+0{,}38170177$

Obliczenie przyrostu szerokości (podajemy rysunek paska ⟺ na odpowiednim fragmencie tablicy dla uzmysłowienia przebiegu obliczeń. Przepisywanie fragmentu tablicy jest oczywiście przy wykonaniu praktycznym zbędne.)

φ 50°	(x)	(y^2)	(xy^2)	(x^2)	(x^2y^2)	(y^4)	(x^3)	(xy^4)	(x^3y^2)
	$-0{,}62152592$	$0{,}68028308$	$-0{,}42281357$	$0{,}38629447$	$0{,}26278959$	$0{,}46278507$	$-0{,}24009203$	$0{,}28763292$	$-0{,}16333055$
45'	3236.51327	-30.99508	-0.72132	-0.25011	-0.01643	0.00348	0.00053	0.00024	-0.00038
46'	3236.50400	-31.01337	-0.72202	-0.25008	-0.01645	0.00348	0.00053	0.00024	-0.00038

$\Delta\varphi_{50°45'} = 2032{,}''45679 \mid 0{,}828818$
$\Delta\varphi_{50°46'} = 2032{,}''46317 \mid 0{,}171182$

$\Delta\varphi_1 = 2032{,}''45788 = 33'52{,}''4579$

$\varphi_1 = 50°45'10{,}''2709$

$\varphi_2 = 50°11'17{,}''8130 = 50°11{,}296883$

$K = 0{,}296883$

$1-K = 0{,}703117$

Obliczenie przyrostu długości (uwaga j. wyżej)

φ 50°	(y)	(xy)	(x^2y)	(y^3)	(x^3y)	(xy^3)	(x^2y^3)	(x^4y)	(y^5)
	$0{,}82479275$	$-0{,}51263007$	$0{,}31861288$	$0{,}56109255$	$-0{,}19802617$	$-0{,}34873356$	$0{,}21674695$	$0{,}12307839$	$0{,}38170177$
45'	5101.63400	97.71352	2.28911	-0.62385	0.05180	-0.04382	-0.00200	0.00119	0.00017
46'	5103.44632	97.80620	2.29214	-0.62481	0.05189	-0.04391	-0.00201	0.00119	0.00017

$\Delta\lambda_{50°45'} = 4158{,}''08395 \mid 0{,}828818$
$\Delta\lambda_{50°46'} = 4159{,}''53167 \mid 0{,}171182$

$\Delta\lambda = 4158{,}''33177$ (lub jeżeli uwzględnić poprawkę p.y.)

poprawka p.y. $-0{,}00009$

$\Delta\lambda = 4158{,}''3317 = 1°09'18{,}''3317$

$\lambda_1 = 22°20'15{,}''00$

$\lambda_2 = 23°29'33{,}''3317$

Obliczenie azymutu l. geod. 1-2 w punkcie 2.

$(y_1) = \begin{matrix} 5101.63400 \cdot 0.828818 \\ 5103.44632 \cdot 0.171182 \end{matrix} \Big\} = 5101.944237$ poprawka p.y. -0.00011 $= 5101.94413$

$(y_2) = \begin{matrix} 5041.02591 \cdot 0.703117 \\ 5042.78086 \cdot 0.296883 \end{matrix} \Big\} = 5041.546925$ poprawka p.y. -0.000018 $= 5041.54674$

$y_2 = y_1 \dfrac{(y_2)}{(y_1)} = \dfrac{0.82479275 \cdot 5041.54674}{5101.94413} = 0.815028\,76$

$x_2 = -\sqrt{S^2 - y_2^2} = -0.63427571$

$A_2 = \operatorname{arc.tg} \dfrac{0.815028\,76}{-0.63427571} = -1.28497552 \qquad A_2 = 127°53'27{,}''397$

Zadanie 2

Dane $\varphi_1 = 50^\circ 45' 10''.2709$ $k = 0.171182$ $1-k = 0.828818$ | $\lambda_1 = 22^\circ 20' 15''.00$

$\varphi_2 = 50^\circ 11' 17''.8130$ $k = 0.296883$ $1-k = 0.703117$ | $\lambda_2 = 23^\circ 29' 33''.3317$

Obliczenie $\Delta\varphi_{12} = -33'32''.4579 = -2032''.4579 = -0.20324579$ dz. t. s. | $\Delta\lambda = 1^\circ 09' 18''.3317 = 4158''.3317 = +0.41583317$ dz. t. s.

przyrostów i potęg ich: $\Delta\varphi^1 = +0.0413\,0885$ | $\Delta\lambda^1 = +0.1729\,1723$

$\Delta\varphi^3 = -0.0083\,9585$ | $\Delta\lambda^3 = +0.0719\,0472$

$\Delta\varphi^4 = +0.0017\,0642$ | $\Delta\lambda^4 = +0.0299\,0037$

Obliczenie składowej x (podajemy rysunek paska na odpowiednim fragmencie tablicy 2 ⟵ dla uzmysłowienia przebiegu obliczeń. Przepisywanie fragmentu tablicy jest oczywiście przy wykonaniu praktycznym zbędne).

$\varphi = 50^\circ$	$\Delta\varphi$	$\Delta\lambda^2$	$\Delta\varphi^2$	$\Delta\varphi\Delta\lambda^2$	$\Delta\varphi^3$	$\Delta\varphi^2\Delta\lambda^2$	$\Delta\lambda^4$
	-0.2032 4579	0.1729 1723	0.0413 0885	-0.0351 4470	-0.0083 9585	0.0071 4301	0.0299 0037
45'	308 974.478	3679.568	73.774	-169.170	-0.449	-5.636	-0.153
46'	308 975.364	3679.135	73.766	-169.308	-0.450	-5.635	-0.153

$X_{\varphi\,50^\circ 45'} = -62152.5492$ | 0.828818

$X_{\varphi\,50^\circ 46'} = -62152.7997$ | 0.171182

$X = -62152.592$ m.

Obliczenie składowej y (uwago j. w.)

$\varphi = 50^\circ$	$\Delta\lambda$	$\Delta\varphi\Delta\lambda$	$\Delta\lambda^3$	$\Delta\varphi^2\Delta\lambda$	$\Delta\varphi\Delta\lambda^3$	$\Delta\varphi^3\Delta\lambda$
	0.4158 3317	-0.0845 1634	0.0719 0472	0.0171 7759	-0.0146 1433	-0.0034 9127
45'	196015.629	-11600.019	-46.048	-155.932	0.891	-0.005
46'	195946.020	-11602.808	-46.054	-155.878	0.894	-0.005

$y_{\varphi\,50^\circ 45'} = 82484.1889$ | 0.828818

$y_{\varphi\,50^\circ 46'} = 82455.4794$ | 0.171182

$y = 82479.2744$

popr. $\Delta\lambda_2$ 0.0005

$y = 82479.275$ m.

Obliczenie azymutu na punkcie początkowym i długości linji.

$A_1 = \text{arc. tg.} \frac{82479.275}{-62152.592} - 1.32704482$ $A_1 = 127^\circ 00'$

$S = \sqrt{x^2 + y^2} = 103275.242$ m.

Obliczenie azymutu l. geod. 1-2 w punkcie 2.

$\Delta\lambda$: $196015.629 \cdot 0.828818$ / $195946.020 \cdot 0.171182$ $= 196003.7132$ (popr. 8) 196003.714

$\Delta\lambda_2$: $198372.319 \cdot 0.703117$ / $198303.283 \cdot 0.296883$ $= 198351.8234$ (popr. 9, 1,7) 198351.825

$y_2 = \frac{y_1 \cdot \Delta\lambda_1}{\Delta\lambda_2} = \frac{82479.275 \cdot 196003.714}{198351.825} = 81502.876$

$x_2 = \sqrt{S^2 - y_2^2} = -63427.571$

$A_2 = \text{arc. tg.} \frac{81502.876}{-63427.571} = \text{arc. tg.} - 1.28497552$ $A_2 = 127^\circ 53' 27''.397$

Introduction.

These mathematical tables, designed for the solution of the basic trigonometrical problems on the ellipsoid of revolution (the so-called direct and inverse principal problems) from geographical coordinates, have been made to comply with the following conditions:

1) The accuracy of the calculations should be:

$\pm 0''.0001$ for the geographical coordinates (φ and λ),

± 0.001 m for the products of the length of the geodesic by the cosine and the sine of the azimuth.

2) The lengths of the geodesics do not exceed 100 km.

3) The scope of applicability of the tables ranges from $\varphi = 48°$ to $\varphi = 56°$ *)

The course followed in calculating the values of the functions given in the tables has been briefly this:

a) The values of the functions for integer arguments of degrees have been calculated by means of „exact" formulae **) with an accuracy higher than stipulated above.

b) The filling up of the tables thus obtained has been carried out by direct interpolation by using the values of functions directly and not their differences - the order of interpolation being chosen so, that the conditions (1) are satisfied.

Although this method led us in some cases to interpolation with the seventh differences, it has been more economical than the calculation of the functions by means of „exact" formulae, owing to the complicated form of the functions and - especially if calculating the coefficients of the „inverse problem" - owing to the poor convergency of the corresponding series.

The coefficients of the direct problem (the so-called Legendre's series) have been taken from Jordan's Handbuch der Vermessungskunde, and thus the function $V = 1 + e'^2 \cos^2 \varphi$ has been introduced.

The coefficients of the inverse problem have been expressed in functions of the coefficients of the direct problem („problem of the inversion of a series") also partly based on Jordan's work. Full use of the Jordan's series was not possible for the algebraic mistakes due probably to printers' errors.

High requirements of accuracy (conditions 1 and 2) made necessary a new calculation of some powers of the fundamental function V, as reliance on Jordan's values would not safisty such requirements.

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*) To accept the limits of applicability of these tables within the latitudes from $\varphi = 49°$ to $\varphi = 54°$ would mean wasting the whole achievement of geodesy in the years 1918 – 1939 and would compel us to treat such uniform mathematical conceptions as triangulation nets, in a fragmentary way.

**) To emphasize the conventional character of the distinction between an „exact" formula and an interpolation formula, the inverted commas have been used. The difference between calculating the value of a function by a power series and by interpolation formula does not

consist in the difference of accuracy, but in the use of different data – in the first case: one value of the function and $n-1$ derivatives, in the second: n values of the function.

Concluding this introduction I should like to express my sincere thanks to. Prof. Dr. Edward Warchałowski, Rector of the Polytechnic University of Warsaw, for his valuable suggestions and his words of encouragement.

Lastly I wish to offer my sincere thanks to Mr. George Szymoński, civil engineer, for his collaboration in filling up the tables by interpolation.

Stefan Hausbrandt

General Explanations.

The tables serve for the solution of the following problems on Bessel's ellipsoid:

Problem 1.

Given the geographical coordinates: latitude φ_1 and longitude λ_1 of the beginning A_1 of an arc of a geodesic, the length S of the geodesic and its azimuth A_1 at the beginning. Find the increments of the geographical coordinates $\Delta\varphi$, $\Delta\lambda$ and the azimut A_2 of the geodesic at the end point A_2

Problem 2

Given the geographical coordinates of two points: φ_1, λ_1, and φ_2 λ_2. Find the length S of the arc of the geodesic joining these two points and the azimuths of the geodesic at the initial point A_1 and at the end point A_2.

The length S of the arc of the geodesic joining the two points mentioned in this problem we shall call henceforth the length of the geodesic. The products of this length by the cosine and by the sine of the azimuth at the end point we may call the components of the geodesic at the end point. Denoting the components by x and y respectivly we may write:

$$\left.\begin{aligned} x_1 &= S\cos A_1 \\ y_1 &= S\sin A_1 \end{aligned}\right\}\ \text{components at the initial point,}$$
$$\left.\begin{aligned} x_2 &= S\cos A_2 \\ y_2 &= S\sin A_2 \end{aligned}\right\}\ \text{components at the end point,}\qquad \Big\}\ \ldots\ldots 1$$

For the solution of Problem 1 we use the well known Legendre's series. Substituting the variables x and y for the variables S and A, the series will take the form:

$$\left.\begin{aligned} \Delta\varphi &= (x)\,x + (y^2)y^2 + (xy^2)\,x\,y^2 + (x^2)x^2 + (x^2y^2)\,x^2y^2 + (y^4)y^4 + (x^3)x^3 + (xy^4)\,x\,y^4 + (x^3y^2)\,x^3y^2 \\ \Delta\lambda &= (y)\,y + (xy)\,x\,y + (x^2y)\,x^2y + (y^3)y^3 + (x^3y)\,x^3y + (xy^3)\,x\,y^3 + (x^2y^3)\,x^2y^3 + (x^4y)\,x^4y + (y^5)y^5 \end{aligned}\right\}\ \ldots\ldots 2$$

where: $\Delta\varphi$ and $\Delta\lambda$ denote the increments of the geographical coordinates along the geodesic, i.e. $\Delta\varphi = \varphi_2 - \varphi_1$, $\Delta\lambda = \lambda_2 - \lambda_1$

x and y - the components of the geodesic at the initial point and $(x)\,(y)\,(y^2)$ ....., - in the general form: $(x^i\,y^k)$ the coefficients (dependent on the latitude of the initial point) by which the corresponding powers of the componets $x^i\,y^k$ are to be multiplied.

The numerical volues of the coefficients are given in Table 1; it should be remembered that if the increments of the geographical coordinates are to be obtained in seconds of arc the components should be given in hundreds of kilometers, e.g. the length 10254,75 m must be expressed by the number 0,1025475, etc.

The azimuth of the geodesic at the end point will be determined from the ratio of the components at that point:

$$A_2 = \text{arc tg}\,\frac{y_2}{x_2} \qquad \ldots\ldots 3$$

To find the components at the end point we use

the proportion $\dfrac{y_2}{y_1} = \dfrac{(y_2)}{(y_1)}$ whence $y_2 = y_1\dfrac{(y_2)}{(y_1)}$

and the relation $x_2 = \sqrt{S^2 - y_2^2}$ $\Big\}\ \ldots\ldots 4$

(The proportionality of the components y to their corresponding coefficients (y) results from

the well known property of a geodesic on a surface of revolution, namely the constancy of the product: the sine of the azimuth by the radius of the parallel.)

For the solution of Problem 2 we use the series, that can be obtained from transformed Legendre's equations (2), by solving them for x and y.

$$\left.\begin{aligned} x &= (\Delta\varphi)\,\Delta\varphi + (\Delta\lambda^2)\,\Delta\lambda^2 + (\Delta\varphi^2)\,\Delta\varphi^2 + (\Delta\varphi\Delta\lambda^2)\,\Delta\varphi\Delta\lambda^2 + (\Delta\varphi^3)\,\Delta\varphi^3 + (\Delta\varphi^2\Delta\lambda^2)\,\Delta\varphi^2\Delta\lambda^2 + (\Delta\lambda^4)\,\Delta\lambda^4 \\ y &= (\Delta\lambda)\,\Delta\lambda + (\Delta\varphi\Delta\lambda)\,\Delta\varphi\Delta\lambda + (\Delta\lambda^3)\,\Delta\lambda^3 + (\Delta\varphi^2\Delta\lambda)\,\Delta\varphi^2\Delta\lambda + (\Delta\varphi\Delta\lambda^3)\,\Delta\varphi\Delta\lambda^3 + (\Delta\varphi^3\Delta\lambda)\,\Delta\varphi^3\Delta\lambda \end{aligned}\right\} \quad \ldots\ldots 5$$

x and y denote here the components of the geodesic at the initial point, i.e.

$$x = S\cos A_1,$$

$$y = S\sin A_1,$$

$\Delta\varphi$ and $\Delta\lambda$ – the increments of the geographical coordinates from the initial point to the end point,

$$\Delta\varphi = \varphi_2 - \varphi_1,$$

$$\Delta\lambda = \lambda_2 - \lambda_1;$$

lastly $(\Delta\varphi)$, $(\Delta\lambda)$, $(\Delta\varphi\Delta\lambda)$ ..... in the general form $(\Delta\varphi^i\Delta\lambda^k)$ denote the coefficients (dependent on the latitude of the initial point) by which the corresponding powers of the increments $\Delta\varphi^i\ \Delta\lambda^k$ should be multiplied.

The numerical values of the components are given in Table 2:, it should be remembered that if the value of the components is to be obtained in metres the increments should be given in tens of thousand of the seconds of arc, e.g. the increment of 1° should be expressed by the number 0,36000000.

The computation of the series (5) leads us to the values of the components x_1 y_1, from which we can easily obtain the length of the geodesic:

$$S = \sqrt{x_1^2 + y_1^2},$$

and the azimuth at the beginning of the geodesic:

$$A_1 = \text{arc. tg.}\ \frac{y_1}{x_1} \quad \ldots\ldots 6$$

To find the azimuth at the end we can use the proportion: *)

$$\left.\begin{aligned} &\frac{y_2}{y_1} = \frac{(\Delta\lambda_2)}{(\Delta\lambda_2)} \quad \text{whence} \quad y_2 = y_1\,\frac{(\Delta\lambda_1)}{(\Delta\lambda_2)} \\ &\text{and the relation:}\ x_2 = \sqrt{S_2 - y_2^2}, \end{aligned}\right\} \quad \ldots\ldots 7$$

from which we obtain $A_2 = \text{arc. tg.}\ \frac{y_2}{x_2}$ $\ldots\ldots 8$

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*) The proportionality of the components to the reciprocals of the coeffitients $(\Delta\lambda)$ results from the following property of a geodesic on a surface of revolution: the product of the sine of the azimuth by the radius of the parallel is constant.

Hints concerning the Technique of Computation.

While computing it should be remembered that the principle of machine computing is this: to record in writing as little as possible. Thus it is not advisable to write down the values of particular products of the power series 2 and 5; all the factors should be prepared in advance, then multiplied in turn and summed up simultaneously, i.e. the product register should not be cleared until the calculation of the function is completed.

The following is a convenient method of preparing the factors for calculation:
First write down the terms of the first order:

$x =$ $\quad y =$ $\quad$ or $\quad \Delta\varphi =$ $\quad \Delta\lambda =$

Then set in the setting register the term of the first order of one of the variables and multiply it by the value written down; write down the result, multiply it by the value last written; write down the result, multiply it by the value last written; write down the result, etc.

In this way you will obtain – without clearing the setting register the successive powers of the variable,

x
x^2
x^3
x^4

Take always the same number of decimals e.g.

x	$= -0.62152592$	$\Delta\varphi$	$= -0.20324579$
x^2	$= +0.38629447$	$\Delta\varphi^2$	$= +0.04130885$
x^3	$= -0.24009203$	$\Delta\varphi^3$	$= -0.00839585$
x^4	$= +0.14922342$	$\Delta\varphi^4$	$= +0.00170642$

or

The further course of the calculation depends on whether the „table factors" (x)(y)(xy) ..... and ($\Delta\varphi$) ($\Delta\lambda$) ($\Delta\varphi\Delta\lambda$)..... for a given argument φ will appear in the problem once only, or several times, i.e. whether the calculation concerns a single geodesic or a pencil of geodesics through the vertex φ.

In the case of a single geodesic the most practicable method is this.

1) Take a strip of cardboard, 1 cm wide, its length being equal to the width of the table of functions. Place the strip on the table from which you are to take the „table factors", then rule the strip with vertical lines so as to divide it into columns corresponding to those of the table.

2) In the spaces thus obtained on the strip write down successively the corresponding powers and the products of the powers, consulting all the time the headings of the table and the previously prepared table of powers.

3) Having filled up the whole strip, place it over that line of the table which contains the table factors for the nearest latitude with defect, then perform the multiplying and the summing up, setting in the register the number written on the strip and multiplying it by the number printed directly below it on the table. The calculation completed (attention must be paid to the signs), write down the result, denoting it as the value of the sought function for the argument φ (φ with defect).

4) Having cleared the product register pass the strip one line lower and compute in the same way the value of the sought function for the argument φ_+ (φ with excess).

5) From the obtained values of the function for the arguments φ_- and φ_+, we may denote them by f_- and f_+, compute the sought value f of the function for the argument φ by interpolation.

It is convenient to apply direct interpolation, i. e. to multiply the value of the function for the argument with defect by the complement to the unit of the „interpolating fraction"*) to multiply the value of the function for the argument with excess by the interpolating fraction, and to sum up the results. This operation, expresed by the formula:

$$f = (1 - k) f_- + k f_+$$

we perform of course directly by computing machine.

In case of a pencil of geodesics it is convenient to interpolate the values of the table factors for the geographical latitude of the common vertex, and then perform a single calculation for each radius of the pencil.

For the computing of the values of the table factors it is also advisable to apply direct interpolation. Write down on a scrap of cardboard the complement to the unit of the interpolation fraction and below it the fraction itself, then pass the scrap $\boxed{\begin{matrix}1-k\\ k\end{matrix}}$ along the line $\begin{matrix}(1-k)\,f_-\\ k\,f_+\end{matrix}$ and perform the successive multiplications

Note

Concerning the terms of the power series (2) and (5), except the terms with $\textcircled{y}$ and $\textcircled{\Delta\lambda}$, the linear interpolation gives the same results (within the limits of the stipulated accuracy 0."0001 and 0.001 m) as those obtained by interpolation of higher order. Interpolating the value of the term $\textcircled{y}$ or $\textcircled{\Delta\lambda}$ by linear interpolation we risk a reduction of the accuracy of the results, amounting in an extreme case (for a geodesic of the length of 100 km.) to 0."0003 and 0.001 m. If the accuracy is insufficient we can introduce a simple „interpolating correction", which consists in diminishing the term $\textcircled{y}$ by the quantity $p.$, or enlarging the term $\textcircled{\Delta\lambda}$ by the quantity q. The quantities p and q may be obtained from the small tables given on the right margin. They are tabulated for the argument k. We may also introduce a correction into the result, i.e. to correct

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*) The quantity k called here the „interpolating fraction" is the ratio of the difference between the given argument and the table argument with defect to the difference between the table values of the argument with excess and with defect: $k = \frac{\varphi - \varphi_-}{\varphi_+ - \varphi_-}$; e. g. interpolating from our tables for $\varphi = 46°\,15'\,20"$ we obtain $k = \frac{20"}{60"} = 0{,}333333\ldots$ etc.

the obtained increment of the longitude $\Delta\lambda$ (Problem 1) by the quantity $p.y$, or to correct the obtained component y (Problem 2) by the quantity $q.\Delta\lambda$. The above corrections, however, are of very little significance; for the length of 100 km of the gedesic it would be logically quite sound to ignore the corrections altogether. In the numerical examples given below we are dealing with geodesics of the length of more then 100 km, and the corrections mentio-ned above have been introduced.

Problem 1

Given:

$\varphi_1 = 50°45'10''.2709 = 50°45'.171182$ k for interpolation $= 0.171182$, $1 - k = 0.828818$

$S = 103275{,}242\ m = 1{,}03275242\ hk$ (hundred kilometres)

$A_1 = 127°0'0''$ $\quad \cos A_1 = -0{,}601815024$

$\sin A_1 = +0{,}798635508$

Calculation of the components and their powers:

$x = S \cos A = -0{,}62152592$ $\quad y = S \sin A = +0{,}82479275$

$x^2 =$	$+0{,}38629447$	$y^2 =$	$+0{,}68028308$
$x^3 =$	$-0{,}24009203$	$y^3 =$	$+0{,}56109255$
$x^4 =$	$+0{,}14922342$	$y^4 =$	$+0{,}46278507$
$x^5 =$	$-0{,}09274622$	$y^5 =$	$+0{,}38170177$

Calculation of the increment in latitude. (To make the method quite clear the strip of cardboard is shown below as a sample ⊂⊃, placed on the corresponding fragment of the table. It is of course unnecessary to copy that fragment while making the actual calculations).

φ-50°	x	y^2	xy^2	x^2	x^2y^2	y^4	x^3	xy^4	x^3y^2
	−0.62152592	0.68028308	−0.42281357	0.38629447	0.26278959	0.46278507	−0.24009203	−0.28763292	−0.16333055
45'	3236.51327	−30.99508	−0.72132	−0.25011	−0.01643	0.00348	0.00053	0.00024	−0.00038
46'	3236.50400	−31.01337	−0.72202	−0.25006	−0.01645	0.00348	0.00053	0.00024	−0.00038

$\Delta\varphi_{50°45'} = 2032''.45679$ | $0{,}828818$

$\Delta k_{50°46'} = 2032''.46317$ | $0{,}171182$

$\Delta\varphi = -2032''.45788 = -33'52''.4579$

$\varphi_1 = 50°45'10''.2709$

$\varphi_2 = 50°11'17''.8130 = 50°11'.296883$

$K = 0.296883$

$1-K = 0.703117$

Calculation of the increment in longitude (cf. the note above).

φ-50°	y	xy	x^2y	y^3	x^3y	xy^3	x^2y^3	x^4y	y^5
	0.82479275	−0.51263007	0.31861288	0.56109255	−0.19802617	−0.34873356	0.21674695	0.12307839	0.38170177
45'	5101.63400	97.71352	2.28911	−0.62385	0.05180	−0.04382	−0.00200	0.00119	0.00017
46'	5103.44632	97.80620	2.29214	−0.62481	0.05189	−0.04391	−0.00201	0.00119	0.00017

$\Delta k_{50°45'} = 4158''.08395$ | $0{,}828818$

$\Delta k_{50°46'} = 4159''.53167$ | $0{,}171182$

$\Delta k = 4158''.33177$ *or if we take into consideration*

corr. p.y. -0.00009 *the correction p.y.*

$\Delta k = 4158''.3317 = 1°09'18''.3317$

$K_1 = 22°20'15''.00$

$K_2 = 23°29'33''.3317$

Calculation of the azimuth of the geodesic 1 - 2 at point 2

$y_1 = 5101.63400.\ 0.828818$

$5103.44632.\ 0.171182$ $\Big\}$ $= 5101.944237$

corr. p.y. -0.00011

5101.94413

$y_2 = 5041.02591.0.703117$

$5042.78086.0.296883$ $\Big\}$ $= 5041.546925$

corr. p.y. -0.00018

5041.54674

$y_2 = y_1 \dfrac{y_2}{y_1} = \dfrac{0.82479275 \cdot 5041.54674}{5101.94413} = 0.81502876$

$x_2 = \sqrt{S^2 - y_2^2} = -0.63427571$

$A_2 = \text{arc. tg.} \dfrac{0.81502876}{-0.63427571}$, $\quad -1.28497552$, $\quad A_2 = 127°53'27''.397$

Problem 2

Given:

$\varphi_1 = 50°45'10''.2709$ $k = 0.171182$ $1-k = 0.828818$

$\varphi_2 = 50°11'17''.8130$ $k = 0.296883$ $1-k = 0.703117$

λ_1 22°20'15''.00

λ_2 23°29'33''.3317

Calculation of the increments and their powers:

$\Delta\varphi_{12}$	$-33'52'.4579 = -2032''.4579 = -0.20324579$	$\Delta\lambda = 1°09'18''.3317 = 4158''.3317 = +0.41583317$
$\Delta\varphi^2$	$+0.04130885$	$\Delta\lambda^2 \quad +0.17291723$
$\Delta\varphi^3$	-0.00839585	$\Delta\lambda^3 \quad +0.07190472$
$\Delta\varphi^4$	$+0.00170642$	$\Delta\lambda^4 \quad +0.02990037$

Calculation of the component x (To make the method clear the strip of cardboard is shown below as a sample ⊂⊃, placed on the corresponding fragment of the table. It is of course unnecessary to copy that fragment while making the actual calculations).

$\varphi=50°$	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^2)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta\lambda^2)$	$(\Delta\lambda^4)$
	−0.20324579	0.17291723	0.04130885	−0.03514470	−0.00839585	0.00714301	0.02990037
45'	308974.478	3679.568	73.774	−169.170	−0.449	−5.636	−0.153
46'	308975.364	3679.135	73.766	−169.308	−0.450	−5.635	−0.153

$x_{\varphi=50°45'} = -62152.5492$ | 0.828818

$x_{\varphi=50°46'} = -62152.7997$ | 0.171182

$x = -62152.592$ m.

Calculation of the component y (cf. the note above).

$\varphi=50°$	$(\Delta\lambda)$	$(\Delta\varphi\Delta\lambda)$	$(\Delta\lambda^3)$	$(\Delta\varphi^2\Delta\lambda)$	$(\Delta\varphi\Delta\lambda^3)$	$(\Delta\varphi^3\Delta\lambda)$
	0.41583317	−0.08451634	0.07190472	0.01717759	−0.01461433	−0.00349127
45'	196015.629	−11600.019	−46.048	−155.932	0.891	−0.005
46'	195946.020	−11602.808	−46.054	−155.878	0.894	−0.005

$y_{\varphi=50°45'} = 82484.1889$ | 0.828818

$y_{\varphi=50°46'} = 82455.4794$ | 0.171182

$y = 82479.2744$

corr. $\Delta\lambda_2$ 0.0005

$y = 82479.275$ m

Calculation of the azimuth at the initial point and of the length of the geodesic.

$$A_1 = \text{arc. tg.} \frac{82479.275}{-62152.592}, \quad -1.32704482, \quad A_1 = 127°00$$

$$S = \sqrt{x^2 + y^2} = 103275.242 \text{ m.}$$

Calculation of the azimuth of the geodesic 1 - 2 at point 2.

$(\Delta\lambda)$ $196015.629 \cdot 0.828818$ / $195946.020 \cdot 0.171172$ $= 196003.7132$

corr. 1

196003.714

$(\Delta\lambda_2)$ $198372.319 \cdot 0.703117$ / $198303.283 \cdot 0.296883$ $= 198351.8234$

corr. 1.7

198351.825

$$y_2 = \frac{y_1(\Delta\lambda_1)}{(\Delta\lambda_2)} = \frac{82479.275 \cdot 196003.714}{198351.825} = 81502.876$$

$$x_2 = -\sqrt{S^2 - y_2^2} = -63427.571$$

$$A_2 = \text{arc. tg.} \frac{81502.876}{-63427.571} = \text{arc. tg. } (-1.28497552) \quad A_2 = 127°53'27''.397$$

Przyrost szerokości geograficznej $\Delta\varphi$

$\Delta\varphi'' = (x) X + (y^2) Y^2 + (xy^2) XY^2 + \ldots$ gdzie $X = s\cos A$ $Y = s\sin A$

s długość linji geodezyjnej wyrażona w setkach kilometrów
A azymut linji geodezyjnej w punkcie wyjściowym

φ 48°	(x)	(y^2)	(xy^2)	(x^2)	(x^2y^2)	(y^4)	(x^3)	(xy^4)	(x^3y^2)
0'	3238.05609	-28.14308	-0.61739	-0.25400	-0.01310	0.00270	0.00028	0.00017	-0.00028
1'	3238.04668	-28.15944	-0.61796	-0.25398	-0.01312	0.00270	0.00028	0.00017	-0.00028
2'	3238.03726	-28.17581	-0.61852	-0.25397	-0.01314	0.00271	0.00028	0.00017	-0.00028
3'	3238.02785	-28.19219	-0.61909	-0.25395	-0.01315	0.00271	0.00028	0.00017	-0.00028
4'	3238.01844	-28.20858	-0.61966	-0.25393	-0.01317	0.00272	0.00028	0.00017	-0.00028
5'	3238.00903	-28.22498	-0.62023	-0.25392	-0.01319	0.00272	0.00029	0.00017	-0.00028
6'	3237.99962	-28.24139	-0.62080	-0.25390	-0.01321	0.00272	0.00029	0.00017	-0.00028
7'	3237.99021	-28.25781	-0.62137	-0.25388	-0.01322	0.00273	0.00029	0.00017	-0.00028
8'	3237.98080	-28.27425	-0.62194	-0.25387	-0.01324	0.00273	0.00029	0.00018	-0.00028
9'	3237.97140	-28.29069	-0.62252	-0.25385	-0.01326	0.00274	0.00029	0.00018	-0.00029
10'	3237.96199	-28.30715	-0.62309	-0.25383	-0.01328	0.00274	0.00029	0.00018	-0.00029
11'	3237.95258	-28.32361	-0.62366	-0.25381	-0.01329	0.00275	0.00030	0.00018	-0.00029
12'	3237.94318	-28.34009	-0.62424	-0.25380	-0.01331	0.00275	0.00030	0.00018	-0.00029
13'	3237.93377	-28.35657	-0.62482	-0.25378	-0.01333	0.00275	0.00030	0.00018	-0.00029
14'	3237.92437	-28.37307	-0.62539	-0.25376	-0.01335	0.00276	0.00030	0.00018	-0.00029
15'	3237.91496	-28.38958	-0.62597	-0.25374	-0.01337	0.00276	0.00030	0.00018	-0.00029
16'	3237.90556	-28.40610	-0.62655	-0.25373	-0.01338	0.00277	0.00030	0.00018	-0.00029
17'	3237.89616	-28.42263	-0.62713	-0.25371	-0.01340	0.00277	0.00030	0.00018	-0.00029
18'	3237.88675	-28.43917	-0.62770	-0.25369	-0.01342	0.00277	0.00031	0.00018	-0.00029
19'	3237.87735	-28.45572	-0.62828	-0.25367	-0.01344	0.00278	0.00031	0.00018	-0.00029
20'	3237.86795	-28.47228	-0.62887	-0.25365	-0.01346	0.00278	0.00031	0.00018	-0.00029
21'	3237.85855	-28.48885	-0.62945	-0.25363	-0.01347	0.00279	0.00031	0.00018	-0.00029
22'	3237.84915	-28.50544	-0.63003	-0.25362	-0.01349	0.00279	0.00031	0.00018	-0.00029
23'	3237.83975	-28.52203	-0.63061	-0.25360	-0.01351	0.00280	0.00031	0.00018	-0.00029
24'	3237.83035	-28.53863	-0.63120	-0.25358	-0.01353	0.00280	0.00032	0.00018	-0.00029
25'	3237.82095	-28.55525	-0.63178	-0.25356	-0.01355	0.00280	0.00032	0.00018	-0.00029
26'	3237.81156	-28.57188	-0.63236	-0.25354	-0.01357	0.00281	0.00032	0.00018	-0.00029
27'	3237.80216	-28.58851	-0.63295	-0.25352	-0.01358	0.00281	0.00032	0.00018	-0.00029
28'	3237.79276	-28.60516	-0.63354	-0.25350	-0.01360	0.00282	0.00032	0.00018	-0.00029
29'	3237.78337	-28.62182	-0.63412	-0.25349	-0.01362	0.00282	0.00032	0.00018	-0.00030
30'	3237.77398	-28.63849	-0.63471	-0.25347	-0.01364	0.00283	0.00032	0.00018	-0.00030
31'	3237.76458	-28.65517	-0.63530	-0.25345	-0.01366	0.00283	0.00033	0.00018	-0.00030
32'	3237.75519	-28.67186	-0.63589	-0.25343	-0.01368	0.00283	0.00033	0.00018	-0.00030
33'	3237.74580	-28.68857	-0.63648	-0.25341	-0.01369	0.00284	0.00033	0.00018	-0.00030
34'	3237.73640	-28.70528	-0.63707	-0.25339	-0.01371	0.00284	0.00033	0.00018	-0.00030
35'	3237.72701	-28.72201	-0.63766	-0.25337	-0.01373	0.00285	0.00033	0.00018	-0.00030
36'	3237.71762	-28.73874	-0.63826	-0.25335	-0.01375	0.00285	0.00033	0.00018	-0.00030
37'	3237.70823	-28.75549	-0.63885	-0.25333	-0.01377	0.00286	0.00034	0.00019	-0.00030
38'	3237.69884	-28.77225	-0.63944	-0.25331	-0.01379	0.00286	0.00034	0.00019	-0.00030
39'	3237.68946	-28.78902	-0.64004	-0.25329	-0.01381	0.00286	0.00034	0.00019	-0.00030
40'	3237.68007	-28.80580	-0.64063	-0.25327	-0.01382	0.00287	0.00034	0.00019	-0.00030
41'	3237.67068	-28.82258	-0.64123	-0.25325	-0.01384	0.00287	0.00034	0.00019	-0.00030
42'	3237.66130	-28.83939	-0.64183	-0.25323	-0.01386	0.00288	0.00034	0.00019	-0.00030
43'	3237.65191	-28.85620	-0.64243	-0.25321	-0.01388	0.00288	0.00034	0.00019	-0.00030
44'	3237.64253	-28.87302	-0.64302	-0.25319	-0.01390	0.00289	0.00035	0.00019	-0.00030
45'	3237.63314	-28.88986	-0.64362	-0.25317	-0.01392	0.00289	0.00035	0.00019	-0.00030
46'	3237.62376	-28.90671	-0.64422	-0.25315	-0.01394	0.00289	0.00035	0.00019	-0.00030
47'	3237.61438	-28.92356	-0.64482	-0.25313	-0.01396	0.00290	0.00035	0.00019	-0.00030
48'	3237.60500	-28.94043	-0.64542	-0.25311	-0.01398	0.00290	0.00035	0.00019	-0.00031
49'	3237.59561	-28.95731	-0.64602	-0.25309	-0.01399	0.00291	0.00035	0.00019	-0.00031
50'	3237.58623	-28.97420	-0.64663	-0.25307	-0.01401	0.00291	0.00036	0.00019	-0.00031
51'	3237.57685	-28.99111	-0.64723	-0.25305	-0.01403	0.00292	0.00036	0.00019	-0.00031
52'	3237.56748	-29.00802	-0.64783	-0.25303	-0.01405	0.00292	0.00036	0.00019	-0.00031
53'	3237.55810	-29.02494	-0.64844	-0.25300	-0.01407	0.00293	0.00036	0.00019	-0.00031
54'	3237.54872	-29.04188	-0.64904	-0.25298	-0.01409	0.00293	0.00036	0.00019	-0.00031
55'	3237.53934	-29.05883	-0.64965	-0.25296	-0.01411	0.00293	0.00036	0.00019	-0.00031
56'	3237.52997	-29.07579	-0.65026	-0.25294	-0.01413	0.00294	0.00036	0.00019	-0.00031
57'	3237.52059	-29.09276	-0.65087	-0.25292	-0.01415	0.00294	0.00037	0.00019	-0.00031
58'	3237.51122	-29.10974	-0.65148	-0.25290	-0.01417	0.00295	0.00037	0.00019	-0.00031
59'	3237.50185	-29.12673	-0.65209	-0.25288	-0.01419	0.00295	0.00037	0.00019	-0.00031
60'	3237.49247	-29.14373	-0.65270	-0.25285	-0.01421	0.00296	0.00037	0.00019	-0.00031

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda'' = (y) Y + (xy) XY + (x^2y) X^2Y + \ldots$ gdzie $X = S\cos A$ $Y = S\sin A$ S długość linii geodezyjnej wyrażona w setkach kilometr. A azymut linii geodezyjnej w punkcie wyjściowym

φ 48°	(y)	(xy)	(x^2y)	(y^3)	(x^3y)	(xy^3)	(x^2y^3)	(x^4y)	(y^5)	Poprawka interpolacyjna dla wyrazu (y)	
										K'	p.
0	4824.68414	83.86603	1.85297	-0.48594	0.03904	-0.03219	-0.00138	0.00084	0.00011		
1'	4826.23886	83.94207	1.85527	-0.48666	0.03910	-0.03225	-0.00138	0.00084	0.00011		
2'	4827.79499	84.01819	1.85757	-0.48739	0.03917	-0.03231	-0.00138	0.00084	0.00011		
3'	4829.35253	84.09440	1.85988	-0.48812	0.03923	-0.03237	-0.00139	0.00084	0.00011		
4'	4830.91149	84.17070	1.86219	-0.48885	0.03930	-0.03242	-0.00139	0.00084	0.00011		
5'	4832.47187	84.24709	1.86450	-0.48957	0.03936	-0.03248	-0.00139	0.00084	0.00011		
6'	4834.03367	84.32356	1.86682	-0.49031	0.03943	-0.03254	-0.00139	0.00085	0.00011		
7'	4835.59690	84.40013	1.86915	-0.49104	0.03949	-0.03260	-0.00140	0.00085	0.00011		
8'	4837.16154	84.47678	1.87147	-0.49177	0.03956	-0.03266	-0.00140	0.00085	0.00011		
9'	4838.72762	84.55352	1.87380	-0.49251	0.03963	-0.03272	-0.00140	0.00085	0.00011		
10'	4840.29512	84.63035	1.87614	-0.49324	0.03969	-0.03278	-0.00141	0.00085	0.00011		
11'	4841.86405	84.70727	1.87847	-0.49398	0.03976	-0.03284	-0.00141	0.00086	0.00012		
12	4843.43441	84.78428	1.88081	-0.49472	0.03983	-0.03290	-0.00141	0.00086	0.00012		
13'	4845.00620	84.86138	1.88316	-0.49546	0.03989	-0.03296	-0.00142	0.00086	0.00012	0'01	1
14'	4846.57943	84.93857	1.88551	-0.49620	0.03996	-0.03302	-0.00142	0.00086	0.00012	0'02	1
15'	4848.15409	85.01585	1.88786	-0.49694	0.04003	-0.03308	-0.00142	0.00086	0.00012	0'03	2
16	4849.73019	85.09322	1.89022	-0.49768	0.04009	-0.03314	-0.00143	0.00086	0.00012	0'04	3
17'	4851.30773	85.17068	1.89258	-0.49843	0.04016	-0.03321	-0.00143	0.00087	0.00012	0'05	3
18'	4852.88671	85.24822	1.89494	-0.49917	0.04023	-0.03327	-0.00143	0.00087	0.00012	0'06	4
19'	4854.46714	85.32586	1.89731	-0.49992	0.04030	-0.03333	-0.00144	0.00087	0.00012	0'07	5
20'	4856.04900	85.40359	1.89968	-0.50067	0.04036	-0.03339	-0.00144	0.00087	0.00012	0'08	5
21'	4857.63232	85.48141	1.90206	-0.50142	0.04043	-0.03345	-0.00144	0.00087	0.00012	0'09	6
22'	4859.21708	85.55932	1.90444	-0.50217	0.04050	-0.03351	-0.00145	0.00088	0.00012	0'10	7
23'	4860.80329	85.63733	1.90682	-0.50292	0.04057	-0.03357	-0.00145	0.00088	0.00012	0'12	8
24'	4862.39095	85.71542	1.90921	-0.50367	0.04063	-0.03363	-0.00145	0.00088	0.00012	0'14	9
25'	4863.98006	85.79380	1.91160	-0.50442	0.04070	-0.03370	-0.00146	0.00088	0.00012	0'15	10
26'	4865.57063	85.87188	1.91400	-0.50518	0.04077	-0.03376	-0.00146	0.00088	0.00012	0'18	11
27'	4867.16265	85.95024	1.91640	-0.50594	0.04084	-0.03382	-0.00146	0.00088	0.00012	0'20	12
28'	4868.75613	86.02870	1.91880	-0.50670	0.04091	-0.03388	-0.00147	0.00089	0.00012	0'25	14
29'	4870.35107	86.10725	1.92121	-0.50746	0.04098	-0.03395	-0.00147	0.00089	0.00012	0'30	15
30'	4871.94747	86.18589	1.92362	-0.50822	0.04105	-0.03401	-0.00147	0.00089	0.00012	0'35	17
31'	4873.54533	86.26463	1.92604	-0.50898	0.04112	-0.03407	-0.00148	0.00089	0.00012	0'40	18
32'	4875.14466	86.34345	1.92846	-0.50974	0.04118	-0.03413	-0.00148	0.00089	0.00012	0'60	19
33'	4876.74546	86.42237	1.93088	-0.51051	0.04125	-0.03420	-0.00148	0.00090	0.00012	0'65	17
34'	4878.34772	86.50138	1.93331	-0.51127	0.04132	-0.03426	-0.00149	0.00090	0.00012	0'70	15
35'	4879.95145	86.58049	1.93574	-0.51204	0.04139	-0.03432	-0.00149	0.00090	0.00012	0'75	14
36'	4881.55666	86.65968	1.93817	-0.51281	0.04146	-0.03439	-0.00149	0.00090	0.00012	0'80	12
37'	4883.16334	86.73897	1.94061	-0.51358	0.04153	-0.03445	-0.00150	0.00090	0.00012	0'82	11
38'	4884.77149	86.81835	1.94306	-0.51435	0.04160	-0.03451	-0.00150	0.00090	0.00012	0'84	10
39'	4886.38112	86.89783	1.94551	-0.51512	0.04167	-0.03458	-0.00150	0.00091	0.00012	0'86	9
40'	4887.99222	86.97740	1.94796	-0.51590	0.04174	-0.03464	-0.00151	0.00091	0.00012	0'88	8
41'	4889.60481	87.05706	1.95041	-0.51667	0.04181	-0.03470	-0.00151	0.00091	0.00012	0'90	7
42'	4891.21888	87.13682	1.95287	-0.51745	0.04188	-0.03477	-0.00151	0.00091	0.00012	0'91	6
43'	4892.83443	87.21667	1.95534	-0.51822	0.04196	-0.03483	-0.00152	0.00091	0.00012	0'92	5
44'	4894.45147	87.29661	1.95780	-0.51900	0.04203	-0.03490	-0.00152	0.00092	0.00012	0'93	5
45'	4896.07000	87.37665	1.96027	-0.51978	0.04210	-0.03496	-0.00152	0.00092	0.00012	0'94	4
46'	4897.69001	87.45679	1.96275	-0.52056	0.04217	-0.03503	-0.00153	0.00092	0.00012	0'95	3
47'	4899.31151	87.53701	1.96523	-0.52135	0.04224	-0.03509	-0.00153	0.00092	0.00013	0'96	3
48'	4900.93451	87.61734	1.96771	-0.52213	0.04231	-0.03516	-0.00153	0.00092	0.00013	0'97	2
49'	4902.55900	87.69775	1.97020	-0.52292	0.04238	-0.03522	-0.00154	0.00093	0.00013	0'98	1
50'	4904.18499	87.77827	1.97269	-0.52370	0.04245	-0.03529	-0.00154	0.00093	0.00013	0'99	1
51	4905.81247	87.85887	1.97519	-0.52449	0.04253	-0.03535	-0.00154	0.00093	0.00013		
52'	4907.44146	87.93958	1.97769	-0.52528	0.04260	-0.03542	-0.00155	0.00093	0.00013		
53'	4909.07194	88.02037	1.98020	-0.52607	0.04267	-0.03548	-0.00155	0.00093	0.00013		
54'	4910.70393	88.10127	1.98270	-0.52686	0.04274	-0.03555	-0.00155	0.00094	0.00013		
55'	4912.33742	88.18226	1.98522	-0.52766	0.04282	-0.03562	-0.00156	0.00094	0.00013		
56'	4913.97242	88.26334	1.98774	-0.52845	0.04289	-0.03568	-0.00156	0.00094	0.00013		
57'	4915.60893	88.34452	1.99026	-0.52925	0.04296	-0.03575	-0.00156	0.00094	0.00013		
58'	4917.24695	88.42580	1.99278	-0.53005	0.04303	-0.03581	-0.00157	0.00094	0.00013		
59'	4918.88648	88.50717	1.99531	-0.53085	0.04311	-0.03588	-0.00157	0.00095	0.00013		
60	4920.52752	88.58864	1.99785	-0.53165	0.04318	-0.03595	-0.00157	0.00095	0.00013		

A.K

I Przyrost szerokości geograficznej $\Delta\varphi$

$\Delta\varphi'' = (A)x + (B)y^2 + (C)xy^2 + \ldots$ gdzie $x = S\cos A$ $y = S\sin A$

S oznacza długość linii geodezyjnej wyrażoną w setkach kilometrów
A oznacza azymut linii geodezyjnej w punkcie wyjściowym

φ 49°	(A)	(y²)	(xy²)	(x³)	(x²y²)	(y⁴)	(x³)	(xy⁴)	(x³y²)
0'	3237.49247	-29.14373	-0.65270	-0.25285	-0.01421	0.00296	0.00037	0.00019	-0.00031
1'	3237.48310	-29.16075	-0.65331	-0.25283	-0.01423	0.00296	0.00037	0.00019	-0.00031
2'	3237.47373	-29.17777	-0.65392	-0.25281	-0.01424	0.00297	0.00037	0.00019	-0.00031
3'	3237.46436	-29.19481	-0.65453	-0.25279	-0.01426	0.00297	0.00038	0.00019	-0.00031
4'	3237.45499	-29.21186	-0.65515	-0.25277	-0.01428	0.00297	0.00038	0.00019	-0.00031
5'	3237.44562	-29.22892	-0.65576	-0.25275	-0.01430	0.00298	0.00038	0.00020	-0.00031
6'	3237.43625	-29.24599	-0.65637	-0.25272	-0.01432	0.00298	0.00038	0.00020	-0.00031
7'	3237.42689	-29.26308	-0.65699	-0.25270	-0.01434	0.00299	0.00038	0.00020	-0.00032
8'	3237.41752	-29.28017	-0.65761	-0.25268	-0.01436	0.00299	0.00038	0.00020	-0.00032
9'	3237.40815	-29.29728	-0.65822	-0.25266	-0.01438	0.00300	0.00038	0.00020	-0.00032
10'	3237.39879	-29.31439	-0.65884	-0.25263	-0.01440	0.00300	0.00039	0.00020	-0.00032
11'	3237.38943	-29.33152	-0.65946	-0.25261	-0.01442	0.00301	0.00039	0.00020	-0.00032
12'	3237.38006	-29.34866	-0.66008	-0.25259	-0.01444	0.00301	0.00039	0.00020	-0.00032
13'	3237.37070	-29.36582	-0.66070	-0.25257	-0.01446	0.00302	0.00039	0.00020	-0.00032
14'	3237.36134	-29.38298	-0.66132	-0.25254	-0.01448	0.00302	0.00039	0.00020	-0.00032
15'	3237.35198	-29.40015	-0.66194	-0.25252	-0.01450	0.00302	0.00039	0.00020	-0.00032
16'	3237.34262	-29.41734	-0.66257	-0.25250	-0.01452	0.00303	0.00040	0.00020	-0.00032
17'	3237.33326	-29.43454	-0.66319	-0.25247	-0.01454	0.00303	0.00040	0.00020	-0.00032
18'	3237.32390	-29.45175	-0.66382	-0.25245	-0.01456	0.00304	0.00040	0.00020	-0.00032
19'	3237.31454	-29.46897	-0.66444	-0.25243	-0.01458	0.00304	0.00040	0.00020	-0.00032
20'	3237.30519	-29.48620	-0.66507	-0.25240	-0.01460	0.00305	0.00040	0.00020	-0.00032
21'	3237.29583	-29.50345	-0.66569	-0.25238	-0.01462	0.00305	0.00040	0.00020	-0.00032
22'	3237.28648	-29.52071	-0.66632	-0.25236	-0.01464	0.00306	0.00040	0.00020	-0.00032
23'	3237.27712	-29.53797	-0.66695	-0.25233	-0.01466	0.00306	0.00041	0.00020	-0.00032
24'	3237.26777	-29.55525	-0.66758	-0.25231	-0.01468	0.00307	0.00041	0.00020	-0.00033
25'	3237.25842	-29.57254	-0.66821	-0.25229	-0.01470	0.00307	0.00041	0.00020	-0.00033
26'	3237.24907	-29.58985	-0.66884	-0.25226	-0.01472	0.00308	0.00041	0.00020	-0.00033
27'	3237.23972	-29.60716	-0.66947	-0.25224	-0.01474	0.00308	0.00041	0.00020	-0.00033
28'	3237.23037	-29.62449	-0.67010	-0.25222	-0.01476	0.00309	0.00041	0.00020	-0.00033
29'	3237.22102	-29.64183	-0.67074	-0.25219	-0.01478	0.00309	0.00042	0.00020	-0.00033
30'	3237.21167	-29.65918	-0.67137	-0.25217	-0.01480	0.00309	0.00042	0.00020	-0.00033
31'	3237.20232	-29.67654	-0.67201	-0.25214	-0.01482	0.00310	0.00042	0.00021	-0.00033
32'	3237.19298	-29.69391	-0.67264	-0.25212	-0.01484	0.00310	0.00042	0.00021	-0.00033
33'	3237.18363	-29.71130	-0.67328	-0.25209	-0.01486	0.00311	0.00042	0.00021	-0.00033
34'	3237.17429	-29.72869	-0.67392	-0.25207	-0.01488	0.00311	0.00042	0.00021	-0.00033
35'	3237.16494	-29.74610	-0.67455	-0.25205	-0.01490	0.00312	0.00042	0.00021	-0.00033
36'	3237.15560	-29.76352	-0.67519	-0.25202	-0.01492	0.00312	0.00043	0.00021	-0.00033
37'	3237.14626	-29.78096	-0.67583	-0.25200	-0.01495	0.00313	0.00043	0.00021	-0.00033
38'	3237.13692	-29.79840	-0.67647	-0.25197	-0.01497	0.00313	0.00043	0.00021	-0.00033
39'	3237.12758	-29.81586	-0.67711	-0.25195	-0.01499	0.00314	0.00043	0.00021	-0.00033
40'	3237.11824	-29.83333	-0.67776	-0.25192	-0.01501	0.00314	0.00043	0.00021	-0.00033
41'	3237.10890	-29.85081	-0.67840	-0.25190	-0.01503	0.00315	0.00043	0.00021	-0.00034
42'	3237.09956	-29.86830	-0.67904	-0.25187	-0.01505	0.00315	0.00044	0.00021	-0.00034
43'	3237.09023	-29.88580	-0.67969	-0.25185	-0.01507	0.00316	0.00044	0.00021	-0.00034
44'	3237.08089	-29.90332	-0.68033	-0.25182	-0.01509	0.00316	0.00044	0.00021	-0.00034
45'	3237.07156	-29.92085	-0.68098	-0.25179	-0.01511	0.00317	0.00044	0.00021	-0.00034
46'	3237.06222	-29.93839	-0.68163	-0.25177	-0.01513	0.00317	0.00044	0.00021	-0.00034
47'	3237.05289	-29.95594	-0.68228	-0.25174	-0.01515	0.00318	0.00044	0.00021	-0.00034
48'	3237.04356	-29.97351	-0.68292	-0.25172	-0.01517	0.00318	0.00044	0.00021	-0.00034
49'	3237.03423	-29.99108	-0.68357	-0.25169	-0.01519	0.00319	0.00045	0.00021	-0.00034
50'	3237.02490	-30.00867	-0.68422	-0.25167	-0.01522	0.00319	0.00045	0.00021	-0.00034
51'	3237.01557	-30.02627	-0.68488	-0.25164	-0.01524	0.00320	0.00045	0.00021	-0.00034
52'	3237.00624	-30.04388	-0.68553	-0.25161	-0.01526	0.00320	0.00045	0.00021	-0.00034
53'	3236.99691	-30.06151	-0.68618	-0.25159	-0.01528	0.00321	0.00045	0.00021	-0.00034
54'	3236.98759	-30.07914	-0.68683	-0.25156	-0.01530	0.00321	0.00045	0.00021	-0.00034
55'	3236.97826	-30.09679	-0.68749	-0.25154	-0.01532	0.00322	0.00045	0.00022	-0.00034
56'	3236.96894	-30.11445	-0.68814	-0.25151	-0.01534	0.00322	0.00046	0.00022	-0.00034
57'	3236.95961	-30.13213	-0.68880	-0.25148	-0.01536	0.00323	0.00046	0.00022	-0.00034
58'	3236.95029	-30.14981	-0.68946	-0.25146	-0.01539	0.00323	0.00046	0.00022	-0.00035
59'	3236.94097	-30.16751	-0.69012	-0.25143	-0.01541	0.00324	0.00046	0.00022	-0.00035
60'	3236.93165	-30.18522	-0.69077	-0.25140	-0.01543	0.00324	0.00046	0.00022	-0.00035

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda'' = (y)y + (xy)xy + (x^2y)x^2y + \dots$ gdzie $x = S\cos A$ $y = S\sin A$ S długość linii geodezyjnej wyrażona w setkach kilometrów, A azymut linii geodezyjnej w punkcie wyjściowym.

φ 49°	(y)	(xy)	(x²y)	(y³)	(x³y)	(xy³)	(x²y³)	(x⁴y)	(y⁵)	Poprawka interpolacyjna dla wyrazu (y)	
										K'	p.
0'	4920.52752	88.58864	1.99785	-0.53165	0.04318	-0.03595	-0.00157	0.00095	0.00013		
1'	4922.17008	88.67021	2.00038	-0.53245	0.04325	-0.03602	-0.00158	0.00095	0.00013		
2'	4923.81416	88.75188	2.00293	-0.53325	0.04333	-0.03608	-0.00158	0.00095	0.00013		
3'	4925.45975	88.83364	2.00547	-0.53406	0.04340	-0.03615	-0.00159	0.00095	0.00013		
4'	4927.10687	88.91549	2.00802	-0.53486	0.04348	-0.03622	-0.00159	0.00096	0.00013		
5'	4928.75551	88.99745	2.01058	-0.53567	0.04355	-0.03628	-0.00159	0.00096	0.00013		
6'	4930.40567	89.07950	2.01314	-0.53648	0.04362	-0.03635	-0.00160	0.00096	0.00013		
7'	4932.05736	89.16165	2.01570	-0.53729	0.04370	-0.03642	-0.00160	0.00096	0.00013		
8'	4933.71058	89.24390	2.01827	-0.53810	0.04377	-0.03649	-0.00160	0.00096	0.00013		
9'	4935.36533	89.32625	2.02084	-0.53891	0.04385	-0.03656	-0.00161	0.00097	0.00013		
10'	4937.02161	89.40869	2.02342	-0.53973	0.04392	-0.03662	-0.00161	0.00097	0.00013		
11'	4938.67942	89.49124	2.02600	-0.54054	0.04400	-0.03669	-0.00161	0.00097	0.00013		
12'	4940.33877	89.57388	2.02858	-0.54136	0.04407	-0.03676	-0.00162	0.00097	0.00013	0.01	1
13	4941.99966	89.65662	2.03117	-0.54218	0.04415	-0.03683	-0.00162	0.00097	0.00013	0.02	1
14	4943.66208	89.73946	2.03377	-0.54300	0.04422	-0.03690	-0.00163	0.00098	0.00013	0.03	2
15	4945.32605	89.82239	2.03636	-0.54382	0.04430	-0.03697	-0.00163	0.00098	0.00013	0.04	3
16	4946.99156	89.90543	2.03897	-0.54464	0.04438	-0.03704	-0.00163	0.00098	0.00013	0.05	4
17'	4948.65862	89.98857	2.04157	-0.54546	0.04445	-0.03710	-0.00164	0.00098	0.00013	0.06	4
18	4950.32722	90.07180	2.04418	-0.54629	0.04453	-0.03717	-0.00164	0.00098	0.00014	0.07	5
19'	4951.99737	90.15514	2.04680	-0.54712	0.04460	-0.03724	-0.00164	0.00099	0.00014	0.08	6
20'	4953.66907	90.23857	2.04942	-0.54794	0.04468	-0.03731	-0.00165	0.00099	0.00014	0.09	6
21'	4955.34232	90.32211	2.05204	-0.54877	0.04476	-0.03738	-0.00165	0.00099	0.00014	0.10	7
22'	4957.01713	90.40574	2.05467	-0.54960	0.04483	-0.03745	-0.00166	0.00099	0.00014	0.12	8
23'	4958.69349	90.48948	2.05731	-0.55044	0.04491	-0.03752	-0.00166	0.00099	0.00014	0.14	9
24'	4960.37141	90.57331	2.05994	-0.55127	0.04499	-0.03759	-0.00166	0.00100	0.00014	0.16	11
25'	4962.05089	90.65725	2.06258	-0.55211	0.04506	-0.03766	-0.00167	0.00100	0.00014	0.18	12
26'	4963.73193	90.74129	2.06523	-0.55294	0.04514	-0.03773	-0.00167	0.00100	0.00014	0.20	13
27'	4965.41453	90.82542	2.06788	-0.55378	0.04522	-0.03780	-0.00167	0.00100	0.00014	0.25	15
28'	4967.09870	90.90966	2.07054	-0.55462	0.04530	-0.03788	-0.00168	0.00100	0.00014	0.30	16
29'	4968.78444	90.99400	2.07320	-0.55546	0.04538	-0.03795	-0.00168	0.00101	0.00014	0.35	18
30'	4970.47174	91.07844	2.07586	-0.55630	0.04545	-0.03802	-0.00169	0.00101	0.00014	0.40	19
31'	4972.16062	91.16299	2.07853	-0.55715	0.04553	-0.03809	-0.00169	0.00101	0.00014	0.50	20
32'	4973.85107	91.24763	2.08120	-0.55799	0.04561	-0.03816	-0.00169	0.00101	0.00014	0.60	19
33'	4975.54309	91.33238	2.08388	-0.55884	0.04569	-0.03823	-0.00170	0.00102	0.00014	0.65	18
34'	4977.23669	91.41723	2.08656	-0.55969	0.04577	-0.03830	-0.00170	0.00102	0.00014	0.70	16
35'	4978.93187	91.50218	2.08925	-0.56054	0.04585	-0.03838	-0.00171	0.00102	0.00014	0.75	15
36'	4980.62863	91.58724	2.09194	-0.56139	0.04592	-0.03845	-0.00171	0.00102	0.00014	0.80	13
37'	4982.32697	91.67239	2.09464	-0.56224	0.04600	-0.03852	-0.00171	0.00102	0.00014	0.82	12
38'	4984.02690	91.75765	2.09734	-0.56310	0.04608	-0.03859	-0.00172	0.00103	0.00014	0.84	11
39'	4985.72841	91.84301	2.10004	-0.56395	0.04616	-0.03866	-0.00172	0.00103	0.00014	0.86	9
40'	4987.43151	91.92848	2.10275	-0.56481	0.04624	-0.03874	-0.00173	0.00103	0.00014	0.88	8
41'	4989.13620	92.01405	2.10546	-0.56567	0.04632	-0.03881	-0.00173	0.00103	0.00014	0.90	7
42'	4990.84249	92.09972	2.10818	-0.56653	0.04640	-0.03888	-0.00173	0.00103	0.00014	0.91	6
43'	4992.55036	92.18550	2.11090	-0.56739	0.04648	-0.03896	-0.00174	0.00104	0.00014	0.92	6
44'	4994.25983	92.27138	2.11363	-0.56825	0.04656	-0.03903	-0.00174	0.00104	0.00014	0.93	5
45'	4995.97090	92.35736	2.11636	-0.56912	0.04664	-0.03910	-0.00174	0.00104	0.00014	0.94	4
46'	4997.68357	92.44345	2.11910	-0.56998	0.04672	-0.03918	-0.00175	0.00104	0.00014	0.95	4
47'	4999.39784	92.52964	2.12184	-0.57085	0.04680	-0.03925	-0.00175	0.00105	0.00015	0.96	3
48	5001.11372	92.61594	2.12459	-0.57172	0.04689	-0.03932	-0.00176	0.00105	0.00015	0.97	2
49'	5002.83119	92.70234	2.12734	-0.57259	0.04697	-0.03940	-0.00176	0.00105	0.00015	0.98	2
50'	5004.55028	92.78884	2.13010	-0.57346	0.04705	-0.03947	-0.00177	0.00105	0.00015	0.99	1
51'	5006.27098	92.87546	2.13286	-0.57434	0.04713	-0.03955	-0.00177	0.00106	0.00015		
52'	5007.99329	92.96217	2.13562	-0.57521	0.04721	-0.03962	-0.00177	0.00106	0.00015		
53'	5009.71721	93.04900	2.13839	-0.57609	0.04729	-0.03970	-0.00178	0.00106	0.00015		
54'	5011.44274	93.13592	2.14116	-0.57697	0.04738	-0.03977	-0.00178	0.00106	0.00015		
55'	5013.16990	93.22296	2.14394	-0.57785	0.04746	-0.03985	-0.00179	0.00106	0.00015		
56'	5014.89867	93.31010	2.14673	-0.57873	0.04754	-0.03992	-0.00179	0.00107	0.00015		
57'	5016.62906	93.39734	2.14951	-0.57961	0.04762	-0.04000	-0.00179	0.00107	0.00015		
58'	5018.36108	93.48470	2.15231	-0.58049	0.04771	-0.04007	-0.00180	0.00107	0.00015		
59'	5020.09472	93.57215	2.15511	-0.58138	0.04779	-0.04015	-0.00180	0.00107	0.00015		
60'	5021.82999	93.65972	2.15791	-0.58227	0.04787	-0.04022	-0.00181	0.00108	0.00015		

Przyrost szerokości geograficznej $\Delta\varphi$

$\Delta\varphi'' = (x) + (y^2)y + (x\,y^2)xy^2 + \ldots$ gdzie x - Sasa A y - Sin A. S długość linji geodezyjnej wyrażona w setkach kilometrów
A azymut linji geodezyjnej w punkcie wyjściowym.

φ 50°	(x)	(y^2)	(xy^2)	(x^2)	(x^2y^2)	(y^4)	(x^3)	(xy^4)	(x^3y^2)
0'	3236. 93165	-30. 18522	- 0. 69077	-0. 25140	-0.01543	0.00324	0. 00046	0. 00022	-0. 00035
1'	3236. 92233	-30 20294	- 0. 69143	-0. 25138	-0. 01545	0. 00325	0. 00046	0. 00022	-0. 00036
2'	3236. 91301	-30. 22068	- 0. 69210	-0. 25135	-0. 01547	0. 00325	0. 00047	0. 00022	-0. 00035
3'	3236. 90369	-30. 23843	- 0. 69278	-0. 25132	-0. 01549	0. 00326	0. 00047	0. 00022	-0. 00035
4'	3236. 89438	-30. 25618	- 0. 69348	-0. 25130	-0. 01551	0. 00326	0. 00047	0. 00022	-0. 00035
5'	3236. 88506	-30. 27396	- 0. 69408	-0. 25127	-0. 01554	0. 00327	0. 00047	0. 00022	-0. 00035
6'	3236. 87575	-30. 29174	- 0. 69475	-0. 25124	-0. 01556	0. 00327	0. 00047	0. 00022	-0. 00035
7'	3236. 86643	-30. 30954	- 0. 69541	-0. 25121	-0. 01558	0. 00328	0. 00047	0. 00022	-0. 00036
8'	3236. 86712	-30. 32734	- 0. 69608	-0. 25119	-0. 01560	0. 00328	0. 00047	0. 00022	-0. 00035
9'	3236. 84781	-30. 34516	- 0. 69674	-0. 25116	-0. 01562	0. 00329	0. 00048	0. 00022	-0. 00035
10'	3236. 83850	-30. 36300	- 0. 69741	-0. 25113	-0. 01564	0. 00329	0. 00048	0. 00022	-0. 00035
11'	3236. 82919	-30. 38084	- 0. 69808	-0. 25110	-0. 01567	0. 00330	0. 00048	0. 00022	-0. 00036
12'	3236. 81988	-30. 39870	- 0. 69875	-0. 25108	-0. 01569	0. 00330	0. 00048	0. 00022	-0. 00035
13'	3236. 81057	-30. 41657	- 0. 69942	-0. 25105	-0. 01571	0. 00331	0. 00048	0. 00022	-0. 00035
14'	3236. 80126	-30. 43445	- 0. 70009	-0. 25102	-0. 01573	0. 00331	0. 00048	0. 00022	-0. 00036
15'	3236. 79196	-30. 45235	- 0. 70076	-0. 25099	-0. 01575	0. 00332	0. 00049	0. 00022	-0. 00036
16'	3236. 78265	-30. 47026	- 0. 70143	-0. 25096	-0. 01578	0. 00332	0. 00049	0. 00022	-0. 00036
17'	3236. 77335	-30. 48818	- 0. 70211	-0. 25094	-0. 01580	0. 00333	0. 00049	0. 00022	-0. 00036
18'	3236. 76405	-30. 50611	- 0. 70278	-0. 25091	-0. 01582	0. 00333	0. 00049	0. 00023	-0. 00036
19'	3236. 75475	-30. 52406	- 0. 70346	-0. 25088	-0. 01584	0. 00334	0. 00049	0. 00023	-0. 00036
20'	3236. 74545	-30. 54201	- 0. 70413	-0. 25085	-0. 01586	0. 00334	0. 00049	0. 00023	-0. 00036
21'	3236. 73615	-30. 55998	- 0. 70481	-0. 25082	-0. 01589	0. 00335	0. 00049	0. 00023	-0. 00036
22'	3236. 72685	-30. 57797	- 0. 70549	-0. 25079	-0. 01591	0. 00335	0. 00050	0. 00023	-0. 00036
23'	3236. 71755	-30. 59596	- 0. 70617	-0. 25077	-0. 01593	0. 00336	0. 00050	0. 00023	-0. 00036
24'	3236. 70825	-30. 61397	- 0. 70684	-0. 25074	-0. 01595	0. 00336	0. 00050	0. 00023	-0. 00036
25'	3236. 69896	-30. 63199	- 0. 70753	-0. 25071	-0. 01598	0. 00337	0. 00050	0. 00023	-0. 00036
26'	3236. 68966	-30. 65002	- 0. 70821	-0. 25068	-0. 01600	0. 00337	0. 00050	0. 00023	-0. 00036
27'	3236. 68037	-30. 66807	- 0. 70889	-0. 25065	-0. 01602	0. 00338	0. 00050	0. 00023	-0. 00036
28'	3236. 67108	-30. 68613	- 0. 70957	-0. 25062	-0. 01604	0. 00338	0. 00051	0. 00023	-0. 00036
29'	3236. 66179	-30. 70420	- 0. 71026	-0. 25059	-0. 01607	0. 00339	0. 00051	0. 00023	-0. 00037
30'	3236. 65250	-30. 72228	- 0. 71094	-0. 25056	-0. 01609	0. 00340	0. 00051	0. 00023	-0. 00037
31'	3236. 64321	-30. 74038	- 0. 71163	-0. 25053	-0. 01611	0. 00340	0. 00051	0. 00023	-0. 00037
32'	3236. 63392	-30. 75849	- 0. 71231	-0. 25050	-0. 01613	0. 00341	0. 00051	0. 00023	-0. 00037
33'	3236. 62463	-30. 77661	- 0. 71300	-0. 25047	-0. 01616	0. 00341	0. 00051	0. 00023	-0. 00037
34'	3236. 61535	-30. 79475	- 0. 71369	-0. 25044	-0. 01618	0. 00342	0. 00051	0. 00023	-0. 00037
35'	3236. 60606	-30. 81289	- 0. 71438	-0. 25042	-0. 01620	0. 00342	0. 00052	0. 00023	-0. 00037
36'	3236. 59678	-30. 83106	- 0. 71507	-0. 25039	-0. 01622	0. 00343	0. 00052	0. 00023	-0. 00037
37'	3236. 58749	-30. 84923	- 0. 71576	-0. 25036	-0. 01625	0. 00343	0. 00052	0. 00023	-0. 00037
38'	3236. 57821	-30. 86742	- 0. 71645	-0. 25033	-0. 01627	0. 00344	0. 00052	0. 00023	-0. 00037
39'	3236. 56893	-30. 88561	- 0. 71715	-0. 25029	-0. 01629	0. 00344	0. 00052	0. 00023	-0. 00037
40'	3236. 55965	-30. 90383	- 0. 71784	-0. 25026	-0. 01632	0. 00345	0. 00052	0. 00024	-0. 00037
41'	3236. 55037	-30. 92205	- 0. 71853	-0. 25023	-0. 01634	0. 00345	0. 00052	0. 00024	-0. 00037
42'	3236. 54110	-30. 94029	- 0. 71923	-0. 25020	-0. 01636	0. 00346	0. 00053	0. 00024	-0. 00037
43'	3236. 53182	-30. 95854	- 0. 71993	-0. 25017	-0. 01638	0. 00346	0. 00053	0. 00024	-0. 00037
44'	3236. 52255	-30. 97680	- 0. 72062	-0. 25014	-0. 01641	0. 00347	0. 00053	0. 00024	-0. 00038
45'	3236. 51327	-30. 99508	- 0. 72132	-0. 25011	-0. 01643	0. 00348	0. 00053	0. 00024	-0. 00038
46'	3236. 50400	-31. 01337	- 0. 72202	-0. 25008	-0. 01645	0. 00348	0. 00053	0. 00024	-0. 00038
47'	3236. 49473	-31. 03167	- 0. 72272	-0. 25005	-0. 01648	0. 00349	0. 00053	0. 00024	-0. 00038
48'	3236. 48546	-31. 04999	- 0. 72342	-0. 25002	-0. 01650	0. 00349	0. 00054	0. 00024	-0. 00038
49'	3236. 47619	-31. 06832	- 0. 72413	-0. 24999	-0. 01652	0. 00350	0. 00054	0. 00024	-0. 00038
50'	3236. 46692	-31. 08666	- 0. 72483	-0. 24996	-0. 01655	0. 00350	0. 00054	0. 00024	-0. 00038
51'	3236. 45765	-31. 10501	- 0. 72553	-0. 24993	-0. 01657	0. 00351	0. 00054	0. 00024	-0. 00038
52'	3236. 44839	-31. 12338	- 0. 72624	-0. 24990	-0. 01659	0. 00351	0. 00054	0. 00024	-0. 00038
53'	3236. 43912	-31. 14176	- 0. 72694	-0. 24987	-0. 01662	0. 00352	0. 00054	0. 00024	-0. 00038
54'	3236. 42986	-31. 16016	- 0. 72765	-0. 24983	-0. 01664	0. 00352	0. 00054	0. 00024	-0. 00038
55'	3236. 42059	-31. 17856	- 0. 72836	-0. 24980	-0. 01666	0. 00353	0. 00055	0. 00024	-0. 00038
56'	3236. 41133	-31. 19698	- 0. 72907	-0. 24977	-0. 01669	0. 00354	0. 00055	0. 00024	-0. 00038
57'	3236. 40207	-31. 21542	- 0. 72978	-0. 24974	-0. 01671	0. 00354	0. 00055	0. 00024	-0. 00038
58'	3236. 39281	-31. 23386	- 0. 73049	-0. 24971	-0. 01674	0. 00355	0. 00055	0. 00024	-0. 00039
59'	3236. 38355	-31. 25232	- 0. 73120	-0. 24968	-0. 01676	0. 00355	0. 00055	0. 00024	-0. 00039
60'	3236. 37430	-31. 27080	- 0. 73191	-0. 24964	-0. 01678	0. 00356	0. 00055	0. 00024	-0. 00039

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda'' = (y) + (xy) + (x^2y) + (y^3) + (x^3y) + (xy^3) + (x^2y^3) + (x^4y) + (y^5)$ ... gdzie $x = S\cos A$ $y = S\sin A$

S długość linji geodezyjnej wyrażona w setkach kilometrów
A azymut linji geodezyjnej w punkcie wyjściowym

φ 50	(y)	(xy)	(x^2y)	(y^3)	(x^3y)	(xy^3)	(x^2y^3)	(x^4y)	(y^5)	Poprawka interpolacyjna dla wyrazu (y) K'	P
0°	5021. 82999	93. 65972	2. 15791	-0. 58227	0. 04787	-0. 04022	-0. 00181	0. 00108	0. 00015		
1'	5023. 56684	93. 74739	2. 16072	-0. 58316	0. 04795	-0. 04030	-0. 00181	0. 00108	0. 00015		
2'	5025. 30541	93 83517	2. 16353	-0. 58405	0. 04804	-0. 04038	-0. 00181	0. 00108	0. 00015		
3'	5027. 04458	93. 92306	2 16634	-0. 58494	0. 04812	-0. 04045	-0. 00182	0. 00108	0. 00015		
4'	5028. 78437	94. 01105	2. 16917	-0. 58583	0. 04821	-0. 04053	-0. 00182	0. 00108	0. 00015		1
5'	5030. 53081	94. 09915	2. 17199	-0. 58673	0. 04829	-0. 04061	-0. 00183	0. 00109	0. 00015		0000
6'	5032. 27588	94. 18736	2. 17482	-0. 58762	0. 04837	-0. 04069	-0. 00183	0. 00109	0. 00015		
7'	5034. 02260	94. 27568	2. 17766	-0. 58852	0. 04846	-0. 04076	-0. 00184	0. 00109	0. 00015	0.01	1
8'	5035. 77095	94 36410	2. 18050	-0. 58942	0. 04854	-0. 04084	-0. 00184	0. 00109	0. 00015	0.02	2
9'	5037. 52096	94 45263	2. 18335	-0. 59032	0. 04863	-0. 04092	-0. 00184	0. 00110	0. 00015	0.03	2
10'	5039. 27261	94. 54128	2. 18620	-0. 59123	0. 04871	-0. 04099	-0. 00185	0. 00110	0. 00015	0.04	3
11'	5041. 02591	94 63003	2. 18905	-0. 59213	0 04880	-0 04107	-0. 00185	0. 00110	0. 00015	0.05	4
12'	5042. 78086	94. 71889	2 19191	-0. 59304	0. 04888	-0. 04115	-0. 00186	0. 00110	0. 00015	0.06	5
13'	5044. 53746	94. 80785	2. 19478	-0. 59394	0. 04897	-0. 04123	-0. 00186	0. 00111	0. 00015	0.07	5
14	5046. 29572	94. 89693	2 19765	-0 59485	0 04905	-0. 04131	-0. 00187	0. 00111	0. 00015	0.08	6
15'	5048. 05564	94. 98612	2. 20052	-0. 59576	0 04914	-0. 04138	-0 00187	0. 00111	0. 00016	0.09	7
16	5049. 81721	95.07541	2. 20340	-0 59668	0 04923	-0 04146	-0. 00187	0. 00111	0. 00016	0.10	8
17'	5051. 58045	95. 16482	2. 20629	-0 59759	0 04931	-0 04154	-0 00188	0. 00112	0. 00016	0.12	9
18'	5053. 34535	95. 25434	2. 20918	-0. 59851	0. 04940	-0. 04162	-0. 00188	0. 00112	0. 00016	0.14	10
19	5055. 11191	95. 34396	2. 21207	-0 59942	0. 04948	-0. 04170	-0 00189	0. 00112	0. 00016	0.16	11
20'	5056. 88015	95. 43370	2. 21497	-0. 60034	0. 04957	-0. 04178	-0 00189	0. 00112	0. 00016	0.18	12
21'	5058 65005	95. 52355	2. 21788	-0 60126	0. 04966	-0 04186	-0 00190	0. 00113	0 00016	0.20	14
22	5060. 42163	95. 61350	2. 22079	-0 60218	0 04974	-0 04194	-0 00190	0. 00113	0. 00016	0.22	15
23'	5062. 19487	95. 70357	2. 22370	-0 60311	0 04983	-0. 04202	-0. 00190	0. 00113	0 00016	0.24	15
24'	5063. 96980	95. 79375	2. 22662	-0. 60403	0. 04992	-0 04210	-0 00191	0. 00113	0. 00016	0.26	16
25	5065 74640	95. 88404	2. 22955	0. 60496	0 05001	-0. 04218	-0. 00191	0. 00114	0. 00016	0.28	17
26	5067. 52468	95. 97445	2 23248	-0. 60589	0. 05009	-0. 04226	-0. 00192	0. 00114	0. 00016	0.30	18
27	5069. 30464	96 06496	2 23541	-0 60682	0. 05018	-0. 04234	-0 00192	0. 00114	0. 00016	0.35	19
28	5071. 08629	96 15559	2. 23835	-0 60775	0. 05027	-0. 04242	-0 00193	0. 00114	0. 00016	0.40	20
29	5072. 86963	96. 24632	2. 24130	-0. 60868	0. 05036	-0 04250	-0 00193	0. 00115	0. 00016	0.45	21
30	5074 65465	96. 33717	2. 24425	-0. 60962	0. 05045	-0. 04258	-0 00194	0. 00115	0. 00016	0.50	21
31	5076. 44136	96. 42814	2. 24720	-0. 61056	0. 05054	-0. 04266	-0. 00194	0. 00115	0. 00016	0.55	21
32	5078. 22977	96. 51921	2 25016	-0. 61150	0. 05063	-0. 04275	-0 00194	0. 00115	0. 00016	0.60	20
33	5080. 01987	96. 61040	2. 25313	-0. 61244	0. 05071	-0 04283	-0 00195	0. 00116	0. 00016	0.65	19
34	5081. 81166	96. 70170	2 25610	-0. 61338	0 05080	-0. 04291	-0. 00195	0. 00116	0 00016	0.70	18
35	5083. 60516	96. 79312	2. 25907	-0. 61432	0 05089	-0. 04299	-0. 00196	0. 00116	0. 00016	0.72	17
36	5085. 40035	96 88464	2. 26205	-0. 61527	0. 05098	-0. 04307	0 00196	0. 00116	0. 00016	0.74	16
37	5087. 19725	96 97628	2. 26504	-0. 61621	0. 05107	-0 04316	-0 00197	0. 00117	0. 00016	0.76	15
38	5088. 99585	97 06804	2 26803	-0. 61716	0 05116	-0 04324	0. 00197	0. 00117	0. 00016	0.78	15
39	5090. 79617	97. 15991	2.27102	-0. 61811	0. 05125	-0. 04332	-0. 00198	0. 00117	0. 00016	0.80	14
40	5092. 59819	97. 25189	2. 27403	-0. 61906	0 05134	-0. 04340	-0. 00198	0. 00117	0. 00017	0.82	12
41	5094. 40192	97. 34399	2. 27703	0. 62002	0 05143	0. 04349	0 00199	0. 00118	0. 00017	0.84	11
42	5096. 20736	97. 43620	2. 28004	-0. 62097	0 05153	0. 04357	-0. 00199	0. 00118	0. 00017	0.86	10
43	5098. 01452	97. 52853	2. 28306	-0. 62193	0 05162	0. 04365	-0. 00200	0. 00118	0. 00017	0.88	9
44	5099. 82340	97. 62097	2. 28608	-0. 62289	0 05171	0. 04374	-0. 00200	0. 00118	0. 00017	0.90	8
45°	5101. 63400	97. 71352	2. 28911	-0. 62385	0. 05180	0. 04382	-0. 00200	0. 00119	0. 00017	0.91	7
46	5103. 44612	97. 80620	2. 29214	-0. 62481	0. 05189	-0. 04391	-0. 00201	0. 00119	0. 00017	0.92	6
47	5105. 26037	97. 89898	2. 29518	-0. 62577	0. 05198	-0. 04399	-0. 00201	0. 00119	0. 00017	0.93	5
48	5107. 07614	97. 99189	2. 29822	-0. 62674	0. 05207	-0. 04408	-0. 00202	0. 00119	0. 00017	0.94	5
49	5108. 89364	98. 08491	2. 30127	-0. 62771	0. 05217	-0. 04416	-0. 00202	0. 00120	0. 00017	0.95	4
50°	5110. 71287	98. 17804	2. 30433	-0. 62867	0. 05226	-0. 04425	-0. 00203	0. 00120	0. 00017	0.96	3
51'	5112. 53383	98. 27129	2. 30738	-0. 62965	0. 05235	0. 04433	0. 00203	0. 00120	0. 00017	0.97	2
52'	5114. 35653	98. 36466	2. 31045	-0. 63062	0. 05244	-0. 04442	-0. 00204	0. 00120	0. 00017	0.98	2
53'	5116. 18097	98 45815	2. 31352	-0. 63159	0. 05254	0. 04450	-0. 00204	0. 00121	0. 00017	0.99	1
54'	5118. 00714	98. 55175	2. 31659	-0. 63257	0. 05263	0. 04459	-0. 00205	0. 00121	0. 00017		
55'	5119. 83506	98. 64547	2. 31967	-0. 63354	0. 05272	0. 04467	0. 00205	0. 00121	0. 00017		
56'	5121. 66472	98 73930	2. 32276	-0. 63452	0. 05282	-0. 04476	-0. 00206	0. 00121	0. 00017		
57'	5123. 49612	98. 83326	2. 32585	-0. 63550	0. 05291	-0. 04484	-0. 00206	0. 00122	0. 00017		
58'	5125. 32928	98 92733	2. 32894	-0. 63649	0. 05301	-0. 04493	-0. 00207	0. 00122	0. 00017		
59	5127. 16418	99. 02152	2. 33204	-0. 63747	0. 05310	-0. 04502	-0. 00207	0. 00123	0. 00017		
60	5129. 00084	99. 11582	2. 33514	-0. 63846	0. 05319	-0. 04510	-0. 00208	0. 00123	0. 00017		

A. K.

1 Przyrost szerokości geograficznej $\Delta\varphi$

$\Delta\varphi'' = (x)X + (y^2)Y^2 + (xy^2)XY^2 + \ldots$ gdzie $X = S\cos A$ $Y = S\sin A$

S długość linii geodezyjnej wyrażona w setkach kilometrów
A azymut linii geodezyjnej w punkcie wyjściowym

φ 51°	(x)	(y^2)	(xy^2)	(x^2)	(x^2y^2)	(y^4)	(x^3)	(xy^4)	(x^3y^2)
0'	3236.37430	-31.27080	-0.73191	-0.24964	-0.01678	0.00356	0.00055	0.00024	-0.00039
1'	3236.36504	-31.28928	-0.73262	-0.24961	-0.01681	0.00356	0.00056	0.00025	-0.00039
2'	3236.35579	-31.30778	-0.73334	-0.24958	-0.01683	0.00357	0.00056	0.00025	-0.00039
3'	3236.34653	-31.32630	-0.73405	-0.24955	-0.01685	0.00357	0.00056	0.00025	-0.00039
4'	3236.33728	-31.34482	-0.73477	-0.24952	-0.01688	0.00358	0.00056	0.00025	-0.00039
5'	3236.32803	-31.36336	-0.73549	-0.24949	-0.01690	0.00359	0.00056	0.00025	-0.00039
6'	3236.31878	-31.38192	-0.73620	-0.24945	-0.01693	0.00359	0.00056	0.00025	-0.00039
7'	3236.30953	-31.40048	-0.73692	-0.24942	-0.01695	0.00360	0.00056	0.00025	-0.00039
8'	3236.30028	-31.41906	-0.73764	-0.24939	-0.01697	0.00360	0.00057	0.00025	-0.00039
9	3236.29104	-31.43766	-0.73836	-0.24936	-0.01700	0.00361	0.00057	0.00025	-0.00039
10'	3236.28179	-31.45626	-0.73909	-0.24932	-0.01702	0.00361	0.00057	0.00025	-0.00039
11'	3236.27255	-31.47488	-0.73981	-0.24929	-0.01705	0.00362	0.00057	0.00025	-0.00039
12'	3236.26330	-31.49352	-0.74053	-0.24926	-0.01707	0.00363	0.00057	0.00025	-0.00040
13'	3236.25406	-31.51216	-0.74126	-0.24922	-0.01710	0.00363	0.00057	0.00025	-0.00040
14'	3236.24482	-31.53082	-0.74198	-0.24919	-0.01712	0.00364	0.00057	0.00025	-0.00040
15'	3236.23558	-31.54950	-0.74271	-0.24916	-0.01714	0.00364	0.00058	0.00025	-0.00040
16	3236.22634	-31.56818	-0.74344	-0.24913	-0.01717	0.00365	0.00058	0.00025	-0.00040
17'	3236.21711	-31.58688	-0.74416	-0.24909	-0.01719	0.00365	0.00058	0.00025	-0.00040
18'	3236.20787	-31.60560	-0.74489	-0.24906	-0.01722	0.00366	0.00058	0.00025	-0.00040
19'	3236.19864	-31.62432	-0.74562	-0.24903	-0.01724	0.00367	0.00058	0.00025	-0.00040
20'	3236.18940	-31.64307	-0.74636	-0.24899	-0.01727	0.00367	0.00058	0.00025	-0.00040
21'	3236.18017	-31.66182	-0.74709	-0.24896	-0.01729	0.00368	0.00059	0.00026	-0.00040
22'	3236.17094	-31.68059	-0.74782	-0.24892	-0.01732	0.00368	0.00059	0.00026	-0.00040
23'	3236.16171	-31.69937	-0.74856	-0.24889	-0.01734	0.00369	0.00059	0.00026	-0.00040
24'	3236.15248	-31.71817	-0.74929	-0.24886	-0.01737	0.00369	0.00059	0.00026	-0.00040
25'	3236.14325	-31.73698	-0.75003	-0.24882	-0.01739	0.00370	0.00059	0.00026	-0.00040
26'	3236.13403	-31.75580	-0.75077	-0.24879	-0.01742	0.00371	0.00059	0.00026	-0.00041
27'	3236.12480	-31.77464	-0.75150	-0.24876	-0.01744	0.00371	0.00059	0.00026	-0.00041
28'	3236.11558	-31.79349	-0.75224	-0.24872	-0.01747	0.00372	0.00060	0.00026	-0.00041
29	3236.10636	-31.81235	-0.75298	-0.24869	-0.01749	0.00372	0.00060	0.00026	-0.00041
30'	3236.09714	-31.83123	-0.75372	-0.24865	-0.01752	0.00373	0.00060	0.00026	-0.00041
31'	3236.08792	-31.85012	-0.75447	-0.24862	-0.01754	0.00374	0.00060	0.00026	-0.00041
32'	3236.07870	-31.86903	-0.75521	-0.24858	-0.01757	0.00374	0.00060	0.00026	-0.00041
33'	3236.06948	-31.88794	-0.75595	-0.24855	-0.01759	0.00375	0.00060	0.00026	-0.00041
34'	3236.06026	-31.90688	-0.75670	-0.24851	-0.01762	0.00375	0.00060	0.00026	-0.00041
35'	3236.05105	-31.92583	-0.75745	-0.24848	-0.01764	0.00376	0.00061	0.00026	-0.00041
36'	3236.04184	-31.94479	-0.75819	-0.24845	-0.01767	0.00376	0.00061	0.00026	-0.00041
37'	3236.03262	-31.96376	-0.75894	-0.24841	-0.01769	0.00377	0.00061	0.00026	-0.00041
38'	3236.02341	-31.98275	-0.75969	-0.24838	-0.01772	0.00378	0.00061	0.00026	-0.00041
39'	3236.01420	-32.00175	-0.76044	-0.24834	-0.01774	0.00378	0.00061	0.00026	-0.00042
40	3236.00499	-32.02077	-0.76119	-0.24831	-0.01777	0.00379	0.00061	0.00027	-0.00042
41'	3235.99579	-32.03980	-0.76194	-0.24827	-0.01779	0.00379	0.00062	0.00027	-0.00042
42'	3235.98658	-32.05884	-0.76270	-0.24823	-0.01782	0.00380	0.00062	0.00027	-0.00042
43'	3235.97738	-32.07790	-0.76345	-0.24820	-0.01785	0.00381	0.00062	0.00027	-0.00042
44'	3235.96817	-32.09698	-0.76421	-0.24816	-0.01787	0.00381	0.00062	0.00027	-0.00042
45'	3235.95897	-32.11606	-0.76496	-0.24813	-0.01790	0.00382	0.00062	0.00027	-0.00042
46'	3235.94977	-32.13516	-0.76572	-0.24809	-0.01792	0.00382	0.00062	0.00027	-0.00042
47'	3235.94057	-32.15428	-0.76648	-0.24806	-0.01795	0.00383	0.00062	0.00027	-0.00042
48'	3235.93137	-32.17341	-0.76724	-0.24802	-0.01797	0.00384	0.00063	0.00027	-0.00042
49'	3235.92218	-32.19255	-0.76800	-0.24798	-0.01800	0.00384	0.00063	0.00027	-0.00042
50'	3235.91298	-32.21171	-0.76876	-0.24795	-0.01803	0.00385	0.00063	0.00027	-0.00042
51'	3235.90379	-32.23088	-0.76952	-0.24791	-0.01805	0.00386	0.00063	0.00027	-0.00042
52'	3235.89459	-32.25006	-0.77028	-0.24788	-0.01808	0.00386	0.00063	0.00027	-0.00043
53	3235.88540	-32.26926	-0.77105	-0.24784	-0.01810	0.00387	0.00063	0.00027	-0.00043
54	3235.87621	-32.25847	-0.77181	-0.24780	-0.01813	0.00387	0.00064	0.00027	-0.00043
55'	3235.86702	-32.30770	-0.77258	-0.24777	-0.01816	0.00388	0.00064	0.00027	-0.00043
56	3235.85784	-32.32694	-0.77335	-0.24773	-0.01818	0.00389	0.00064	0.00027	-0.00043
57'	3235.84865	-32.34620	-0.77412	-0.24770	-0.01821	0.00389	0.00064	0.00027	-0.00043
58	3235.83946	-32.36547	-0.77489	-0.24766	-0.01824	0.00390	0.00064	0.00028	-0.00043
59'	3235.83028	-32.38476	-0.77566	-0.24762	-0.01826	0.00390	0.00064	0.00028	-0.00043
60'	3235.82110	-32.40406	-0.77643	-0.24758	-0.01829	0.00391	0.00064	0.00028	-0.00043

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda = (y) y + (xy) xy + (x^2y) x^2y + \ldots$ gdzie $X = S\cos A$ $y = S\sin A$. S długość linii geodezyjnej wyrażona w setkach kilometrów, A azymut linii geodezyjnej w punkcie wyjściowym.

φ 51°	(y)	(xy)	(x^2y)	(y^3)	(xy^3)	(x^3y^3)	(x^2y^3)	(x^4y)	(y^5)	Poprawka interpolacyjna dla wyrazu (y)	
										X'	p_i
0'	5129.00084	99.11582	2.33516	-0.63846	0.05319	-0.04510	-0.00208	0.00123	0.00017		
1'	5130.63925	99.21025	2.33827	-0.63944	0.05329	-0.04519	-0.00208	0.00123	0.00017		
2'	5132.67942	99.30479	2.34139	-0.64043	0.05338	-0.04528	-0.00209	0.00123	0.00018		
3'	5134.52135	99.39946	2.34451	-0.64143	0.05348	-0.04536	-0.00209	0.00123	0.00018		
4'	5136.36504	99.49424	2.34764	-0.64242	0.05357	-0.04545	-0.00210	0.00124	0.00018		$\frac{1}{10000}$
5'	5138.21049	99.58914	2.35077	-0.64341	0.05367	-0.04554	-0.00210	0.00124	0.00018		
6'	5140.05771	99.68416	2.35391	-0.64441	0.05377	-0.04563	-0.00211	0.00124	0.00018		
7'	5141.90669	99.77930	2.35706	-0.64541	0.05386	-0.04572	-0.00211	0.00124	0.00018	0'.01	1
8'	5143.75745	99.87456	2.36021	-0.64641	0.05396	-0.04580	-0.00212	0.00125	0.00018	0'.02	2
9'	5145.60998	99.96994	2.36336	-0.64741	0.05405	-0.04589	-0.00212	0.00125	0.00018	0'.03	3
10'	5147.46428	100.06544	2.36653	-0.64842	0.05415	-0.04598	-0.00213	0.00125	0.00018	0'.04	4
11'	5149.32037	100.16106	2.36969	-0.64942	0.05425	-0.04607	-0.00213	0.00126	0.00018	0'.05	4
12'	5151.17823	100.25680	2.37287	-0.65043	0.05434	-0.04616	-0.00214	0.00126	0.00018	0'.06	5
13'	5153.03787	100.35266	2.37604	-0.65144	0.05444	-0.04625	-0.00214	0.00126	0.00018	0'.07	6
14'	5154.89930	100.44865	2.37923	-0.65245	0.05454	-0.04634	-0.00215	0.00126	0.00018	0'.08	7
15'	5156.76251	100.54475	2.38242	-0.65346	0.05464	-0.04643	-0.00215	0.00127	0.00018	0'.09	7
16'	5158.62751	100.64098	2.38561	-0.65448	0.05473	-0.04652	-0.00216	0.00127	0.00018	0'.10	8
17'	5160.49430	100.73732	2.38881	-0.65549	0.05483	-0.04661	-0.00216	0.00127	0.00018	0'.12	10
18'	5162.36288	100.83379	2.39202	-0.65651	0.05493	-0.04670	-0.00217	0.00127	0.00018	0'.14	11
19'	5164.23326	100.93038	2.39523	-0.65753	0.05503	-0.04679	-0.00217	0.00128	0.00018	0'.16	12
20'	5166.10544	101.02710	2.39845	-0.65855	0.05513	-0.04688	-0.00218	0.00128	0.00018	0'.18	13
21'	5167.97941	101.12393	2.40167	-0.65958	0.05523	-0.04697	-0.00218	0.00128	0.00018	0'.20	15
22'	5169.85519	101.22089	2.40490	-0.66060	0.05533	-0.04706	-0.00219	0.00129	0.00018	0'.22	16
23'	5171.73277	101.31797	2.40814	-0.66163	0.05543	-0.04716	-0.00219	0.00129	0.00018	0'.24	17
24'	5173.61216	101.41518	2.41138	-0.66266	0.05552	-0.04725	-0.00220	0.00129	0.00018	0'.26	18
25'	5175.49336	101.51251	2.41462	-0.66369	0.05562	-0.04734	-0.00220	0.00129	0.00019	0'.28	18
26'	5177.37637	101.60996	2.41787	-0.66472	0.05572	-0.04743	-0.00221	0.00130	0.00019	0'.30	19
27'	5179.26119	101.70753	2.42113	-0.66576	0.05582	-0.04752	-0.00221	0.00130	0.00019	0'.35	21
28'	5181.14782	101.80523	2.42439	-0.66679	0.05593	-0.04762	-0.00222	0.00130	0.00019	0'.40	22
29'	5183.03628	101.90306	2.42766	-0.66783	0.05603	-0.04771	-0.00222	0.00131	0.00019	0'.45	23
30'	5184.92655	102.00100	2.43094	-0.66887	0.05613	-0.04780	-0.00223	0.00131	0.00019	0'.50	23
31'	5186.81865	102.09908	2.43422	-0.66992	0.05623	-0.04789	-0.00223	0.00131	0.00019	0'.55	23
32'	5188.71257	102.19727	2.43750	-0.67096	0.05633	-0.04799	-0.00224	0.00132	0.00019	0'.60	22
33'	5190.60832	102.29560	2.44080	-0.67201	0.05643	-0.04808	-0.00225	0.00132	0.00019	0'.65	21
34'	5192.50590	102.39404	2.44409	-0.67306	0.05653	-0.04818	-0.00225	0.00132	0.00019	0'.70	19
35'	5194.40531	102.49262	2.44740	-0.67411	0.05663	-0.04827	-0.00226	0.00132	0.00019	0'.72	18
36'	5196.30656	102.59132	2.45071	-0.67516	0.05674	-0.04836	-0.00226	0.00133	0.00019	0'.74	18
37'	5198.20964	102.69014	2.45402	-0.67621	0.05684	-0.04846	-0.00227	0.00133	0.00019	0'.76	17
38'	5200.11456	102.78908	2.45734	-0.67727	0.05694	-0.04855	-0.00227	0.00133	0.00019	0'.78	16
39'	5202.02132	102.88817	2.46067	-0.67832	0.05704	-0.04865	-0.00228	0.00134	0.00019	0'.80	15
40'	5203.92993	102.98738	2.46400	-0.67938	0.05715	-0.04874	-0.00228	0.00134	0.00019	0'.82	13
41'	5205.84038	103.08671	2.46734	-0.68045	0.05725	-0.04884	-0.00229	0.00134	0.00019	0'.84	12
42'	5207.75268	103.18617	2.47069	-0.68151	0.05735	-0.04893	-0.00229	0.00134	0.00019	0'.86	11
43'	5209.66683	103.28575	2.47404	-0.68257	0.05746	-0.04903	-0.00230	0.00135	0.00019	0'.88	10
44'	5211.58284	103.38547	2.47739	-0.68364	0.05756	-0.04912	-0.00230	0.00135	0.00019	0'.90	8
45'	5213.50070	103.48531	2.48076	-0.68471	0.05767	-0.04922	-0.00231	0.00135	0.00020	0'.91	7
46'	5215.42041	103.58528	2.48412	-0.68578	0.05777	-0.04932	-0.00232	0.00136	0.00020	0'.92	7
47'	5217.34199	103.68537	2.48750	-0.68685	0.05788	-0.04941	-0.00232	0.00136	0.00020	0'.93	6
48'	5219.26543	103.78560	2.49088	-0.68793	0.05798	-0.04951	-0.00233	0.00136	0.00020	0'.94	5
49'	5221.19073	103.88595	2.49427	-0.68901	0.05809	-0.04960	-0.00233	0.00137	0.00020	0'.95	4
50'	5223.11791	103.98644	2.49766	-0.69008	0.05819	-0.04970	-0.00234	0.00137	0.00020	0'.96	4
51'	5225.04695	104.08705	2.50106	-0.69117	0.05830	-0.04980	-0.00234	0.00137	0.00020	0'.97	3
52'	5226.97786	104.18779	2.50446	-0.69225	0.05840	-0.04990	-0.00235	0.00138	0.00020	0'.98	2
53'	5228.91065	104.28866	2.50787	-0.69333	0.05851	-0.05000	-0.00235	0.00138	0.00020	0'.99	1
54'	5230.84532	104.38966	2.51129	-0.69442	0.05861	-0.05010	-0.00236	0.00138	0.00020		
55'	5232.78186	104.49079	2.51471	-0.69551	0.05872	-0.05019	-0.00237	0.00138	0.00020		
56'	5234.72029	104.59205	2.51814	-0.69660	0.05883	-0.05029	-0.00237	0.00139	0.00020		
57'	5236.66060	104.69345	2.52158	-0.69769	0.05894	-0.05039	-0.00238	0.00139	0.00020		
58'	5238.60280	104.79497	2.52502	-0.69879	0.05904	-0.05049	-0.00238	0.00139	0.00020		
59'	5240.54689	104.89662	2.52846	-0.69988	0.05915	-0.05059	-0.00239	0.00140	0.00020		
60'	5242.49286	104.99841	2.53192	-0.70098	0.05926	-0.05069	-0.00239	0.00140	0.00020		

A.K.

Przyrost szerokości geograficznej $\Delta\varphi$

1

$\Delta\varphi'' = \textcircled{x} + \textcircled{y^2} y^2 + \textcircled{x^2y^2} x^2y^2 + \ldots$ gdzie $x = S\cos A$ $y = S\sin A$.

S długość linji geodezyjnej wyrażona w setkach kilometrów
A azymut linji geodezyjnej w punkcie wyjściowym

φ.52'	$\textcircled{x}$	$\textcircled{y^2}$	$\textcircled{x^2y^2}$	$\textcircled{x^4}$	$\textcircled{x^2y^2}$	$\textcircled{y^4}$	$\textcircled{x^3}$	$\textcircled{xy^4}$	$\textcircled{x^3y^2}$
0'	3235. 82110	-32. 40406	-0. 77643	-0. 24756	-0. 01829	0. 00391	0. 00064	0. 00028	-0. 00043
1'	3235. 81192	-32. 42337	-0. 77720	-0. 24755	-0. 01831	0. 00392	0. 00065	0. 00028	-0. 00043
2'	3235. 80274	-32. 44270	-0. 77797	-0. 24751	-0. 01834	0. 00392	0. 00065	0. 00028	-0. 00043
3'	3235. 79356	-32 46 204	-0. 77875	-0. 24747	-0. 01837	0. 00393	0. 00065	0. 00028	-0. 00043
4'	3235. 78438	-32. 48140	-0. 77953	-0. 24744	-0. 01839	0. 00394	0. 00065	0. 00028	-0. 00044
5'	3235. 77521	-32. 50077	-0. 78030	-0. 24740	-0. 01842	0. 00394	0. 00066	0. 00028	-0. 00044
6'	3235. 76603	-32. 52015	-0. 78108	-0. 24736	-0. 01845	0. 00395	0. 00065	0. 00028	-0. 00044
7'	3235. 75686	-32. 53955	-0. 78186	-0. 24732	-0. 01847	0. 00395	0. 00065	0. 00028	-0. 00044
8'	3235. 74769	-32. 55897	-0. 78264	-0. 24729	-0. 01850	0. 00396	0. 00066	0. 00028	-0. 00044
9'	3235. 73852	-32. 57840	-0. 78342	-0. 24725	-0. 01853	0. 00397	0. 00066	0. 00028	-0. 00044
10'	3235. 72935	-32. 59784	-0. 78420	-0. 24721	-0. 01855	0. 00397	0. 00066	0. 00028	-0. 00044
11'	3235. 72018	-32 61730	-0. 78498	-0. 24717	-0. 01858	0. 00398	0. 00066	0. 00028	-0. 00044
12'	3235. 71102	-32. 63677	-0. 78577	-0. 24714	-0. 01861	0. 00399	0. 00066	0. 00028	-0. 00044
13'	3235. 70185	-32. 65626	-0. 78655	-0. 24710	-0. 01864	0. 00399	0. 00066	0. 00028	-0. 00044
14'	3235. 69269	-32. 67576	-0. 78734	-0. 24706	-0. 01866	0. 00400	0. 00066	0. 00028	-0. 00044
15'	3235. 68353	-32. 69528	-0. 78813	-0. 24702	-0. 01869	0. 00401	0. 00067	0. 00028	-0. 00044
16'	3235. 67437	-32 71481	-0. 78892	-0. 24698	-0. 01872	0. 00401	0. 00067	0. 00029	-0. 00045
17'	3235. 66521	-32. 73435	-0. 78971	-0. 24695	-0. 01874	0. 00402	0. 00067	0. 00029	-0. 00045
18'	3235. 65605	-32. 75391	-0. 79050	-0. 24691	-0. 01877	0. 00402	0. 00067	0. 00029	-0. 00045
19'	3235. 64689	-32. 77349	-0. 79129	-0. 24687	-0. 01880	0. 00403	0. 00067	0. 00029	-0. 00045
20'	3235. 63774	-32. 79308	-0. 79208	-0. 24683	-0. 01883	0. 00404	0. 00067	0. 00029	-0. 00045
21'	3235. 62858	-32 81268	-0. 79287	-0. 24679	-0. 01885	0. 00404	0. 00068	0. 00029	-0. 00045
22'	3235. 61943	-32 83230	-0. 79367	-0. 24675	-0. 01888	0. 00405	0. 00068	0. 00029	-0. 00045
23'	3235. 61028	-32. 85194	-0. 79446	-0. 24672	-0. 01891	0. 00406	0. 00068	0. 00029	-0. 00045
24'	3235. 60113	-32. 87158	-0. 79526	-0. 24668	-0. 01894	0. 00406	0. 00068	0. 00029	-0. 00045
25'	3235. 59198	-32. 89125	-0. 79606	-0. 24664	-0. 01896	0. 00407	0. 00068	0. 00029	-0. 00045
26'	3235. 58284	-32. 91093	-0. 79686	-0. 24660	-0. 01899	0. 00408	0. 00068	0. 00029	-0. 00045
27'	3235. 57369	-32. 93062	-0. 79766	-0. 24656	-0. 01902	0. 00408	0. 00068	0. 00029	-0. 00045
28'	3235. 56455	-32 95033	-0. 79846	-0. 24652	-0. 01905	0. 00409	0. 00069	0. 00029	-0. 00046
29'	3235. 55541	-32. 97005	-0. 79926	-0. 24648	-0. 01908	0. 00410	0. 00069	0. 00029	-0. 00046
30'	3235. 54627	-32. 98979	-0. 80007	-0. 24644	-0. 01910	0. 00410	0. 00069	0. 00029	-0. 00046
31'	3235. 53713	-33 00954	-0. 80087	-0. 24640	-0. 01913	0. 00411	0. 00069	0. 00029	-0. 00046
32'	3235. 52799	-33. 02931	-0. 80168	-0. 24636	-0. 01916	0. 00412	0. 00069	0. 00030	-0. 00046
33'	3235. 51885	-33. 04909	-0. 80248	-0. 24632	-0. 01919	0. 00412	0. 00069	0. 00030	-0. 00046
34'	3235. 50972	-33. 06889	-0. 80329	-0. 24628	-0. 01922	0. 00413	0. 00069	0. 00030	-0. 00046
35'	3235. 50058	-33 08870	-0. 80410	-0. 24624	-0. 01924	0. 00414	0. 00070	0. 00030	-0. 00046
36'	3235. 49145	-33. 10853	-0. 80491	-0. 24620	-0. 01927	0. 00414	0. 00070	0. 00030	-0. 00046
37'	3235. 48232	-33. 12838	-0. 80572	-0. 24616	-0. 01930	0. 00415	0. 00070	0. 00030	-0. 00046
38'	3235. 47319	-33. 14823	-0. 80653	-0. 24612	-0. 01933	0. 00416	0. 00070	0. 00030	-0. 00046
39'	3235. 46407	-33. 16811	-0. 80735	-0. 24608	-0. 01936	0. 00416	0. 00070	0. 00030	-0. 00047
40'	3235. 45494	-33. 18800	-0. 80816	-0. 24604	-0. 01938	0. 00417	0. 00070	0. 00030	-0. 00047
41'	3235. 44581	-33. 20790	-0. 80898	-0. 24600	-0. 01941	0. 00418	0. 00071	0. 00030	-0. 00047
42'	3235. 43669	-33. 22782	-0. 80980	-0. 24596	-0. 01944	0. 00418	0. 00071	0. 00030	-0. 00047
43'	3235. 42757	-33. 24775	-0. 81061	-0. 24592	-0. 01947	0. 00419	0. 00071	0. 00030	-0. 00047
44'	3235. 41845	-33. 26770	-0. 81143	-0. 24588	-0. 01950	0. 00420	0. 00071	0. 00030	-0. 00047
45'	3235. 40933	-33. 28767	-0. 81225	-0. 24584	-0. 01953	0. 00420	0. 00071	0. 00030	-0. 00047
46'	3235. 40021	-33. 30764	-0. 81307	-0. 24580	-0. 01956	0. 00421	0. 00071	0. 00030	-0. 00047
47'	3235. 39110	-33. 32764	-0. 81390	-0. 24576	-0. 01959	0. 00422	0. 00071	0. 00030	-0. 00047
48'	3235. 38198	-33. 34765	-0. 81472	-0. 24572	-0. 01961	0. 00422	0. 00072	0. 00030	-0. 00047
49'	3235. 37287	-33. 36767	-0. 81555	-0. 24568	-0. 01964	0. 00423	0. 00072	0. 00031	-0. 00047
50'	3235. 36376	-33. 38772	-0. 81637	-0. 24564	-0. 01967	0. 00424	0. 00072	0. 00031	-0. 00048
51'	3235. 35465	-33. 40777	-0. 81720	-0. 24560	-0. 01970	0. 00424	0. 00072	0. 00031	-0. 00048
52'	3235. 34554	-33. 42784	-0. 81803	-0. 24556	-0. 01973	0. 00425	0. 00072	0. 00031	-0. 00048
53'	3235. 33643	-33 44793	-0. 81886	-0. 24551	-0. 01976	0. 00426	0. 00072	0. 00031	-0. 00048
54'	3235. 32733	-33. 46803	-0. 81969	-0. 24547	-0. 01979	0. 00426	0. 00072	0. 00031	-0. 00048
55'	3235. 31822	-33. 48815	-0. 82052	-0. 24543	-0. 01982	0. 00427	0. 00073	0. 00031	-0. 00048
56'	3235. 30912	-33 50828	-0. 82135	-0. 24539	-0. 01985	0. 00428	0. 00073	0. 00031	-0. 00048
57'	3235. 30002	-33 52843	-0. 82218	-0. 24535	-0. 01988	0. 00429	0. 00073	0. 00031	-0. 00048
58'	3235. 29092	-33 54859	-0. 82302	-0. 24531	-0. 01991	0. 00429	0. 00073	0. 00031	-0. 00048
59'	3235. 28182	-33. 56877	-0. 82385	-0. 24527	-0. 01993	0. 00430	0. 00073	0. 00031	-0. 00048
60'	3235. 27273	-33. 58897	-0. 82469	-0. 24522	-0. 01996	0. 00431	0. 00073	0. 00031	-0. 00048

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda'' = (y) y + (xy)\,xy + (x^2y)\,x^2y + \dots$ gdzie $x = S\cos A$ $y = S\sin A$

S odległość linii geodezyjnej wyrażona w setkach kilometrów
A azymut linii geodezyjnej w punkcie wyjściowym

φ 52°	(y)	(xy)	(x^2y)	(y^3)	(x^3y)	(xy^3)	(x^4y)	(x^4y^3)	(x^4y)	(y^5)	Poprawka interpolacyjna dla wyrazu (y)	
											K'	p.
0°	5242. 49286	104. 99841	2. 53192	-0. 70098	0. 05926	-0. 05069	-0. 00239	0. 00140	0. 00020			
1°	5244. 44074	105. 10032	2. 53538	-0. 70208	0. 05937	-0. 05079	-0. 00240	0. 00140	0. 00020			
2°	5246. 38051	105. 20237	2. 53884	-0. 70318	0. 05947	-0. 05089	-0. 00241	0. 00141	0. 00020			
3°	5248. 34218	105. 30455	2. 54231	-0. 70429	0. 05958	-0. 05099	-0. 00241	0. 00141	0. 00020			
4°	5250. 29575	105. 40686	2. 54579	-0. 70540	0. 05969	-0. 05109	-0. 00242	0. 00141	0. 00020			1
5°	5252. 25122	105. 50930	2. 54928	-0. 70650	0. 05980	-0. 05119	-0. 00242	0. 00142	0. 00021			0.0001"
6°	5254. 20860	105. 61188	2. 55277	-0. 70761	0. 05991	-0. 05129	-0. 00243	0. 00142	0. 00021			
7°	5256. 16789	105. 71459	2. 55626	-0. 70873	0. 06002	-0. 05139	-0. 00244	0. 00142	0. 00021		0'01	
8°	5258. 12909	105. 81743	2. 55977	-0. 70984	0. 06013	-0. 05149	-0. 00244	0. 00143	0. 00021		0'02	2
9°	5260. 09220	105. 92041	2. 56328	-0. 71096	0. 06024	-0. 05159	-0. 00245	0. 00143	0. 00021		0'03	3
10°	5262. 05723	106. 02351	2. 56679	-0. 71208	0. 06035	-0. 05170	-0. 00245	0. 00143	0. 00021		0'04	4
11°	5264. 02418	106. 12676	2. 57032	-0. 71320	0. 06046	-0. 05180	-0. 00246	0. 00144	0. 00021		0'05	5
12°	5265. 99305	106. 23013	2. 57384	-0. 71432	0. 06057	-0. 05190	-0. 00246	0. 00144	0. 00021		0'06	6
13°	5267. 96385	106. 33364	2. 57738	-0. 71545	0. 06068	-0. 05200	-0. 00247	0. 00144	0. 00021		0'07	6
14°	5269. 93657	106. 43729	2. 58092	-0. 71657	0. 06079	-0. 05210	-0. 00248	0. 00145	0. 00021		0'08	7
15°	5271. 91122	106. 54107	2. 58447	-0. 71770	0. 06090	-0. 05221	-0. 00248	0. 00145	0. 00021		0'09	8
16°	5273. 88780	106. 64498	2. 58802	-0. 71883	0. 06101	-0. 05231	-0. 00249	0. 00145	0. 00021		0'10	9
17°	5275. 86631	106. 74904	2. 59158	-0. 71997	0. 06113	-0. 05241	-0. 00249	0. 00146	0. 00021		0'12	10
18°	5277. 84676	106. 85322	2. 59515	-0. 72110	0. 06124	-0. 05252	-0. 00250	0. 00146	0. 00021		0'14	12
19°	5279. 82915	106. 95754	2. 59872	-0. 72224	0. 06135	-0. 05262	-0. 00251	0. 00147	0. 00021		0'16	13
20°	5281. 81348	107. 06200	2. 60230	-0. 72338	0. 06146	-0. 05273	-0. 00251	0. 00147	0. 00021		0'18	15
21°	5283. 79976	107. 16659	2. 60588	-0. 72452	0. 06158	-0. 05283	-0. 00252	0. 00147	0. 00021		0'20	16
22°	5285. 78798	107. 27132	2. 60948	-0. 72566	0. 06169	-0. 05294	-0. 00252	0. 00147	0. 00021		0'22	17
23°	5287. 77815	107. 37619	2. 61308	-0. 72681	0. 06180	-0. 05304	-0. 00253	0. 00148	0. 00021		0'24	18
24°	5289. 77027	107. 48119	2. 61668	-0. 72796	0. 06192	-0. 05314	-0. 00254	0. 00148	0. 00022		0'26	19
25°	5291. 76435	107. 58633	2. 62029	-0. 72911	0. 06203	-0. 05325	-0. 00254	0. 00148	0. 00022		0'28	20
26°	5293. 76038	107. 69161	2. 62391	-0. 73026	0. 06215	-0. 05336	-0. 00255	0. 00149	0. 00022		0'30	21
27°	5295. 75837	107. 79703	2. 62754	-0. 73141	0. 06226	-0. 05346	-0. 00256	0. 00149	0. 00022		0'35	22
28°	5297. 75833	107. 90258	2. 63117	-0. 73257	0. 06237	-0. 05357	-0. 00256	0. 00149	0. 00022		0'40	24
29°	5299. 76024	108. 00827	2. 63480	-0. 73373	0. 06249	-0. 05367	-0. 00257	0. 00150	0. 00022		0'45	24
30°	5301. 76413	108. 11410	2. 63845	-0. 73489	0. 06260	-0. 05378	-0. 00257	0. 00150	0. 00022		0'50	25
31°	5303. 76998	108. 22007	2. 64210	-0. 73605	0. 06272	-0. 05389	-0. 00258	0. 00150	0. 00022		0'55	24
32°	5305. 77781	108. 32617	2. 64576	-0. 73722	0. 06284	-0. 05400	-0. 00259	0. 00151	0. 00022		0'60	24
33°	5307. 78761	108. 43242	2. 64942	-0. 73839	0. 06295	-0. 05410	-0. 00259	0. 00151	0. 00022		0'65	22
34°	5309. 79939	108. 53880	2. 65309	-0. 73955	0. 06307	-0. 05421	-0. 00260	0. 00151	0. 00022		0'70	21
35°	5311. 81315	108. 64533	2. 65677	-0. 74073	0. 06319	-0. 05432	-0. 00261	0. 00152	0. 00022		0'72	20
36°	5313. 82889	108. 75199	2. 66045	-0. 74190	0. 06330	-0. 05443	-0. 00261	0. 00152	0. 00022		0'74	19
37°	5315. 84661	108. 85880	2. 66414	-0. 74308	0. 06342	-0. 05453	-0. 00262	0. 00152	0. 00022		0'76	18
38°	5317. 86632	108. 96574	2. 66784	-0. 74425	0. 06354	-0. 05464	-0. 00263	0. 00153	0. 00022		0'78	17
39°	5319. 88803	109. 07283	2. 67155	-0. 74543	0. 06365	-0. 05475	-0. 00263	0. 00153	0. 00022		0'80	16
40°	5321. 91172	109. 18006	2. 67526	-0. 74662	0. 06377	-0. 05486	-0. 00264	0. 00153	0. 00022		0'82	15
41°	5323. 93742	109. 28742	2. 67897	-0. 74780	0. 06389	-0. 05497	-0. 00264	0. 00154	0. 00023		0'84	13
42°	5325. 96511	109. 39493	2. 68270	-0. 74899	0. 06401	-0. 05508	-0. 00265	0. 00154	0. 00023		0'86	12
43°	5327. 99480	109. 50258	2. 68643	-0. 75018	0. 06413	-0. 05519	-0. 00266	0. 00154	0. 00023		0'88	10
44°	5330. 02649	109. 61038	2. 69017	-0. 75137	0. 06425	-0. 05530	-0. 00266	0. 00155	0. 00023		0'90	9
45°	5332. 06019	109. 71831	2. 69391	-0. 75256	0. 06436	-0. 05541	-0. 00267	0. 00155	0. 00023		0'91	8
46°	5334. 09590	109. 82639	2. 69766	-0. 75376	0. 06448	-0. 05552	-0. 00268	0. 00155	0. 00023		0'92	7
47°	5336. 13362	109. 93461	2. 70142	-0. 75495	0. 06460	-0. 05563	-0. 00268	0. 00156	0. 00023		0'93	6
48°	5338. 17335	110. 04297	2. 70519	-0. 75615	0. 06472	-0. 05574	-0. 00269	0. 00156	0. 00023		0'94	6
49°	5340. 21510	110. 15148	2. 70896	-0. 75736	0. 06484	-0. 05585	-0. 00270	0. 00157	0. 00023		0'95	5
50°	5342. 25887	110. 26013	2. 71274	-0. 75856	0. 06497	-0. 05597	-0. 00270	0. 00157	0. 00023		0'96	4
51°	5344. 30466	110. 36892	2. 71652	-0. 75977	0. 06509	-0. 05608	-0. 00271	0. 00157	0. 00023		0'97	3
52°	5346. 35248	110. 47786	2. 72032	-0. 76098	0. 06521	-0. 05619	-0. 00272	0. 00158	0. 00023		0'98	2
53°	5348. 40232	110. 58694	2. 72412	-0. 76219	0. 06533	-0. 05630	-0. 00272	0. 00158	0. 00023		0'99	1
54°	5350. 45420	110. 69616	2. 72792	-0. 76340	0. 06545	-0. 05642	-0. 00273	0. 00158	0. 00023			
55°	5352. 50810	110. 80553	2. 73174	-0. 76462	0. 06557	-0. 05653	-0. 00274	0. 00159	0. 00023			
56°	5354. 56405	110. 91505	2. 73556	-0. 76583	0. 06569	-0. 05664	-0. 00274	0. 00159	0. 00023			
57°	5356. 62203	111. 02471	2. 73939	-0. 76706	0. 06582	-0. 05676	-0. 00275	0. 00159	0. 00024			
58°	5358. 68205	111. 13451	2. 74322	-0. 76828	0. 06594	-0. 05687	-0. 00276	0. 00160	0. 00024			
59°	5360. 74411	111. 24447	2. 74706	-0. 76950	0. 06606	-0. 05698	-0. 00276	0. 00160	0. 00024			
60°	5362. 80822	111. 35456	2. 75091.	-0. 77073	0. 06619	-0. 05710.	-0. 00277	0. 00161.	0. 00024			

A. K.

Przyrost szerokości geograficznej $\Delta\varphi$

$\Delta\varphi'' = (x) + (y^2) + (xy^2) + (x^2y^2) + \ldots$ gdzie $x = S\cos A$ $y = S\sin A$

S długość linii geodezyjnej wyrażona w setkach kilometrów
A azymut linii geodezyjnej w punkcie wyjściowym

φ 53°	(x)	(y^2)	(xy^2)	(x^2)	(x^2y^2)	(y^4)	(x^3)	(xy^4)	(x^3y^2)
0'	3235.27273	-33.58897	-0.82469	-0.24522	-0.01996	0.00431	0.00073	0.00031	-0.00048
1'	3235.26363	-33.60918	-0.82553	-0.24518	-0.01999	0.00431	0.00073	0.00031	-0.00049
2'	3235.25454	-33.62940	-0.82637	-0.24514	-0.02002	0.00432	0.00074	0.00031	-0.00049
3'	3235.24544	-33.64965	-0.82721	-0.24510	-0.02005	0.00433	0.00074	0.00031	-0.00049
4'	3235.23635	-33.66990	-0.82805	-0.24506	-0.02008	0.00433	0.00074	0.00032	-0.00049
5'	3235.22726	-33.69018	-0.82890	-0.24501	-0.02011	0.00434	0.00074	0.00032	-0.00049
6'	3235.21818	-33.71047	-0.82974	-0.24497	-0.02014	0.00435	0.00074	0.00032	-0.00049
7'	3235.20909	-33.73077	-0.83059	-0.24493	-0.02017	0.00435	0.00074	0.00032	-0.00049
8'	3235.20001	-33.75108	-0.83143	-0.24489	-0.02020	0.00436	0.00075	0.00032	-0.00049
9'	3235.19093	-33.77143	-0.83228	-0.24484	-0.02023	0.00437	0.00075	0.00032	-0.00049
10'	3235.18184	-33.79178	-0.83313	-0.24480	-0.02026	0.00438	0.00075	0.00032	-0.00049
11'	3235.17276	-33.81215	-0.83398	-0.24476	-0.02029	0.00438	0.00075	0.00032	-0.00049
12'	3235.16369	-33.83253	-0.83483	-0.24472	-0.02032	0.00439	0.00075	0.00032	-0.00050
13'	3235.15461	-33.85293	-0.83568	-0.24467	-0.02035	0.00440	0.00075	0.00032	-0.00050
14'	3235.14554	-33.87334	-0.83654	-0.24463	-0.02038	0.00440	0.00075	0.00032	-0.00050
15'	3235.13646	-33.89377	-0.83739	-0.24459	-0.02041	0.00441	0.00076	0.00032	-0.00050
16'	3235.12739	-33.91422	-0.83825	-0.24454	-0.02044	0.00442	0.00076	0.00032	-0.00050
17'	3235.11832	-33.93468	-0.83910	-0.24450	-0.02047	0.00443	0.00076	0.00032	-0.00050
18'	3235.10925	-33.95516	-0.83996	-0.24446	-0.02050	0.00443	0.00076	0.00032	-0.00050
19'	3235.10019	-33.97566	-0.84082	-0.24441	-0.02053	0.00444	0.00076	0.00033	-0.00050
20'	3235.09112	-33.99617	-0.84168	-0.24437	-0.02057	0.00445	0.00076	0.00033	-0.00050
21'	3235.08206	-34.01669	-0.84255	-0.24433	-0.02060	0.00446	0.00076	0.00033	-0.00050
22'	3235.07299	-34.03723	-0.84341	-0.24428	-0.02063	0.00446	0.00077	0.00033	-0.00051
23'	3235.06393	-34.05779	-0.84427	-0.24424	-0.02066	0.00447	0.00077	0.00033	-0.00051
24'	3235.05487	-34.07837	-0.84514	-0.24420	-0.02069	0.00448	0.00077	0.00033	-0.00051
25'	3235.04582	-34.09896	-0.84601	-0.24416	-0.02072	0.00448	0.00077	0.00033	-0.00051
26'	3235.03676	-34.11956	-0.84687	-0.24411	-0.02075	0.00449	0.00077	0.00033	-0.00051
27'	3235.02771	-34.14019	-0.84774	-0.24406	-0.02078	0.00450	0.00077	0.00033	-0.00051
28'	3235.01865	-34.16083	-0.84861	-0.24402	-0.02081	0.00451	0.00077	0.00033	-0.00051
29'	3235.00960	-34.18148	-0.84949	-0.24398	-0.02084	0.00451	0.00078	0.00033	-0.00051
30'	3235.00055	-34.20215	-0.85036	-0.24393	-0.02087	0.00452	0.00078	0.00033	-0.00051
31'	3234.99151	-34.22284	-0.85123	-0.24389	-0.02091	0.00453	0.00078	0.00033	-0.00051
32'	3234.98246	-34.24355	-0.85211	-0.24384	-0.02094	0.00454	0.00078	0.00033	-0.00052
33'	3234.97342	-34.26427	-0.85298	-0.24380	-0.02097	0.00454	0.00078	0.00033	-0.00052
34'	3234.96437	-34.28500	-0.85386	-0.24375	-0.02100	0.00455	0.00078	0.00034	-0.00052
35'	3234.95533	-34.30576	-0.85474	-0.24371	-0.02103	0.00456	0.00079	0.00034	-0.00052
36'	3234.94629	-34.32653	-0.85562	-0.24366	-0.02106	0.00457	0.00079	0.00034	-0.00052
37'	3234.93726	-34.34731	-0.85650	-0.24362	-0.02109	0.00457	0.00079	0.00034	-0.00052
38'	3234.92822	-34.36811	-0.85739	-0.24357	-0.02113	0.00458	0.00079	0.00034	-0.00052
39'	3234.91919	-34.38893	-0.85827	-0.24353	-0.02116	0.00459	0.00079	0.00034	-0.00052
40'	3234.91015	-34.40977	-0.85915	-0.24348	-0.02119	0.00459	0.00079	0.00034	-0.00052
41'	3234.90112	-34.43062	-0.86004	-0.24344	-0.02122	0.00460	0.00079	0.00034	-0.00052
42'	3234.89209	-34.45149	-0.86093	-0.24339	-0.02125	0.00461	0.00080	0.00034	-0.00053
43'	3234.88306	-34.47237	-0.86182	-0.24335	-0.02128	0.00462	0.00080	0.00034	-0.00053
44'	3234.87404	-34.49327	-0.86271	-0.24330	-0.02132	0.00463	0.00080	0.00034	-0.00053
45'	3234.86501	-34.51419	-0.86360	-0.24326	-0.02135	0.00463	0.00080	0.00034	-0.00053
46'	3234.85599	-34.53512	-0.86449	-0.24321	-0.02138	0.00464	0.00080	0.00034	-0.00053
47'	3234.84697	-34.55607	-0.86539	-0.24317	-0.02141	0.00465	0.00080	0.00034	-0.00053
48'	3234.83795	-34.57704	-0.86628	-0.24312	-0.02145	0.00466	0.00080	0.00035	-0.00053
49'	3234.82893	-34.59802	-0.86718	-0.24308	-0.02148	0.00466	0.00081	0.00035	-0.00053
50'	3234.81991	-34.61902	-0.86808	-0.24303	-0.02151	0.00467	0.00081	0.00036	-0.00053
51'	3234.81090	-34.64004	-0.86897	-0.24298	-0.02154	0.00468	0.00081	0.00035	-0.00053
52'	3234.80189	-34.66108	-0.86987	-0.24294	-0.02157	0.00469	0.00081	0.00036	-0.00054
53'	3234.79288	-34.68213	-0.87078	-0.24289	-0.02161	0.00469	0.00081	0.00035	-0.00054
54'	3234.78387	-34.70319	-0.87168	-0.24285	-0.02164	0.00470	0.00081	0.00035	-0.00054
55'	3234.77486	-34.72428	-0.87258	-0.24280	-0.02167	0.00471	0.00081	0.00035	-0.00054
56'	3234.76586	-34.74538	-0.87349	-0.24275	-0.02171	0.00472	0.00082	0.00035	-0.00054
57'	3234.75685	-34.76650	-0.87439	-0.24271	-0.02174	0.00473	0.00082	0.00035	-0.00054
58'	3234.74784	-34.78763	-0.87530	-0.24266	-0.02177	0.00473	0.00082	0.00035	-0.00054
59'	3234.73884	-34.80878	-0.87621	-0.24261	-0.02180	0.00474	0.00082	0.00035	-0.00054
60'	3234.72984	-34.82995	-0.87712	-0.24257	-0.02184	0.00475	0.00082	0.00036	-0.00054

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda'' = (y)y + (xy)xy + (x^2y)x^2y + \ldots$ gdzie $x = S\cos A$ $y = S\sin A$

S długość linji geodezyjnej wyrażona w setkach kilometrow
A azymut linji geodezyjnej w punkcie wyjściowym.

φ 53°	(1)	(xy)	(x^2y)	(y^3)	(x^3y)	(xy^3)	(x^2y^3)	(x^4y)	(y^5)	Poprawka interpolacyjna dla wyrazu (y)	
										K'	P
0'	5362. 80822	111. 35456	2. 75091	-0. 77073	0. 06819	-0. 05710	-0. 00277	0. 00161	0. 00026		
1'	5364. 87438	111. 46481	2. 75477	-0. 77196	0. 06631	-0. 05721	-0. 00278	0. 00161	0. 00024		
2'	5366. 94259	111. 57520	2. 75863	-0. 77319	0. 06643	-0. 05733	-0. 00278	0. 00161	0. 00024		
3'	5369. 01286	111. 68574	2. 76250	-0. 77442	0. 06656	-0. 05744	-0. 00279	0. 00162	0. 00024		
4'	5371. 08518	111. 79642	2. 76638	-0. 77566	0. 06668	-0. 05756	-0. 00280	0. 00162	0. 00024		
5'	5373. 15957	111. 90725	2. 77026	-0. 77690	0. 06681	-0. 05767	-0. 00280	0. 00162	0. 00024		
6'	5375. 23601	112. 01823	2. 77415	-0. 77814	0. 06693	-0. 05779	-0. 00281	0. 00163	0. 00024		
7'	5377. 31452	112. 12936	2. 77805	-0. 77938	0. 06706	-0. 05791	-0. 00282	0. 00163	0. 00024	0'1	1
8'	5379. 39510	112. 24063	2. 78196	-0. 78063	0. 06718	-0. 05802	-0. 00283	0. 00164	0. 00024	0'2	2
9'	5381. 47775	112. 35206	2. 78587	-0. 78188	0. 06731	-0. 05814	-0. 00283	0. 00164	0. 00024	0'3	3
10'	5383. 56248	112. 46363	2. 78979	-0. 78313	0. 06743	-0. 05826	-0. 00284	0. 00164	0. 00024	0'4	4
11	5385. 64928	112. 57535	2. 79371	-0. 78438	0. 06756	-0. 05837	-0. 00285	0. 00165	0. 00024	0'5	5
12'	5387. 73816	112. 68722	2. 79765	-0. 78564	0. 06769	-0. 05849	-0. 00285	0. 00165	0. 00025	0'6	6
13'	5389. 82912	112. 79924	2. 80159	-0. 78689	0. 06781	-0. 05861	-0. 00286	0. 00166	0. 00025	0'7	7
14'	5391. 92217	112. 91141	2. 80554	-0. 78815	0. 06794	-0. 05873	-0. 00287	0. 00166	0. 00025	0'8	8
15'	5394. 01730	113. 02373	2. 80950	-0. 78941	0. 06807	-0. 05885	-0. 00287	0. 00166	0. 00025	0'9	9
16'	5396. 11453	113. 13620	2. 81346	-0. 79068	0. 06820	-0. 05897	-0. 00288	0. 00167	0. 00025	0'10	10
17'	5398. 21384	113. 24882	2. 81743	-0. 79195	0. 06833	-0. 05908	-0. 00289	0. 00167	0. 00025	0'12	11
18'	5400. 31525	113. 36160	2. 82141	-0. 79322	0. 06845	-0. 05920	-0. 00290	0. 00167	0. 00025	0'14	13
19'	5402. 41877	113. 47452	2. 82539	-0. 79449	0. 06858	-0. 05932	-0. 00290	0. 00168	0. 00025	0'16	14
20'	5404. 52438	113. 58759	2. 82938	-0. 79576	0. 06871	-0. 05944	-0. 00291	0. 00168	0. 00025	0'18	16
21'	5406. 63210	113. 70082	2. 83339	-0. 79704	0. 06884	-0. 05956	-0. 00292	0. 00169	0. 00025	0'20	17
22'	5408. 74193	113. 81420	2. 83739	-0. 79832	0. 06897	-0. 05968	-0. 00292	0. 00169	0. 00025	0'22	18
23'	5410. 85386	113. 92773	2. 84141	-0. 79960	0. 06910	-0. 05980	-0. 00293	0. 00169	0. 00025	0'24	19
24'	5412. 96791	114. 04141	2. 84543	-0. 80088	0. 06923	-0. 05993	-0. 00294	0. 00170	0. 00025	0'26	21
25'	5415. 08407	114. 15525	2. 84946	-0. 80217	0. 06936	-0. 06005	-0. 00295	0. 00170	0. 00025	0'28	22
26'	5417. 20236	114. 26924	2. 85350	-0. 80346	0. 06949	-0. 06017	-0. 00295	0. 00171	0. 00026	0'30	22
27'	5419. 32276	114. 38338	2. 85754	-0. 80475	0. 06962	-0. 06029	-0. 00296	0. 00171	0. 00026	0'35	24
28'	5421. 44529	114. 49768	2. 86159	-0. 80604	0. 06976	-0. 06041	-0. 00297	0. 00171	0. 00026	0'40	26
29'	5423. 56995	114. 61213	2. 86565	-0. 80734	0. 06989	-0. 06054	-0. 00298	0. 00172	0. 00026	0'45	26
30'	5425. 69673	114. 72673	2. 86972	-0. 80863	0. 07002	-0. 06066	-0. 00298	0. 00172	0. 00026	0'50	27
31'	5427. 82565	114. 84149	2. 87379	-0. 80993	0. 07015	-0. 06078	-0. 00299	0. 00173	0. 00026	0'55	26
32'	5429. 95671	114. 95640	2. 87788	-0. 81124	0. 07029	-0. 06090	-0. 00300	0. 00173	0. 00026	0'80	26
33'	5432. 08990	115. 07147	2. 88197	-0. 81254	0. 07042	-0. 06103	-0. 00301	0. 00173	0. 00026	0'85	24
34'	5434. 22524	115. 18670	2. 88606	-0. 81385	0. 07055	-0. 06115	-0. 00301	0. 00174	0. 00026	0'70	22
35'	5436. 36272	115. 30208	2. 89017	-0. 81516	0. 07068	-0. 06128	-0. 00302	0. 00174	0. 00026	0'72	22
36	5438. 50234	115. 41761	2. 89428	-0. 81648	0. 07082	-0. 06140	-0. 00303	0. 00175	0. 00026	0'74	21
37'	5440. 64412	115. 53330	2. 89840	-0. 81779	0. 07095	-0. 06153	-0. 00304	0. 00175	0. 00026	0'76	19
38	5442. 78805	115. 64915	2. 90253	-0. 81911	0. 07109	-0. 06165	-0. 00304	0. 00175	0. 00026	0'78	18
39'	5444. 93414	115. 76516	2. 90666	-0. 82043	0. 07122	-0. 06178	-0. 00305	0. 00176	0. 00026	0'80	17
40'	5447. 08238	115. 88132	2. 91081	-0. 82175	0. 07136	-0. 06190	-0. 00306	0. 00176	0. 00026	0'82	16
41	5449. 23279	115. 99764	2. 91496	-0. 82308	0. 07149	-0. 06203	-0. 00307	0. 00177	0. 00026	0'84	14
42'	5451. 38537	116. 11412	2. 91912	-0. 82441	0. 07163	-0. 06215	-0. 00307	0. 00177	0. 00027	0'86	13
43'	5453. 54011	116. 23075	2. 92328	-0. 82574	0. 07177	-0. 06228	-0. 00308	0. 00178	0. 00027	0'88	11
44	5455. 69702	116. 34755	2. 92746	-0. 82707	0. 07190	-0. 06241	-0. 00309	0. 00178	0. 00027	0'90	10
45'	5457. 85611	116. 46450	2. 93164	-0. 82841	0. 07204	-0. 06254	-0. 00310	0. 00178	0. 00027	0'91	9
46	5460. 01737	116. 58161	2. 93583	-0. 82975	0. 07218	-0. 06266	-0. 00310	0. 00179	0. 00027	0'92	8
47'	5462. 18081	116. 69888	2. 94003	-0. 83109	0. 07231	-0. 06279	-0. 00311	0. 00179	0. 00027	0'93	7
48	5464. 34644	116. 81631	2. 94423	-0. 83243	0. 07245	-0. 06292	-0. 00312	0. 00180	0. 00027	0'94	6
49'	5466. 51425	116. 93390	2. 94845	-0. 83378	0. 07259	-0. 06305	-0. 00313	0. 00180	0. 00027	0'95	5
50'	5468. 68424	117. 05165	2. 95267	-0. 83512	0. 07273	-0. 06318	-0. 00314	0. 00180	0. 00027	0'98	4
51	5470. 85644	117. 16956	2. 95690	-0. 83647	0. 07287	-0. 06331	-0. 00314	0. 00181	0. 00027	0'97	3
52'	5473. 03082	117. 28763	2. 96114	-0. 83783	0. 07301	-0. 06344	-0. 00315	0. 00181	0. 00027	0'98	2
53'	5475. 20740	117. 40587	2. 96538	-0. 83918	0. 07315	-0. 06357	-0. 00316	0. 00182	0. 00027	0'99	1
54'	5477. 38619	117. 52426	2. 96963	-0. 84054	0. 07328	-0. 06370	-0. 00317	0. 00182	0. 00027		
55'	5479. 56717	117. 64281	2. 97389	-0. 84190	0. 07342	-0. 06383	-0. 00318	0. 00183	0. 00027		
56'	5481. 75037	117. 76153	2. 97816	-0. 84327	0. 07357	-0. 06396	-0. 00318	0. 00183	0. 00028		
57'	5483. 93577	117. 88041	2. 98244	-0. 84464	0. 07371	-0. 06409	-0. 00319	0. 00184	0. 00028		
58'	5486. 12339	117. 99945	2. 98673	-0. 84601	0. 07385	-0. 06422	-0. 00320	0. 00184	0. 00028		
59'	5488. 31322	118. 11865	2. 99102	-0. 84738	0. 07399	-0. 06435	-0. 00321	0. 00184	0. 00028		
60'	5490. 50527	118. 23802	2. 99532	-0. 84875	0. 07413	-0. 06448	-0. 00321	0. 00185	0. 00028		

Przyrost szerokości geograficznej $\Delta\varphi$

$\Delta\varphi'' = (x) + (y^2) + (xy^2) + (x^2) + (x^2y^2) + (y^4) + (x^3) + (xy^4) + (x^3y^2)$ ..... gdzie $x = S\cos A$ $y = S\sin A$

S długość linji geodezyjnej wyrażona w setkach kilometrów

A azymut linji geodezyjnej w punkcie wyjściowym.

φ54	(x)	(y²)	(xy²)	(x²)	(x²y²)	(y⁴)	(x³)	(xy⁴)	(x³y²)
0'	3234. 72984	-34. 82995	-0. 87712	-0. 24257	-0. 02184	0. 00475	0. 00082	0. 00036	-0. 00054
1'	3234. 72085	-34. 85114	-0. 87803	-0. 24252	-0. 02187	0. 00476	0. 00082	0. 00036	-0. 00055
2'	3234. 71185	-34. 87234	-0. 87895	-0. 24247	-0. 02190	0. 00476	0. 00083	0. 00036	-0. 00055
3'	3234. 70286	-34. 89356	-0. 87986	-0. 24242	-0. 02194	0. 00477	0. 00083	0. 00036	-0. 00055
4'	3234. 69386	-34. 91479	-0. 88078	-0. 24238	-0. 02197	0. 00478	0. 00083	0. 00036	-0. 00055
5'	3234. 68487	-34. 93605	-0. 88170	-0. 24233	-0. 02200	0. 00479	0. 00083	0. 00036	-0. 00055
6'	3234. 67588	-34. 95732	-0. 88261	-0. 24228	-0. 02204	0. 00480	0. 00083	0. 00036	-0. 00055
7'	3234. 66689	-34. 97861	-0. 88353	-0. 24224	-0. 02207	0. 00480	0. 00083	0. 00036	-0. 00055
8'	3234. 65791	-34. 99991	-0. 88445	-0. 24219	-0. 02210	0. 00481	0. 00083	0. 00036	-0. 00055
9	3234. 64893	-35. 02123	-0. 88538	-0. 24214	-0. 02214	0. 00482	0. 00084	0. 00036	-0. 00055
10'	3234. 63994	-35. 04257	-0. 88630	-0. 24209	-0. 02217	0. 00483	0. 00084	0. 00036	-0. 00056
11'	3234. 63096	-35. 06393	-0. 88722	-0. 24205	-0. 02220	0. 00484	0. 00084	0. 00036	-0. 00056
12'	3234. 62198	-35. 08530	-0. 88815	-0. 24200	-0. 02224	0. 00484	0. 00084	0. 00036	-0. 00056
13'	3234. 61301	-35. 10669	-0. 88908	-0. 24195	-0. 02227	0. 00485	0. 00084	0. 00036	-0. 00056
14'	3234. 60403	-35. 12810	-0. 89001	-0. 24190	-0. 02230	0. 00486	0. 00084	0. 00036	-0. 00056
15'	3234. 59506	-35. 14952	-0. 89094	-0. 24186	-0. 02234	0. 00487	0. 00084	0. 00037	-0. 00056
16'	3234. 58609	-35. 17097	-0. 89187	-0. 24181	-0. 02237	0. 00488	0. 00085	0. 00037	-0. 00056
17'	3234. 57712	-35. 19242	-0. 89280	-0. 24176	-0. 02241	0. 00488	0. 00085	0. 00037	-0. 00056
18'	3234. 56815	-35. 21390	-0. 89373	-0. 24171	-0. 02244	0. 00489	0. 00085	0. 00037	-0. 00056
19'	3234. 55918	-35. 23540	-0. 89467	-0. 24166	-0. 02247	0. 00490	0. 00085	0. 00037	-0. 00057
20'	3234. 55022	-35. 25691	-0. 89561	-0. 24161	-0. 02251	0. 00491	0. 00085	0. 00037	-0. 00057
21'	3234. 54125	-35. 27844	-0. 89654	-0. 24157	-0. 02254	0. 00492	0. 00085	0. 00037	-0. 00057
22'	3234. 53229	-35. 29998	-0. 89748	-0. 24152	-0. 02258	0. 00492	0. 00085	0. 00037	-0. 00057
23'	3234. 52333	-35. 32155	-0. 89843	-0. 24147	-0. 02261	0. 00493	0. 00086	0. 00037	-0. 00057
24'	3234. 51438	-35. 34313	-0. 89937	-0. 24142	-0. 02265	0. 00494	0. 00086	0. 00037	-0. 00057
25'	3234. 50542	-35. 36473	-0. 90031	-0. 24137	-0. 02268	0. 00495	0. 00086	0. 00037	-0. 00057
26'	3234. 49647	-35. 38634	-0. 90126	-0. 24132	-0. 02272	0. 00496	0. 00086	0. 00037	-0. 00057
27'	3234. 48751	-35. 40798	-0. 90220	-0. 24127	-0. 02275	0. 00497	0. 00086	0. 00038	-0. 00057
28'	3234. 47856	-35. 42963	-0. 90315	-0. 24122	-0. 02279	0. 00497	0. 00086	0. 00038	-0. 00058
29'	3234. 46961	-35. 45130	-0. 90410	-0. 24118	-0. 02282	0. 00498	0. 00086	0. 00038	-0. 00058
30'	3234. 46067	-35. 47298	-0. 90505	-0. 24113	-0. 02286	0. 00499	0. 00087	0. 00038	-0. 00058
31'	3234. 45172	-35. 49469	-0. 90600	-0. 24108	-0. 02289	0. 00500	0. 00087	0. 00038	-0. 00058
32'	3234. 44278	-35. 51641	-0. 90695	-0. 24103	-0. 02293	0. 00501	0. 00087	0. 00038	-0. 00058
33'	3234. 43384	-35. 53815	-0. 90791	-0. 24098	-0. 02296	0. 00502	0. 00087	0. 00038	-0. 00058
34'	3234. 42490	-35. 55991	-0. 90886	-0. 24093	-0. 02300	0. 00502	0. 00087	0. 00038	-0. 00058
35'	3234. 41596	-35. 58168	-0. 90982	-0. 24088	-0. 02303	0. 00503	0. 00087	0. 00038	-0. 00058
36'	3234. 40703	-35. 60348	-0. 91078	-0. 24083	-0. 02307	0. 00504	0. 00087	0. 00038	-0. 00058
37'	3234. 39809	-35. 62529	-0. 91174	-0. 24078	-0. 02310	0. 00505	0. 00088	0. 00038	-0. 00059
38'	3234. 38916	-35. 64712	-0. 91270	-0. 24073	-0. 02314	0. 00506	0. 00088	0. 00038	-0. 00059
39'	3234. 38023	-35. 66896	-0. 91366	-0. 24068	-0. 02317	0. 00507	0. 00088	0. 00038	-0. 00059
40'	3234. 37130	-35. 69083	-0. 91463	-0. 24063	-0. 02321	0. 00507	0. 00088	0. 00039	-0. 00059
41'	3234. 36237	-35. 71271	-0. 91559	-0. 24058	-0. 02324	0. 00508	0. 00088	0. 00039	-0. 00059
42'	3234. 35345	-35. 73461	-0. 91656	-0. 24053	-0. 02328	0. 00509	0. 00088	0. 00039	-0. 00059
43'	3234. 34452	-35. 75653	-0. 91752	-0. 24048	-0. 02332	0. 00510	0. 00088	0. 00039	-0. 00059
44'	3234. 33560	-35. 77847	-0. 91849	-0. 24043	-0. 02335	0. 00511	0. 00089	0. 00039	-0. 00059
45'	3234. 32668	-35. 80042	-0. 91947	-0. 24038	-0. 02339	0. 00512	0. 00089	0. 00039	-0. 00060
46'	3234. 31777	-35. 82239	-0. 92044	-0. 24033	-0. 02342	0. 00512	0. 00089	0. 00039	-0. 00060
47'	3234. 30885	-35. 84438	-0. 92141	-0. 24028	-0. 02346	0. 00513	0. 00089	0. 00039	-0. 00060
48'	3234. 29994	-35. 86639	-0. 92239	-0. 24023	-0. 02350	0. 00514	0. 00089	0. 00039	-0. 00060
49	3234. 29102	-35. 88842	-0. 92336	-0. 24018	-0. 02353	0. 00515	0. 00089	0. 00039	-0. 00060
50	3234. 28211	-35. 91046	-0. 92434	-0. 24013	-0. 02357	0. 00516	0. 00090	0. 00039	-0. 00060
51'	3234. 27321	-35. 93253	-0. 92532	-0. 24008	-0. 02360	0. 00517	0. 00090	0. 00039	-0. 00060
52'	3234. 26430	-35. 95461	-0. 92630	-0. 24002	-0. 02364	0. 00518	0. 00090	0. 00040	-0. 00060
53'	3234. 25539	-35. 97671	-0. 92728	-0. 23997	-0. 02368	0. 00519	0. 00090	0. 00040	-0. 00061
54'	3234. 24649	-35. 99883	-0. 92827	-0. 23992	-0. 02371	0. 00519	0. 00090	0. 00040	-0. 00061
55'	3234. 23759	-36. 02096	-0. 92925	-0. 23987	-0. 02375	0. 00520	0. 00090	0. 00040	-0. 00061
56'	3234. 22869	-36. 04312	-0. 93024	-0. 23982	-0. 02379	0. 00521	0. 00090	0. 00040	-0. 00061
57'	3234. 21979	-36. 06529	-0. 93123	-0. 23977	-0. 02382	0. 00522	0. 00091	0. 00040	-0. 00061
58'	3234. 21090	-36. 08748	-0. 93222	-0. 23972	-0. 02386	0. 00523	0. 00091	0. 00040	-0. 00061
59'	3234. 20201	-36. 10969	-0. 93321	-0. 23967	-0. 02390	0. 00524	0. 00091	0. 00040	-0. 00061
60'	3234. 19311	-36. 13192	-0. 93420	-0. 23961	-0. 02393	0. 00525	0. 00091	0. 00040	-0. 00061

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda'' = (y)\,y + (xy)\,xy + (x^2y)\,x^2y + \ldots$ gdzie $x = s\cos A$, $y = s\sin A$

s długość linii geodezyjnej wyrażona w setkach kilometrów

A azymut linii geodezyjnej w punkcie wyjściowym

φ 54	(y)	(xy)	(x²y)	(y³)	(x³y)	(xy³)	(x²y³)	(x⁴y)	(y⁵)	Poprawka interpolacyjna dla wyrazu (y)	
										K'	p.
0'	5490. 50527	118. 23802	2. 98532	-0. 84875	0. 07413	-0. 06448	-0. 00321	0. 00185	0. 00028		
1'	5492. 69954	118. 35755	2. 99963	-0. 85013	0. 07427	-0. 06461	-0. 00322	0. 00185	0. 00028		
2'	5494. 89604	118. 47724	3. 00395	-0. 85151	0. 07441	-0. 06475	-0. 00323	0. 00186	0. 00028		
3'	5497. 09476	118. 59710	3. 00827	-0. 85289	0. 07456	-0. 06488	-0. 00324	0. 00186	0. 00028		
4'	5499. 29572	118. 71712	3. 01261	-0. 85428	0. 07470	-0. 06501	-0. 00325	0. 00187	0. 00028		
5'	5501. 49891	118. 83731	3. 01695	-0. 85566	0. 07484	-0. 06515	-0. 00326	0. 00187	0. 00028		1
6'	5503. 70433	118. 95766	3. 02130	-0. 85705	0. 07499	-0. 06528	-0. 00326	0. 00187	0. 00028		·10000
7'	5505. 91200	119. 07817	3. 02566	-0. 85845	0. 07513	-0. 06541	-0. 00327	0. 00188	0. 00028		
8'	5508. 12191	119. 19885	3. 03002	-0. 85984	0. 07528	-0. 06555	-0. 00328	0. 00188	0. 00028	0'01	1
9'	5510. 33406	119. 31970	3. 03440	-0. 86124	0. 07542	-0. 06568	-0. 00329	0. 00189	0. 00028	0'02	2
10'	5512. 54847	119. 44071	3. 03878	-0. 86264	0. 07557	-0. 06582	-0. 00330	0. 00189	0. 00029	0'03	3
11'	5514. 76513	119. 56190	3. 04317	-0. 86405	0. 07571	-0. 06595	-0. 00331	0. 00190	0. 00029	0'04	4
12'	5516. 98404	119. 68324	3. 04757	-0. 86545	0. 07586	-0. 06609	-0. 00331	0. 00190	0. 00029	0'05	6
13'	5519. 20521	119. 80476	3. 05198	-0. 86686	0. 07600	-0. 06623	-0. 00332	0. 00191	0. 00029	0'06	7
14'	5521. 42864	119. 92644	3. 05640	-0. 86828	0. 07615	-0. 06636	-0. 00333	0. 00191	0. 00029	0'07	8
15'	5523. 65434	120. 04829	3. 06082	-0. 86969	0. 07630	-0. 06650	-0. 00334	0. 00192	0. 00029	0'08	9
16'	5525. 88231	120. 17030	3. 06525	-0. 87111	0. 07644	-0. 06664	-0. 00335	0. 00192	0. 00029	0'09	10
17'	5528. 11254	120. 29249	3. 06969	-0. 87253	0. 07659	-0. 06677	-0. 00336	0. 00192	0. 00029	0'10	10
18'	5530. 34505	120. 41484	3. 07414	-0. 87395	0. 07674	-0. 06691	-0. 00336	0. 00193	0. 00029	0'12	12
19'	5532. 57984	120. 53736	3. 07860	-0. 87538	0. 07689	-0. 06705	-0. 00337	0. 00193	0. 00029	0'14	14
20'	5534. 81691	120. 66006	3. 08307	-0. 87681	0. 07703	-0. 06719	-0. 00338	0. 00194	0. 00029	0'16	16
21'	5537. 05626	120. 78292	3. 08754	-0. 87824	0. 07718	-0. 06733	-0. 00339	0. 00194	0. 00029	0'18	17
22'	5539. 29790	120. 90595	3. 09203	-0. 87967	0. 07733	-0. 06747	-0. 00340	0. 00195	0. 00029	0'20	19
23'	5541. 54183	121. 02915	3. 09652	-0. 88111	0. 07748	-0. 06761	-0. 00341	0. 00195	0. 00030	0'22	20
24'	5543. 78806	121. 15253	3. 10102	-0. 88255	0. 07763	-0. 06775	-0. 00342	0. 00196	0. 00030	0'24	21
25'	5546. 03657	121. 27607	3. 10553	-0. 88399	0. 07778	-0. 06789	-0. 00342	0. 00196	0. 00030	0'26	22
26'	5548. 28739	121. 39978	3. 11005	-0. 88543	0. 07793	-0. 06803	-0. 00343	0. 00197	0. 00030	0'30	23
27'	5550. 54051	121. 52367	3. 11457	-0. 88688	0. 07808	-0. 06817	-0. 00344	0. 00197	0. 00030	0'35	24
28'	5552. 79594	121. 64773	3. 11911	-0. 88833	0. 07823	-0. 06831	-0. 00345	0. 00198	0. 00030	0'40	26
29'	5555. 05367	121. 77196	3. 12365	-0. 88979	0. 07839	-0. 06845	-0. 00346	0. 00198	0. 00030	0'45	28
30'	5557. 31372	121. 89636	3. 12820	-0. 89124	0. 07854	-0. 06859	-0. 00347	0. 00199	0. 00030	0'50	29
31'	5559. 57609	122. 02093	3. 13276	-0. 89270	0. 07869	-0. 06874	-0. 00348	0. 00199	0. 00030	0'55	29
32'	5561. 84077	122. 14568	3. 13733	-0. 89416	0. 07884	-0. 06888	-0. 00349	0. 00200	0. 00030	0'60	28
33'	5564. 10778	122. 27060	3. 14191	-0. 89563	0. 07900	-0. 06902	-0. 00349	0. 00200	0. 00030	0'65	26
34'	5566. 37711	122. 39570	3. 14650	-0. 89710	0. 07915	-0. 06916	-0. 00350	0. 00200	0. 00030	0'70	24
35'	5568. 64876	122. 52097	3. 15109	-0. 89857	0. 07930	-0. 06931	-0. 00351	0. 00201	0. 00030	0'72	23
36'	5570. 92275	122. 64641	3. 15570	-0. 90004	0. 07946	-0. 06945	-0. 00352	0. 00201	0. 00031	0'74	22
37'	5573. 19908	122. 77203	3. 16031	-0. 90152	0. 07961	-0. 06960	-0. 00353	0. 00202	0. 00031	0'76	21
38'	5575. 47774	122. 89782	3. 16493	-0. 90299	0. 07977	-0. 06974	-0. 00354	0. 00202	0. 00031	0'78	20
39'	5577. 75874	123. 02379	3. 16957	-0. 90448	0. 07992	-0. 06989	-0. 00355	0. 00203	0. 00031	0'80	19
40'	5580. 04209	123. 14993	3. 17420	-0. 90596	0. 08008	-0. 07003	-0. 00356	0. 00203	0. 00031	0'82	17
41'	5582. 32779	123. 27625	3. 17885	-0. 90745	0. 08024	-0. 07018	-0. 00357	0. 00204	0. 00031	0'84	16
42'	5584. 61584	123. 40275	3. 18351	-0. 90894	0. 08039	-0. 07032	-0. 00358	0. 00204	0. 00031	0'86	14
43'	5586. 90625	123. 52943	3. 18818	-0. 91043	0. 08055	-0. 07047	-0. 00358	0. 00205	0. 00031	0'88	12
44'	5589. 19901	123. 65628	3. 19285	-0. 91193	0. 08071	-0. 07062	-0. 00359	0. 00205	0. 00031	0'90	10
45'	5591. 49413	123. 78331	3. 19754	-0. 91343	0. 08086	-0. 07076	-0. 00360	0. 00206	0. 00031	0'91	10
46'	5593. 79162	123. 91051	3. 20223	-0. 91493	0. 08102	-0. 07091	-0. 00361	0. 00206	0. 00031	0'92	9
47'	5596. 09147	124. 03790	3. 20693	-0. 91644	0. 08118	-0. 07106	-0. 00362	0. 00207	0. 00031	0'93	8
48'	5598. 39370	124. 16546	3. 21164	-0. 91795	0. 08134	-0. 07121	-0. 00363	0. 00207	0. 00032	0'94	7
49'	5600. 69830	124. 29320	3. 21637	-0. 91946	0. 08150	-0. 07136	-0. 00364	0. 00208	0. 00032	0'95	6
50'	5603. 00528	124 42112	3. 22110	-0. 92097	0. 08166	-0. 07151	-0. 00365	0. 00208	0. 00032	0'96	4
51'	5605. 31464	124. 54922	3. 22583	-0. 92249	0. 08182	-0. 07166	-0. 00366	0. 00209	0. 00032	0'97	3
52'	5607. 62638	124. 67750	3. 23058	-0. 92401	0. 08198	-0. 07181	-0. 00367	0. 00209	0. 00032	0'98	2
53'	5609. 94051	124. 80597	3. 23534	-0. 92553	0. 08214	-0. 07196	-0. 00368	0. 00210	0. 00032	0'99	1
54'	5612. 25704	124. 93461	3. 24010	-0. 92706	0. 08230	-0. 07211	-0. 00369	0. 00210	0. 00032		
55'	5614. 57595	125. 06343	3. 24488	-0. 92859	0. 08246	-0. 07226	-0. 00370	0. 00211	0. 00032		
56'	5616. 89727	125. 19243	3. 24966	-0. 93012	0. 08262	-0. 07241	-0. 00371	0. 00211	0. 00032		
57'	5619. 22098	125. 32162	3. 25446	-0. 93165	0. 08278	-0. 07256	-0. 00372	0. 00212	0. 00032		
58'	5621. 54710	125. 45098	3. 25926	-0. 93319	0. 08295	-0. 07271	-0. 00372	0. 00212	0. 00032		
59'	5623. 87563	125. 58053	3. 26407	-0. 93473	0. 08311	-0. 07286	-0. 00373	0. 00213	0. 00033		
60'	5626. 20657	125. 71026	3. 26890	-0. 93628	0. 08327	-0. 07302	-0. 00374	0. 00213	0. 00033		

A. K.

1 Przyrost szerokości geograficznej $\Delta\varphi$

$\Delta\varphi'' = (x) + (y^2) + (xy^2) + (x^2y^2) + \ldots$ gdzie $x = S\cos A$ $y = S\sin A$. S długość linji geodezyjnej wyrażona w setkach kilometrów A azymut linji geodezyjnej w punkcie wyjściowym.

φ 55	(x)	(y^2)	(xy^2)	(x^2)	(x^2y^2)	(y^4)	(x^3)	(xy^4)	(x^3y^2)
0'	3234. 19311	-36. 13192	-0. 93420	-0. 23961	-0. 02393	0. 00525	0. 00091	0. 00040	-0. 00061
1'	3234. 18423	-36. 15416	-0. 93519	-0. 23958	-0. 02397	0. 00526	0. 00091	0. 00040	-0. 00061
2'	3234. 17534	-36. 17643	-0. 93619	-0. 23951	-0. 02401	0. 00526	0. 00091	0. 00040	-0. 00062
3'	3234. 16645	-36. 19871	-0. 93718	-0. 23946	-0. 02405	0. 00527	0. 00091	0. 00041	-0. 00062
4'	3234. 15757	-36. 22102	-0. 93818	-0. 23941	-0. 02408	0. 00528	0. 00092	0. 00041	-0. 00062
5'	3234. 14869	-36. 24334	-0. 93918	-0. 23936	-0. 02412	0. 00529	0. 00092	0. 00041	-0. 00062
6'	3234. 13981	-36. 26568	-0. 94018	-0. 23930	-0. 02416	0. 00530	0. 00092	0. 00041	-0. 00062
7'	3234. 13093	-36. 28803	-0. 94118	-0. 23925	-0. 02420	0. 00531	0. 00092	0. 00041	-0. 00062
8'	3234. 12205	-36. 31041	-0. 94219	-0. 23920	-0. 02423	0. 00532	0. 00092	0. 00041	-0. 00062
9'	3234. 11318	-36. 33281	-0. 94319	-0. 23915	-0. 02427	0. 00533	0. 00092	0. 00041	-0. 00062
10'	3234. 10430	-36. 35522	-0. 94420	-0. 23909	-0. 02431	0. 00534	0. 00092	0. 00041	-0. 00063
11'	3234. 09543	-36. 37765	-0. 94521	-0. 23904	-0. 02435	0. 00534	0. 00093	0. 00041	-0. 00063
12'	3234. 08657	-36. 40010	-0. 94622	-0. 23899	-0. 02438	0. 00535	0. 00093	0. 00041	-0. 00063
13'	3234. 07770	-36. 42257	-0. 94723	-0. 23894	-0. 02442	0. 00536	0. 00093	0. 00041	-0. 00063
14'	3234. 06883	-36. 44506	-0. 94824	-0. 23888	-0. 02446	0. 00537	0. 00093	0. 00042	-0. 00063
15'	3234. 05997	-36. 46757	-0. 94926	-0. 23883	-0. 02450	0. 00538	0. 00093	0. 00042	-0. 00063
16'	3234. 05111	-36. 49010	-0. 95027	-0. 23878	-0. 02454	0. 00539	0. 00093	0. 00042	-0. 00063
17'	3234. 04225	-36. 51264	-0. 95129	-0. 23873	-0. 02457	0. 00540	0. 00093	0. 00042	-0. 00064
18'	3234. 03339	-36. 53521	-0. 95231	-0. 23867	-0. 02461	0. 00541	0. 00094	0. 00042	-0. 00064
19'	3234. 02454	-36. 55779	-0. 95333	-0. 23862	-0. 02465	0. 00542	0. 00094	0. 00042	-0. 00064
20'	3234. 01569	-36. 58039	-0. 95435	-0. 23857	-0. 02469	0. 00543	0. 00094	0. 00042	-0. 00064
21'	3234. 00683	-36. 60301	-0. 95537	-0. 23851	-0. 02473	0. 00544	0. 00094	0. 00042	-0. 00064
22'	3233. 99799	-36. 62565	-0. 95640	-0. 23846	-0. 02477	0. 00544	0. 00094	0. 00042	-0. 00064
23'	3233. 98914	-36. 64831	-0. 95742	-0. 23841	-0. 02481	0. 00545	0. 00094	0. 00042	-0. 00064
24'	3233. 98029	-36. 67099	-0. 95845	-0. 23835	-0. 02484	0. 00546	0. 00094	0. 00042	-0. 00064
25'	3233. 97145	-36. 69369	-0. 95948	-0. 23830	-0. 02488	0. 00547	0. 00095	0. 00043	-0. 00065
26'	3233. 96261	-36. 71640	-0. 96051	-0. 23825	-0. 02492	0. 00548	0. 00095	0. 00043	-0. 00065
27'	3233. 95377	-36. 73914	-0. 96154	-0. 23819	-0. 02496	0. 00549	0. 00095	0. 00043	-0. 00065
28'	3233. 94493	-36. 76190	-0. 96258	-0. 23814	-0. 02500	0. 00550	0. 00095	0. 00043	-0. 00065
29'	3233. 93610	-36. 78467	-0. 96361	-0. 23808	-0. 02504	0. 00551	0. 00095	0. 00043	-0. 00065
30'	3233. 92726	-36. 80746	-0. 96465	-0. 23803	-0. 02508	0. 00552	0. 00095	0. 00043	-0. 00065
31'	3233. 91843	-36. 83028	-0. 96569	-0. 23798	-0. 02512	0. 00553	0. 00095	0. 00043	-0. 00065
32'	3233. 90960	-36. 85311	-0. 96673	-0. 23792	-0. 02516	0. 00554	0. 00096	0. 00043	-0. 00065
33'	3233. 90077	-36. 87596	-0. 96777	-0. 23787	-0. 02520	0. 00555	0. 00096	0. 00043	-0. 00066
34'	3233. 89195	-36. 89883	-0. 96881	-0. 23781	-0. 02524	0. 00556	0. 00096	0. 00043	-0. 00066
35'	3233. 88312	-36. 92172	-0. 96986	-0. 23776	-0. 02528	0. 00557	0. 00096	0. 00043	-0. 00066
36'	3233. 87430	-36. 94463	-0. 97090	-0. 23770	-0. 02532	0. 00558	0. 00096	0. 00044	-0. 00066
37'	3233. 86548	-36. 96756	-0. 97195	-0. 23765	-0. 02536	0. 00559	0. 00096	0. 00044	-0. 00066
38'	3233. 85667	-36. 99051	-0. 97300	-0. 23760	-0. 02540	0. 00559	0. 00096	0. 00044	-0. 00066
39'	3233. 84785	-37. 01348	-0. 97405	-0. 23754	-0. 02543	0. 00560	0. 00097	0. 00044	-0. 00066
40'	3233. 83904	-37. 03646	-0. 97510	-0. 23749	-0. 02548	0. 00561	0. 00097	0. 00044	-0. 00067
41'	3233. 83023	-37. 05947	-0. 97615	-0. 23743	-0. 02552	0. 00562	0. 00097	0. 00044	-0. 00067
42'	3233. 82142	-37. 08250	-0. 97721	-0. 23738	-0. 02556	0. 00563	0. 00097	0. 00044	-0. 00067
43'	3233. 81261	-37. 10555	-0. 97827	-0. 23732	-0. 02560	0. 00564	0. 00097	0. 00044	-0. 00067
44'	3233. 80380	-37. 12861	-0. 97932	-0. 23727	-0. 02564	0. 00565	0. 00097	0. 00044	-0. 00067
45'	3233. 79500	-37. 15170	-0. 98038	-0. 23721	-0. 02568	0. 00566	0. 00097	0. 00044	-0. 00067
46'	3233. 78620	-37. 17480	-0. 98145	-0. 23716	-0. 02572	0. 00567	0. 00098	0. 00045	-0. 00067
47'	3233. 77740	-37. 19793	-0. 98251	-0. 23710	-0. 02576	0. 00568	0. 00098	0. 00045	-0. 00068
48'	3233. 76860	-37. 22107	-0. 98357	-0. 23705	-0. 02580	0. 00569	0. 00098	0. 00045	-0. 00068
49'	3233. 75981	-37. 24424	-0. 98464	-0. 23699	-0. 02584	0. 00570	0. 00098	0. 00045	-0. 00068
50'	3233. 75101	-37. 26742	-0. 98571	-0. 23693	-0. 02588	0. 00571	0. 00098	0. 00045	-0. 00068
51'	3233. 74222	-37. 29062	-0. 98678	-0. 23688	-0. 02592	0. 00572	0. 00098	0. 00045	-0. 00068
52'	3233. 73343	-37. 31385	-0. 98785	-0. 23682	-0. 02596	0. 00573	0. 00098	0. 00045	-0. 00068
53'	3233. 72465	-37. 33709	-0. 98892	-0. 23677	-0. 02600	0. 00574	0. 00099	0. 00045	-0. 00068
54'	3233. 71586	-37. 36036	-0. 98999	-0. 23671	-0. 02604	0. 00575	0. 00099	0. 00045	-0. 00069
55'	3233. 70708	-37. 38364	-0. 99107	-0. 23666	-0. 02608	0. 00576	0. 00099	0. 00045	-0. 00069
56'	3233. 69830	-37. 40694	-0. 99215	-0. 23660	-0. 02613	0. 00577	0. 00099	0. 00046	-0. 00069
57'	3233. 68952	-37. 43027	-0. 99323	-0. 23654	-0. 02617	0. 00578	0. 00099	0. 00046	-0. 00069
58'	3233. 68074	-37. 45361	-0. 99431	-0. 23649	-0. 02621	0. 00579	0. 00099	0. 00046	-0. 00069
59'	3233. 67197	-37. 47698	-0. 99539	-0. 23643	-0. 02625	0. 00580	0. 00099	0. 00046	-0. 00069
60'	3233. 66313	-37. 50036	-0. 99647	-0. 23637	-0. 02629	0. 00581	0. 00100	0. 00046	-0. 00069

Przyrost długości geograficznej $\Delta\lambda$

$\Delta\lambda'' = (y) y + (xy) xy + (x^2y) x^2y + \ldots$ gdzie $x = S\cos A$, $y = S\sin A$. S długość linii geodezyjnej wyrażona w setkach kilometrów, A azymut linii geodezyjnej w punkcie wyjściowym.

φ 55	(y)	(xy)	(x^2y)	(y^3)	(x^3y)	(xy^3)	(x^2y^3)	(x^4y)	(y^5)	Poprawka interpolacyjna dla wyrazu (y)	
										K'	p.
0'	5626.20657	125.71026	3.26890	-0.93628	0.08327	-0.07302	-0.00374	0.00213	0.00033		
1'	5628.53993	125.84017	3.27373	-0.93782	0.08344	-0.07317	-0.00375	0.00214	0.00033		
2'	5630.87570	125.97027	3.27857	-0.93937	0.08360	-0.07332	-0.00376	0.00215	0.00033		
3'	5633.21390	126.10055	3.28342	-0.94093	0.08377	-0.07348	-0.00377	0.00215	0.00033		
4'	5635.55452	126.23102	3.28827	-0.94248	0.08393	-0.07363	-0.00378	0.00216	0.00033		
5'	5637.89757	126.36167	3.29314	-0.94404	0.08410	-0.07379	-0.00379	0.00216	0.00033		-0.0000
6	5640.24305	126.49250	3.29802	-0.94561	0.08426	-0.07394	-0.00380	0.00217	0.00033		
7'	5642.59097	126.62352	3.30291	-0.94717	0.08443	-0.07410	-0.00381	0.00217	0.00033	0'01	1
8'	5644.94132	126.75472	3.30781	-0.94874	0.08459	-0.07425	-0.00382	0.00218	0.00033	0'02	2
9'	5647.29412	126.88611	3.31271	-0.95031	0.08476	-0.07441	-0.00383	0.00218	0.00033	0'03	4
10'	5643.64936	127.01769	3.31763	-0.95189	0.08493	-0.07457	-0.00384	0.00219	0.00034	0'04	5
11'	5652.00705	127.14945	3.32255	-0.95347	0.08510	-0.07472	-0.00385	0.00219	0.00034	0'05	6
12'	5654.36720	127.28140	3.32749	-0.95505	0.08526	-0.07488	-0.00386	0.00220	0.00034	0'06	7
13'	5656.72980	127.41354	3.33243	-0.95663	0.08543	-0.07504	-0.00387	0.00220	0.00034	0'07	8
14'	5659.09486	127.54586	3.33739	-0.95822	0.08560	-0.07520	-0.00388	0.00221	0.00034	0'08	9
15'	5661.46239	127.67838	3.34235	-0.95981	0.08577	-0.07536	-0.00389	0.00221	0.00034	0'09	10
16'	5663.83238	127.81108	3.34732	-0.96140	0.08594	-0.07551	-0.00390	0.00222	0.00034	0'10	11
17'	5666.20484	127.94396	3.35231	-0.96300	0.08611	-0.07567	-0.00391	0.00223	0.00034	0'12	13
18'	5668.57977	128.07704	3.35730	-0.96460	0.08628	-0.07583	-0.00392	0.00223	0.00034	0'14	15
19'	5670.95719	128.21031	3.36230	-0.96620	0.08645	-0.07599	-0.00393	0.00224	0.00034	0'16	17
20'	5673.33708	128.34377	3.36731	-0.96781	0.08662	-0.07615	-0.00394	0.00224	0.00034	0'18	19
21'	5675.71946	128.47742	3.37233	-0.96942	0.08680	-0.07631	-0.00395	0.00225	0.00034	0'20	20
22'	5678.10432	128.61125	3.37737	-0.97103	0.08697	-0.07648	-0.00396	0.00225	0.00035	0'22	22
23	5680.49168	128.74528	3.38241	-0.97265	0.08714	-0.07664	-0.00397	0.00226	0.00035	0'24	23
24'	5682.88153	128.87950	3.38746	-0.97427	0.08731	-0.07680	-0.00398	0.00226	0.00035	0'26	24
25'	5685.27388	129.01391	3.39252	-0.97589	0.08749	-0.07696	-0.00399	0.00227	0.00035	0'28	25
26'	5687.66873	129.14852	3.39759	-0.97751	0.08766	-0.07713	-0.00400	0.00228	0.00035	0'30	26
27'	5690.06609	129.28331	3.40267	-0.97914	0.08784	-0.07729	-0.00401	0.00228	0.00035	0'35	28
28'	5692.46596	129.41830	3.40776	-0.98077	0.08801	-0.07746	-0.00403	0.00229	0.00035	0'40	30
29	5694.86834	129.55348	3.41286	-0.98241	0.08819	-0.07762	-0.00404	0.00229	0.00035	0'45	31
30'	5697.27323	129.68886	3.41797	-0.98405	0.08836	-0.07778	-0.00405	0.00230	0.00035	0'50	32
31	5699.68065	129.82443	3.42309	-0.98569	0.08854	-0.07795	-0.00406	0.00230	0.00036	0'55	31
32'	5702.09059	129.96019	3.42822	-0.98734	0.08871	-0.07811	-0.00407	0.00231	0.00036	1'00	30
33'	5704.50306	130.09615	3.43337	-0.98898	0.08889	-0.07828	-0.00408	0.00232	0.00036	1'15	28
34	5706.91806	130.23230	3.43852	-0.99064	0.08907	-0.07844	-0.00409	0.00232	0.00036	1'30	26
35	5709.33559	130.36865	3.44368	-0.99229	0.08925	-0.07861	-0.00410	0.00233	0.00036	1'72	25
36'	5711.75586	130.50519	3.44885	-0.99395	0.08943	-0.07878	-0.00411	0.00233	0.00036	1'71	24
37'	5714.17827	130.64193	3.45403	-0.99561	0.08960	-0.07895	-0.00412	0.00234	0.00036	1'76	23
38'	5716.60343	130.77887	3.45922	-0.99728	0.08978	-0.07911	-0.00413	0.00234	0.00036	1'78	22
39'	5719.03113	130.91600	3.46442	-0.99895	0.08996	-0.07928	-0.00414	0.00235	0.00036	1'80	20
40'	5721.46139	131.05333	3.46964	-1.00062	0.09014	-0.07945	-0.00415	0.00236	0.00036	1'82	19
41	5723.89421	131.19086	3.47486	-1.00229	0.09032	-0.07962	-0.00416	0.00236	0.00036	1'84	17
42	5726.32959	131.32859	3.48009	-1.00397	0.09050	-0.07979	-0.00417	0.00237	0.00037	1'86	15
43'	5728.76753	131.46651	3.48533	-1.00565	0.09069	-0.07996	-0.00418	0.00237	0.00037	1'88	13
44'	5731.20804	131.60463	3.49059	-1.00734	0.09087	-0.08013	-0.00420	0.00238	0.00037	1'90	11
45'	5733.65112	131.74296	3.49585	-1.00903	0.09105	-0.08030	-0.00421	0.00238	0.00037	1'91	10
46	5736.09677	131.88148	3.50112	-1.01072	0.09123	-0.08047	-0.00422	0.00239	0.00037	1'92	9
47'	5738.54500	132.02020	3.50641	-1.01241	0.09142	-0.08064	-0.00423	0.00240	0.00037	1'93	8
48	5740.99581	132.15912	3.51170	-1.01411	0.09160	-0.08082	-0.00424	0.00240	0.00037	1'94	7
49'	5743.44921	132.29825	3.51701	-1.01581	0.09178	-0.08099	-0.00425	0.00241	0.00037	1'95	6
50	5745.90521	132.43757	3.52232	-1.01752	0.09197	-0.08116	-0.00426	0.00241	0.00037	1'96	5
51'	5748.36379	132.57709	3.52765	-1.01923	0.09215	-0.08134	-0.00427	0.00242	0.00038	1'97	4
52'	5750.82497	132.71682	3.53299	-1.02094	0.09234	-0.08151	-0.00428	0.00243	0.00038	1'98	2
53'	5753.28876	132.85675	3.53833	-1.02265	0.09252	-0.08169	-0.00430	0.00243	0.00038	1'99	1
54'	5755.76514	132.99688	3.54369	-1.02438	0.09271	-0.08186	-0.00431	0.00244	0.00038		
55'	5758.22414	133.13722	3.54906	-1.02610	0.09290	-0.08204	-0.00432	0.00245	0.00038		
56'	5760.69575	133.27776	3.55444	-1.02782	0.09308	-0.08221	-0.00433	0.00245	0.00038		
57'	5763.16997	133.41850	3.55983	-1.02955	0.09327	-0.08239	-0.00434	0.00246	0.00038		
58'	5765.64682	133.55945	3.56523	-1.03129	0.09346	-0.08256	-0.00435	0.00246	0.00038		
59'	5768.12629	133.70060	3.57064	-1.03302	0.09365	-0.08274	-0.00436	0.00247	0.00038		
60'	5770.60838	133.84196	3.57606	-1.03476	0.09384	-0.08292	-0.00438	0.00248	0.00038		

Iloczyn długości linji geodezyjnej przez COSINUS azymutu X

$X_m = (\Delta P)\Delta\varphi + (\Delta K^3)\Delta K^2 + (\Delta\varphi^2)\Delta\varphi^2 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcznych sek. ΔK przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek łuku

$\varphi = 48$	$(\Delta\varphi)$	(ΔK^2)	$(\Delta\varphi^2)$	$(\Delta\varphi\Delta K^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta K^2)$	(ΔK^4)
0'	308827.263	3733.786	74.814	- 146.109	- 0.217	- 5.713	- 0.085
1'	308828.161	3733.561	74.809	- 146.250	- 0.219	- 5.713	- 0.086
2'	308829.059	3733.334	74.805	- 146.390	- 0.220	- 5.712	- 0.086
3'	308829.956	3733.106	74.801	- 146.531	- 0.221	- 5.712	- 0.087
4'	308830.854	3732.877	74.797	- 146.671	- 0.223	- 5.712	- 0.087
5'	308831.751	3732.647	74.792	- 146.812	- 0.224	- 5.712	- 0.088
6'	308832.649	3732.415	74.788	- 146.953	- 0.226	- 5.711	- 0.088
7'	308833.546	3732.182	74.783	- 147.093	- 0.227	- 5.711	- 0.088
8'	308834.444	3731.948	74.779	- 147.234	- 0.228	- 5.711	- 0.089
9'	308835.341	3731.713	74.775	- 147.374	- 0.230	- 5.710	- 0.089
10'	308836.238	3731.476	74.770	- 147.515	- 0.231	- 5.710	- 0.090
11'	308837.135	3731.238	74.766	- 147.655	- 0.233	- 5.710	- 0.090
12'	308838.032	3730.999	74.761	- 147.796	- 0.234	- 5.709	- 0.090
13'	308838.930	3730.758	74.757	- 147.936	- 0.235	- 5.709	- 0.091
14'	308839.827	3730.517	74.752	- 148.077	- 0.237	- 5.709	- 0.091
15'	308840.724	3730.274	74.747	- 148.217	- 0.238	- 5.708	- 0.092
16'	308841.621	3730.029	74.743	- 148.358	- 0.240	- 5.708	- 0.092
17'	308842.517	3729.784	74.738	- 148.498	- 0.241	- 5.708	- 0.093
18'	308843.414	3729.537	74.734	- 148.639	- 0.242	- 5.707	- 0.093
19'	308844.311	3729.289	74.729	- 148.779	- 0.244	- 5.707	- 0.093
20'	308845.208	3729.040	74.724	- 148.920	- 0.245	- 5.707	- 0.094
21'	308846.104	3728.789	74.719	- 149.060	- 0.247	- 5.706	- 0.094
22'	308847.001	3728.537	74.715	- 149.201	- 0.248	- 5.706	- 0.095
23'	308847.898	3728.284	74.710	- 149.341	- 0.250	- 5.706	- 0.095
24'	308848.794	3728.030	74.705	- 149.482	- 0.251	- 5.705	- 0.095
25'	308849.691	3727.774	74.700	- 149.622	- 0.252	- 5.705	- 0.096
26'	308850.587	3727.517	74.695	- 149.762	- 0.254	- 5.704	- 0.096
27'	308851.483	3727.259	74.691	- 149.903	- 0.255	- 5.704	- 0.097
28'	308852.380	3727.000	74.686	- 150.043	- 0.257	- 5.704	- 0.097
29'	308853.276	3726.739	74.681	- 150.184	- 0.258	- 5.703	- 0.098
30'	308854.172	3726.477	74.676	- 150.324	- 0.259	- 5.703	- 0.098
31'	308855.068	3726.214	74.671	- 150.464	- 0.261	- 5.703	- 0.098
32'	308855.964	3725.949	74.666	- 150.605	- 0.262	- 5.702	- 0.099
33'	308856.860	3725.683	74.661	- 150.745	- 0.264	- 5.702	- 0.099
34'	308857.756	3725.416	74.656	- 150.885	- 0.265	- 5.701	- 0.100
35'	308858.652	3725.148	74.651	- 151.026	- 0.266	- 5.701	- 0.100
36'	308859.548	3724.878	74.646	- 151.166	- 0.268	- 5.701	- 0.100
37'	308860.443	3724.608	74.640	- 151.306	- 0.269	- 5.700	- 0.101
38'	308861.339	3724.336	74.635	- 151.447	- 0.271	- 5.700	- 0.101
39'	308862.234	3724.062	74.630	- 151.587	- 0.272	- 5.700	- 0.102
40'	308863.130	3723.788	74.625	- 151.727	- 0.273	- 5.699	- 0.102
41'	308864.025	3723.512	74.620	- 151.867	- 0.275	- 5.699	- 0.103
42'	308864.921	3723.235	74.614	- 152.008	- 0.276	- 5.698	- 0.103
43'	308865.816	3722.956	74.609	- 152.148	- 0.278	- 5.698	- 0.103
44'	308866.712	3722.677	74.604	- 152.288	- 0.279	- 5.698	- 0.104
45'	308867.607	3722.396	74.598	- 152.428	- 0.280	- 5.697	- 0.104
46'	308868.502	3722.114	74.593	- 152.569	- 0.282	- 5.697	- 0.105
47'	308869.397	3721.830	74.588	- 152.709	- 0.283	- 5.696	- 0.105
48'	308870.292	3721.546	74.582	- 152.849	- 0.285	- 5.696	- 0.105
49'	308871.187	3721.260	74.577	- 152.989	- 0.286	- 5.696	- 0.106
50'	308872.082	3720.973	74.571	- 153.129	- 0.288	- 5.695	- 0.106
51'	308872.977	3720.684	74.566	- 153.270	- 0.289	- 5.695	- 0.107
52'	308873.871	3720.394	74.560	- 153.410	- 0.290	- 5.694	- 0.107
53'	308874.766	3720.103	74.555	- 153.550	- 0.292	- 5.694	- 0.108
54'	308875.661	3719.811	74.549	- 153.690	- 0.293	- 5.694	- 0.108
55'	308876.555	3719.518	74.544	- 153.830	- 0.295	- 5.693	- 0.108
56'	308877.450	3713.223	74.538	- 153.970	- 0.296	- 5.693	- 0.109
57'	308878.344	3718.927	74.532	- 154.110	- 0.297	- 5.693	- 0.109
58	308879.239	3718.630	74.527	- 154.250	- 0.299	- 5.692	- 0.110
59'	308880.133	3718.331	74.521	- 154.391	- 0.300	- 5.691	- 0.110
60'	308881.027	3718.032	74.515	154.531	- 0.302	- 5.691	- 0.110

Iloczyn długości linji geodezyjnej przez SINUS azymutu Y

$y_m = (\Delta\lambda)\Delta\lambda + (\Delta\varphi\Delta\lambda)\Delta\varphi\Delta\lambda + (\Delta\lambda^3)\Delta\lambda^3 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku

$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku

$\varphi = 48°$	$(\Delta\lambda)$	$(\Delta\varphi\Delta\lambda)$	$(\Delta\lambda^3)$	$(\Delta\varphi^2\Delta\lambda)$	$(\Delta\varphi\Delta\lambda^3)$	$(\Delta\varphi^3\Delta\lambda)$	Poprawka interpolacyjna dla wyrazu $\Delta\lambda$ K'	K
0'	207267.454	-11126.638	- 44.841	- 164.599	0.438	- 0.016		
1'	207200.686	-11129.584	- 44.850	- 164.547	0.441	- 0.016		
2'	207133.899	-11132.529	- 44.859	- 164.496	0.443	- 0.016		
3'	207067.095	-11135.473	- 44.868	- 164.445	0.446	- 0.016		
4'	207000.274	-11138.417	- 44.877	- 164.393	0.449	- 0.015		
5'	206933.434	-11141.359	- 44.886	- 164.342	0.451	- 0.015		
6'	206866.577	-11144.301	- 44.895	- 164.291	0.454	- 0.015		
7'	206799.703	-11147.241	- 44.904	- 164.239	0.457	- 0.015		
8'	206732.810	-11150.181	- 44.913	- 164.188	0.459	- 0.015		
9'	206665.901	-11153.120	- 44.922	- 164.137	0.462	- 0.015		
10'	206598.973	-11156.057	- 44.931	- 164.085	0.465	- 0.015		
11'	206532.028	-11158.994	- 44.939	- 164.034	0.467	- 0.015		
12'	206465.065	-11161.930	- 44.948	- 163.982	0.470	- 0.015		
13'	206398.085	-11164.865	- 44.957	- 163.931	0.473	- 0.015		
14'	206331.087	-11167.799	- 44.966	- 163.879	0.475	- 0.015		
15'	206264.071	-11170.732	- 44.975	- 163.828	0.478	- 0.015		
16'	206197.038	-11173.664	- 44.983	- 163.776	0.481	- 0.015		
17'	206129.987	-11176.596	- 44.992	- 163.725	0.483	- 0.015		
18'	206062.919	-11179.526	- 45.001	- 163.673	0.486	- 0.015		
19	205995.833	-11182.456	- 45.009	- 163.622	0.489	- 0.014		
20'	205928.729	-11185.384	- 45.018	- 163.570	0.491	- 0.014		
21'	205861.608	-11188.312	- 45.027	- 163.518	0.494	- 0.014		+ 0.001
22'	205794.469	-11191.238	- 45.035	- 163.467	0.497	- 0.014		
23'	205727.313	-11194.164	- 45.044	- 163.415	0.499	- 0.014		
24'	205660.140	-11197.089	- 45.052	- 163.364	0.502	- 0.014		
25'	205592.948	-11200.012	- 45.061	- 163.312	0.505	- 0.014	0'1	1
26'	205525.739	-11202.935	- 45.069	- 163.260	0.508	- 0.014	0'2	1
27'	205458.513	-11205.857	- 45.078	- 163.208	0.510	- 0.014	0'3	2
28'	205391.269	-11208.778	- 45.086	- 163.157	0.513	- 0.014	0'4	2
29'	205324.008	-11211.698	- 45.095	- 163.105	0.516	- 0.014	0'5	2
30'	205256.729	-11214.618	- 45.103	- 163.053	0.518	- 0.014	0'6	2
31'	205189.432	-11217.536	- 45.112	- 163.002	0.521	- 0.014	0'7	2
32'	205122.118	-11220.453	- 45.120	- 162.950	0.524	- 0.014	0'8	1
33'	205054.787	-11223.369	- 45.128	- 162.898	0.526	- 0.014	0'9	1
34'	204987.438	-11226.285	- 45.137	- 162.846	0.529	- 0.014	1'0	
35'	204920.071	-11229.199	- 45.145	- 162.794	0.532	- 0.014		
36'	204852.687	-11232.113	- 45.153	- 162.743	0.534	- 0.013		
37'	204785.286	-11235.026	- 45.162	- 162.691	0.537	- 0.013		
38'	204717.867	-11237.937	- 45.170	- 162.639	0.540	- 0.013		
39'	204650.431	-11240.848	- 45.178	- 162.587	0.543	- 0.013		
40'	204582.977	-11243.758	- 45.187	- 162.535	0.545	- 0.013		
41'	204515.506	-11246.667	- 45.195	- 162.483	0.548	- 0.013		
42'	204448.017	-11249.575	- 45.203	- 162.431	0.551	- 0.013		
43'	204380.511	-11252.482	- 45.211	- 162.379	0.553	- 0.013		
44'	204312.987	-11255.388	- 45.219	- 162.327	0.556	- 0.013		
45'	204245.446	-11258.293	- 45.227	- 162.276	0.559	- 0.013		
46'	204177.888	-11261.197	- 45.235	- 162.224	0.562	- 0.013		
47'	204110.312	-11264.100	- 45.244	- 162.172	0.564	- 0.013		
48'	204042.718	-11267.003	- 45.252	- 162.120	0.567	- 0.013		
49'	203975.108	-11269.904	- 45.260	- 162.068	0.570	- 0.013		
50'	203907.480	-11272.804	- 45.268	- 162.015	0.572	- 0.013		
51'	203839.834	-11275.704	- 45.276	- 161.963	0.575	- 0.012		
52'	203772.171	-11278.602	- 45.284	- 161.911	0.578	- 0.012		
53'	203704.491	-11281.500	- 45.292	- 161.859	0.581	- 0.012		
54'	203636.793	-11284.397	- 45.300	- 161.807	0.583	- 0.012		
55'	203569.078	-11287.292	- 45.308	- 161.755	0.586	- 0.012		
56'	203501.346	-11290.187	- 45.315	- 161.703	0.589	- 0.012		
57'	203433.596	-11293.081	- 45.323	- 161.651	0.591	- 0.012		
58'	203365.829	-11295.974	- 45.331	- 161.599	0.594	- 0.012		
59'	203298.044	-11298.866	- 45.339	- 161.546	0.597	- 0.012		
60'	203230.242	-11301.757	- 45.347	- 161.494	0.600	- 0.012		

AK

II Iloczyn długości linji geodezyjnej przez COSINUS azymutu X

$X_m = (\Delta\varphi)\Delta\varphi + (\Delta\lambda^2)\Delta\lambda^2 + (\Delta\varphi^2)\Delta\varphi^2 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku; $\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.

$\varphi = 49°$	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta\lambda^2)$	$(\Delta\lambda^4)$
0'	308 881. 027	3718. 032	74. 515	− 154. 530	− 0. 302	− 5. 691	− 0. 110
1'	308 881. 921	3717. 730	74. 510	− 154. 671	− 0. 303	− 5. 691	− 0. 111
2'	308 882. 815	3717. 428	74. 504	− 154. 811	− 0. 304	− 5. 690	− 0. 111
3'	308 883. 709	3717. 125	74. 498	− 154. 951	− 0. 306	− 5. 690	− 0. 112
4	308 884. 603	3716. 820	74. 492	− 155. 091	− 0. 307	− 5. 689	− 0. 112
5'	308 885. 497	3716. 514	74. 486	− 155. 231	− 0. 309	− 5. 689	− 0. 112
6'	308 886. 391	3716. 206	74. 480	− 155. 371	− 0. 310	− 5. 688	− 0. 113
7'	308 887. 285	3715. 898	74. 475	− 155. 511	− 0. 311	− 5. 688	− 0. 113
8'	308 888. 178	3715. 588	74. 469	− 155. 651	− 0. 313	− 5. 687	− 0. 114
9'	308 889. 072	3715. 277	74. 463	− 155. 791	− 0. 314	− 5. 687	− 0. 114
10'	308 889. 965	3714. 965	74. 457	− 155. 931	− 0. 316	− 5. 687	− 0. 115
11'	308 890. 859	3714. 651	74. 451	− 156. 071	− 0. 317	− 5. 686	− 0. 115
12'	308 891. 752	3714. 336	74. 445	− 156. 211	− 0. 318	− 5. 686	− 0. 115
13'	308 892. 645	3714. 020	74. 439	− 156. 351	− 0. 320	− 5. 685	− 0. 116
14'	308 893. 539	3713. 703	74. 433	− 156. 490	− 0. 321	− 5. 685	− 0. 116
15'	308 894. 432	3713. 384	74. 426	− 156. 630	− 0. 323	− 5. 684	− 0. 117
16'	308 895. 325	3713. 064	74. 420	− 156. 770	− 0. 324	− 5. 684	− 0. 117
17'	308 896 218	3712. 743	74. 414	− 156. 910	− 0. 325	− 5. 683	− 0. 117
18'	308 897. 111	3712. 420	74. 408	− 157. 050	− 0. 327	− 5. 683	− 0. 118
19'	308 898 004	3712 097	74. 402	− 157. 190	− 0. 328	− 5. 683	− 0. 118
20'	308 898. 896	3711. 772	74. 396	− 157. 330	− 0. 330	− 5. 682	− 0. 119
21'	308 899. 789	3711. 445	74. 389	− 157. 470	− 0. 331	− 5. 682	− 0. 119
22'	308 900. 682	3711. 118	74. 383	− 157. 609	− 0. 332	− 5. 681	− 0. 119
23'	308 901. 574	3710. 789	74. 377	− 157. 749	− 0. 334	− 5. 681	− 0. 120
24'	308 902. 467	3710. 459	74. 370	− 157. 889	− 0. 335	− 5. 680	− 0. 120
25	308 903. 359	3710. 128	74. 364	− 158. 029	− 0. 337	− 5. 680	− 0. 121
26'	308 904. 251	3709. 796	74. 358	− 158. 169	− 0. 338	− 5. 679	− 0. 121
27'	308 905. 144	3709. 462	74. 351	− 158. 308	− 0. 339	− 5. 679	− 0. 121
28'	308 906. 036	3709. 127	74. 345	− 158. 448	− 0. 341	− 5. 678	− 0. 122
29'	308 906. 928	3708. 791	74. 338	− 158. 588	− 0. 342	− 5. 678	− 0. 122
30'	308 907. 820	3708. 453	74. 332	− 158. 728	− 0. 344	− 5. 677	− 0. 123
31'	308 908. 712	3708. 114	74. 325	− 158. 867	− 0. 345	− 5. 677	− 0. 123
32'	308 909 604	3707. 774	74. 319	− 159. 007	− 0. 346	− 5. 676	− 0. 123
33'	308 910. 496	3707. 433	74. 312	− 159. 147	− 0. 348	− 5. 676	− 0. 124
34'	308 911. 387	3707. 090	74. 306	− 159. 287	− 0. 349	− 5. 675	− 0. 124
35'	308 912. 279	3706. 747	74. 299	− 159. 426	− 0. 351	− 5. 675	− 0. 125
36'	308 913. 171	3706. 402	74. 293	− 159. 566	− 0. 352	− 5. 674	− 0. 125
37'	308 914. 062	3706. 056	74. 286	− 159. 705	− 0. 354	− 5. 674	− 0. 125
38'	308 914. 953	3705. 708	74. 279	− 159 845	− 0. 355	− 5. 673	− 0. 126
39'	308 915. 845	3705. 359	74. 273	− 159. 985	− 0 356	− 5. 673	− 0. 126
40'	308 916. 736	3705. 009	74. 266	− 160. 124	− 0. 358	− 5. 672	− 0. 127
41'	308 917. 627	3704. 657	74. 259	− 160. 264	− 0. 359	− 5. 672	− 0. 127
42'	308 918 518	3704. 305	74. 252	− 160. 404	− 0. 360	− 5. 671	− 0 128
43'	308 919. 409	3703. 951	74 245	− 160. 543	− 0. 362	− 5. 671	− 0. 128
44'	308 920. 300	3703. 596	74. 239	− 160. 683	− 0 363	− 5. 670	− 0 128
45'	308 921. 191	3703. 240	74. 232	− 160. 822	− 0. 365	− 5. 670	− 0. 129
46	308 922. 082	3702. 882	74. 225	− 160. 962	− 0 366	− 5. 669	− 0. 129
47'	308 922. 972	3702. 523	74. 218	− 161. 101	− 0. 367	− 5. 669	− 0. 130
48	308 923. 863	3702 163	74. 211	− 161. 241	− 0. 369	− 5. 668	− 0. 130
49	308 924. 753	3701. 802	74. 204	− 161. 380	− 0. 370	− 5. 668	− 0 130
50'	308 925. 644	3701. 439	74. 197	− 161. 520	− 0. 372	− 5. 667	− 0. 131
51'	308 926. 534	3701. 075	74. 190	− 161. 659	− 0. 373	− 5. 667	− 0 131
52'	308 927. 424	3700. 710	74. 183	− 161. 799	− 0 374	− 5. 666	− 0. 132
53'	308 928. 314	3700. 344	74. 176	− 161. 938	− 0. 376	− 5. 666	− 0 132
54'	308 929. 204	3699. 976	74. 169	− 162. 078	− 0. 377	− 5. 665	− 0 132
55	308 930. 094	3699. 607	74. 162	− 162. 217	− 0. 379	− 5. 665	− 0. 133
56'	308 930. 984	3699. 237	74. 155	− 162. 356	− 0. 380	− 5. 664	− 0. 133
57'	308 931. 874	3698. 866	74. 148	− 162. 496	− 0. 381	− 5. 663	− 0. 134
58'	308 932. 764	3698 493	74. 140	− 162. 635	− 0 383	− 5. 663	− 0 134
59	308 933. 654	3698. 119	74. 133	− 162. 775	− 0. 384	− 5. 662	− 0. 134
60	308 934. 543	3697. 744	74. 126	− 162 914	− 0. 386	− 5. 662	− 0. 135

Iloczyn długości linji geodezyjnej przez SINUS azymutu Y

$Y_m \Delta\lambda \Delta\varphi\Delta\lambda \Delta\varphi^2\Delta\lambda \Delta\varphi\Delta\lambda^2 \Delta\lambda^3 \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.

φ 49°	$\Delta\lambda$	$\Delta\varphi\Delta\lambda$	$\Delta\lambda^3$	$\Delta\varphi^2\Delta\lambda$	$\Delta\varphi\Delta\lambda^2$	$\Delta\varphi^3\Delta\lambda$	Poprawka interpolacyjna dla wyrazu $\Delta\lambda$ K'	K
0'	203 230. 242	-11301. 757	- 45. 347	- 161. 494	0. 600	- 0. 012		
1'	203 162. 423	-11304. 647	- 45. 355	- 161. 442	0. 602	- 0. 012		
2'	203 094. 587	-11307. 536	- 45. 362	- 161. 390	0. 605	- 0. 012		
3'	203 026. 733	-11310. 424	- 45. 370	- 161. 338	0. 608	- 0. 012		
4'	202 958. 861	-11313. 312	- 45. 378	- 161. 285	0. 611	- 0. 012		
5'	202 890. 973	-11316. 198	- 45. 386	- 161. 233	0. 613	- 0. 012		
6'	202 823. 067	-11319. 083	- 45. 393	- 161. 181	0. 616	- 0. 012		
7'	202 755 144	-11321. 968	- 45. 401	- 161. 129	0. 619	- 0. 011		
8'	202 687. 203	-11324. 851	- 45. 409	- 161. 076	0. 621	- 0. 011		
9'	202 619. 246	-11327. 734	- 45. 416	- 161. 024	0. 624	- 0. 011		
10'	202 551. 271	-11330. 615	- 45. 424	- 160. 972	0. 627	- 0. 011		
11'	202 483. 278	-11333. 496	- 45. 431	- 160. 919	0. 630	- 0. 011		
12'	202 415. 269	-11336. 376	- 45. 439	- 160 867	0. 632	- 0. 011		
13'	202 347. 242	-11339. 254	- 45. 447	- 160. 815	0. 635	- 0. 011		
14'	202 279. 198	-11342. 132	- 45. 454	- 160. 762	0. 638	- 0. 011		
15'	202 211. 136	-11345. 009	- 45. 462	- 160. 710	0. 641	- 0. 011		
16'	202 143. 058	-11347. 885	- 45. 469	- 160. 657	0. 643	- 0. 011		
17'	202 074. 962	-11350. 760	- 45. 476	- 160. 605	0. 646	- 0. 011		
18'	202 006. 848	-11353. 634	- 45. 484	- 160. 552	0. 649	- 0. 011		
19'	201 938. 718	-11356. 507	- 45. 491	- 160. 500	0. 652	- 0. 011		
20'	201 870. 570	-11359. 379	- 45. 499	- 160. 448	0. 654	- 0. 011		
21'	201 802. 406	-11362. 250	- 45. 506	- 160. 395	0. 657	- 0. 011		+ 0001'
22'	201 734. 223	-11365. 120	- 45. 513	- 160. 343	0. 660	- 0. 010		
23'	201 666. 024	-11367. 990	- 45. 521	- 160. 290	0. 663	- 0. 010		
24'	201 597. 808	-11370. 858	- 45. 528	- 160. 237	0. 665	- 0. 010		
25'	201 529. 574	-11373. 725	- 45. 535	- 160. 185	0. 668	- 0. 010	0.1	1
26'	201 461. 323	-11376. 592	- 45. 543	- 160. 132	0. 671	- 0. 010	0.2	1
27'	201 393. 055	-11379. 457	- 45. 550	- 160. 080	0. 674	- 0. 010	0.3	2
28'	201 324. 769	-11382. 322	- 45. 557	- 160. 027	0. 676	- 0. 010	0.4	2
29'	201 256. 467	-11385. 185	- 45. 564	- 159. 975	0. 679	- 0. 010	0.5	2
30'	201 188. 147	-11388. 048	- 45. 571	- 159. 922	0. 682	- 0. 010	0.6	2
31'	201 119. 810	-11390. 910	- 45. 579	- 159 869	0. 685	- 0. 010	0.7	2
32'	201 051 456	-11393. 771	- 45. 586	- 159. 817	0. 687	- 0. 010	0.8	1
33'	200 983. 085	-11396. 630	- 45. 593	- 159. 764	0. 690	- 0. 010	0.9	1
34'	200 914. 697	-11399. 489	- 45. 600	- 159. 711	0. 693	- 0. 010	1.0	
35'	200 846. 291	-11402. 347	- 45. 607	- 159. 658	0. 696	- 0. 010		
36'	200 777. 868	-11405. 204	- 45. 614	- 159. 606	0. 698	- 0 010		
37'	200 709. 429	-11408 060	- 45. 621	- 159 553	0. 701	- 0 010		
38'	200 640 972	-11410. 915	- 45 628	- 159. 500	0. 704	- 0 009		
39'	200 572. 498	-11413. 769	- 45. 635	- 159. 447	0. 707	- 0 009		
40'	200 504. 006	-11416. 622	- 45. 642	- 159. 395	0. 709	- 0 009		
41'	200 435. 498	-11419. 474	- 45. 649	- 159. 342	0. 712	- 0 009		
42'	200 366. 973	-11422. 325	- 45. 656	- 159. 289	0. 715	- 0 009		
43'	200 298. 430	-11425. 176	- 45. 663	- 159. 236	0. 718	- 0 009		
44'	200 229. 871	-11428. 025	- 45. 670	- 159. 183	0. 721	- 0 009		
45'	200 161. 294	-11430. 873	- 45 677	- 159. 131	0. 723	- 0 009		
46'	200 092. 700	-11433 721	- 45 683	- 159 078	0. 726	- 0 009		
47'	200 024. 089	-11436. 567	- 45 690	- 159. 025	0 729	- 0 009		
48'	199 955. 461	-11439. 413	- 45. 697	- 158. 972	0 732	- 0 009		
49'	199 886. 816	-11442. 257	- 45. 704	- 158. 919	0. 734	- 0 009		
50'	199 818. 154	-11445. 101	- 45 711	- 158 866	0 737	- 0 009		
51'	199 749. 475	-11447. 943	- 45. 717	- 158. 813	0 740	- 0 009		
52'	199 680. 779	-11450. 785	- 45. 724	- 158 760	0 743	- 0 009		
53'	199 612. 066	-11453. 626	- 45 731	- 158 707	0 746	- 0 009		
54'	199 543. 335	-11456 466	- 45. 737	- 158. 654	0. 748	- 0. 008		
55'	199 474. 588	-11459. 304	- 45. 744	- 158. 601	0 751	- 0 008		
56'	199 405. 824	-11462. 142	- 45. 751	- 158 548	0 754	- 0 008		
57'	199 337. 042	-11464. 979	- 45. 757	- 158. 495	0. 757	- 0 008		
58'	199 268. 244	-11467. 815	- 45. 764	- 158. 442	0. 759	- 0 008		
59'	199 199. 429	-11470. 650	- 45. 770	- 158. 389	0. 762	- 0 008		
60'	199 130. 596	-11473. 484	- 45. 777	- 158 336	0. 765	- 0 008		

A. K.

Iloczyn długości linji geodezyjnej przez COSINUS azymutu X

$X_m = (\Delta\varphi)\Delta\varphi + (\Delta\varphi^2)\Delta\varphi^2 + (\Delta\varphi^3)\Delta\varphi^3 \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku

$\varphi = 50°$	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^2)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta\lambda^2)$	$(\Delta\lambda^4)$
0'	308 934. 543	3697. 744	74. 126	- 162. 914	- 0. 386	- 5. 662	- 0. 135
1'	308 935. 433	3697. 368	74. 119	- 163. 053	- 0. 387	- 5. 661	- 0. 135
2'	308 936. 322	3696. 990	74. 111	- 163. 193	- 0. 389	- 5. 661	- 0. 136
3'	308 937. 211	3696. 611	74. 104	- 163. 332	- 0 390	- 5. 660	- 0. 136
4'	308 938. 100	3696. 231	74. 097	- 163. 471	- 0. 391	- 5. 660	- 0. 136
5'	308 938. 990	3695. 849	74. 089	- 163. 610	- 0. 393	- 5. 659	- 0. 137
6'	308 939. 879	3695. 467	74. 082	- 163. 750	- 0. 394	- 5. 659	- 0. 137
7'	308 940. 767	3695. 083	74. 075	- 163. 889	- 0 396	- 5. 658	- 0. 138
8'	308 941. 656	3694. 698	74. 067	- 164 028	- 0 397	- 5. 658	- 0. 138
9'	308 942. 545	3694 311	74. 060	- 164. 167	- 0. 398	- 5. 657	- 0. 138
10'	308 943. 434	3693. 924	74. 052	- 164. 307	- 0. 400	- 5. 656	- 0. 139
11'	308 944. 322	3693. 535	74. 045	- 164. 446	- 0 401	- 5. 656	- 0. 139
12'	308 945. 211	3693. 145	74. 037	- 164. 585	- 0. 402	- 5. 655	- 0. 140
13'	308 946. 099	3692. 753	74. 029	- 164. 724	- 0. 404	- 5. 655	- 0. 140
14'	308 946. 987	3692 360	74. 022	- 164. 863	- 0 405	- 5. 654	- 0. 140
15'	308 947. 876.	3691. 966	74. 014	- 165. 002	- 0. 407	- 5. 654	- 0. 141
16'	308 948. 764	3691. 571	74. 007	- 165. 142	- 0 408	- 5. 653	- 0. 141
17'	308 949. 652	3691. 175	73. 999	- 165. 281	- 0. 409	- 5 652	- 0. 142
18'	308 950. 540	3690. 777	73. 991	- 165. 420	- 0 411	- 5. 652	- 0. 142
19'	308 951. 428	3690. 378	73. 984	- 165. 559	- 0. 412	- 5. 651	- 0. 142
20'	308 952. 315	3689. 978	73. 976	- 165. 698	- 0 414	- 5. 651	- 0. 143
21'	308 953. 203	3689. 577	73. 968	- 165. 837	- 0. 415	- 5. 650	- 0. 143
22'	308 954. 091	3689 174	73. 960	- 165. 976	- 0. 416	- 5. 650	- 0. 144
23'	308 954. 978	3688. 770	73. 952	- 166. 115	- 0 418	- 5. 649	- 0. 144
24'	308 955. 866	3688 365	73. 945	- 166. 254	- 0. 419	- 5. 648	- 0. 144
25'	308 956. 753	3687. 958	73. 937	- 166. 393	- 0. 421	- 5. 648	- 0. 145
26'	308 957. 640	3687 551	73. 929	- 166. 532	- 0. 422	- 5. 647	- 0. 145
27'	308 958. 527	3687. 142	73. 921	- 166. 671	- 0. 423	- 5. 647	- 0. 146
28'	308 959. 414	3686. 732	73. 913	- 166. 810	- 0. 425	- 5. 646	- 0. 146
29'	308 960. 301	3686. 320	73. 905	- 166. 949	- 0. 426	- 5. 645	- 0. 146
30'	308 961. 188	3685. 908	73. 897	- 167. 088	- 0. 428	- 5. 645	- 0. 147
31'	308 962. 075	3685. 494	73. 889	- 167. 227	- 0. 429	- 5. 644	- 0. 147
32'	308 962 961	3685. 079	73. 881	- 167 366	- 0. 430	- 5. 644	- 0 148
33'	308 963. 848	3684. 662	73. 873	- 167. 504	- 0. 432	- 5. 643	- 0 148
34'	308 964. 734	3684. 244	73. 865	- 167. 643	- 0. 433	- 5. 642	- 0. 148
35'	308 965. 621	3683. 826	73. 857	- 167. 782	- 0. 435	- 5. 642	- 0. 149
36'	308 966. 507	3683. 405	73. 849	- 167. 921	- 0. 436	- 5. 641	- 0. 149
37'	308 967. 393	3682. 984	73. 840	- 168 060	- 0. 437	- 5. 641	- 0. 150
38'	308 968. 279	3682. 561	73. 832	- 168. 199	- 0 439	- 5. 640	- 0. 150
39'	308 969. 165	3682. 137	73. 824	- 168 337	- 0. 440	- 5. 639	- 0. 150
40'	308 970. 051	3681. 712	73. 816.	- 168. 476	- 0. 442	- 5 639	- 0. 151
41'	308 970. 936	3681. 286	73. 807	- 168. 615	- 0. 443	- 5. 638	- 0. 151
42'	308 971. 822	3680. 858	73. 799	- 168. 754	- 0. 444	- 5. 637	- 0. 151
43'	308 972. 708	3680. 429	73. 791	- 168. 892	- 0. 446	- 5. 637	- 0. 152
44'	308 973. 593	3679. 999	73. 782	- 169. 031	- 0. 447	- 5. 636	- 0. 152
45'	308 974 478	3679 568	73. 774	- 169. 170	- 0. 449	- 5. 636	- 0. 153
46'	308 975. 364	3679. 135	73. 766	- 169. 308	- 0. 450	- 5. 635	- 0. 153
47'	308 976. 249	3678. 701	73. 757	- 169. 447	- 0. 451	- 5 634	- 0. 153
48'	308 977. 134	3678 266	73. 749	- 169. 586	- 0. 453	- 5. 634	- 0. 154
49'	308 978 019	3677 830	73. 740	- 169. 724	- 0. 454	- 5. 633	- 0 154
50'	308 978. 904	3677. 392	73. 732	- 169. 863	- 0. 456	- 5. 632	- 0. 155
51'	308 979. 788	3676. 953	73. 723	- 170. 002	- 0. 457	- 5. 632	- 0. 155
52'	308 980. 673	3676. 513	73. 715	- 170. 140	- 0. 458	- 5 631	- 0. 155
53'	308 981 557	3676 072	73. 706	- 170. 279	- 0. 460	- 5. 630	- 0. 156
54'	308 982. 442	3675. 629	73. 698	- 170. 417	- 0. 461	- 5. 630	- 0. 156
55'	308 983. 326	3675. 185	73. 689	- 170. 556	- 0. 462	- 5. 629	- 0. 157
56'	308 984. 210	3674. 740	73. 680	- 170. 694	- 0. 464	- 5 629	- 0. 157
57'	308 985. 094	3674. 294	73 672	- 170 833	- 0. 465	- 5. 628	- 0 157
58'	308 985. 978	3673. 846	73. 663	- 170. 971	- 0. 467	- 5. 627	- 0 158
59'	308 986. 862	3673 397	73. 654	- 171. 110	- 0. 468	- 5. 627	- 0 158
60'	308 987. 746	3672. 947	73. 646	- 171. 248	- 0. 470	- 5 626	- 0. 158

Iloczyn długości linji geodezyjnej przez SINUS azymutu Y

$y_m = (\Delta\lambda)\Delta\lambda - (\Delta\varphi\Delta\lambda)\Delta\varphi\Delta\lambda + (\Delta\lambda^3)\Delta\lambda^3 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku

φ 50°	$(\Delta\lambda)$	$(\Delta\varphi\Delta\lambda)$	$(\Delta\lambda^3)$	$(\Delta\varphi^2\Delta\lambda)$	$(\Delta\varphi\Delta\lambda^3)$	$(\Delta\varphi^3\Delta\lambda)$	Poprawka interpolacyjna dla wyrazu $\Delta\lambda$	
							K'	Q·
0'	199 130. 596.	- 11 473. 484	- 45. 777	- 158. 336	0. 765	- 0. 008		
1'	199 061. 747	- 11 476. 317	- 45. 783	- 158. 283	0. 768	- 0. 008		
2'	198 992. 881	- 11 479. 149	- 45. 790	- 158. 230	0. 771	- 0. 008		
3'	198 923. 997	- 11 481. 980	- 45. 796	- 158. 177	0. 773	- 0. 008		
4'	198 855. 097	- 11 484. 810	- 45. 803	- 158. 124	0. 776	- 0. 008		
5'	198 786. 179	- 11 487. 640	- 45. 809	- 158. 070	0. 779	- 0. 008		
6'	198 717. 245	- 11 490. 468	- 45. 816	- 158. 017	0. 782	- 0. 008		
7'	198 648. 294	- 11 493. 295	- 45. 822	- 157. 964	0. 785	- 0. 008		
8'	198 579. 326	- 11 496. 122	- 45. 828	- 157. 911	0. 787	- 0. 008		
9'	198 510. 340	- 11 498. 947	- 45. 835	- 157. 858	0. 790	- 0. 007		
10'	198 441. 338	- 11 501. 771	- 45. 841	- 157. 804	0. 793	- 0. 007		
11'	198 372. 319	- 11 504. 595	- 45. 847	- 157. 751	0 796	- 0. 007		
12'	198 303. 283	- 11 507. 417	- 45. 853	- 157. 698	0. 798	- 0. 007		
13'	198 234. 230	- 11 510. 239	- 45. 860	- 157. 645	0. 801	- 0. 007		
14'	198 165. 160	- 11 513. 059	- 45. 866	- 157. 591	0. 804	- 0. 007		
15'	198 096. 073	- 11 515. 879	- 45. 872	- 157. 538	0. 807	- 0. 007		
16'	198 026. 970	- 11 518. 698	- 45. 878	- 157. 485	0. 810	- 0. 007		
17'	197 957. 849	- 11 521. 515	- 45. 885	- 157. 431	0. 812	- 0. 007		
18'	197 888. 712	- 11 524. 332	- 45. 891	- 157. 378	0. 815	- 0. 007		
19'	197 819. 557	- 11 527. 148	- 45. 897	- 157. 325	0. 818	- 0. 007		
20'	197 750. 386	- 11 529. 963	- 45. 903	- 157. 271	0. 821	- 0. 007		
21'	197 681. 198	- 11 532. 776	- 45. 909	- 157. 218	0. 824	- 0. 007		·1000+
22'	197 611. 993	- 11 535. 589	- 45. 915	- 157. 165	0. 827	- 0. 007		
23'	197 542. 771	- 11 538. 401	- 45. 921	- 157. 111	0. 829	- 0. 007		
24'	197 473. 532	- 11 541. 212	- 45. 927	- 157. 058	0. 832	- 0. 007		
25'	197 404. 276.	- 11 544. 022	- 45. 933	- 157. 004	0. 835	- 0. 006	0.1	1
26'	197 335. 003	- 11 546. 831	- 45. 939	- 156. 951	0. 838	- 0. 006	0.2	1
27'	197 265. 714	- 11 549. 639	- 45. 945	- 156. 897	0. 841	- 0. 006	0.3	2
28'	197 196. 408	- 11 552. 446	- 45 951	- 156. 844	0. 843	- 0. 006	0.4	2
29'	197 127. 085	- 11 555. 252	- 45. 957	- 156. 790	0 846	- 0. 006	0.5	2
30'	197 057. 745	- 11 558. 057	- 45. 963	- 156. 737	0. 849	- 0. 006.	0.6	2
31'	196 988 388	- 11 560. 862	- 45. 968	- 156 683	0. 852	- 0. 006	0.7	2
32'	196 919. 014	- 11 563. 665	- 45. 974	- 156. 630	0. 855	- 0. 006	0.8	1
33'	196 849. 624	- 11 566. 467	- 45. 980	- 156. 576	0. 857	- 0. 006	0.9	1
34'	196 780. 217	- 11 569. 268	- 45. 986	- 156. 523	0. 860	- 0. 006	1.0	
35'	196 710. 793	- 11 572. 069	- 45. 992	- 156. 469	0. 863	- 0. 006		
36'	196 641. 352	- 11 574. 868	- 45. 997	- 156. 415	0. 866	- 0 006		
37'	196 571. 894	- 11 577. 667	- 46. 003	- 156. 362	0 869	- 0 006		
38'	196 502. 420	- 11 580. 464	- 46. 009	- 156. 308	0. 872	- 0. 006		
39'	196 432. 929	- 11 583. 260	- 46. 015	- 156. 254	0. 874	- 0. 005		
40'	196 363. 421	- 11 586. 056	- 46. 020	- 156. 201	0. 877	- 0. 005		
41'	196 293. 896	- 11 588. 850	- 46. 026	- 156. 147	0. 880	- 0. 005		
42'	196 224. 354	- 11 591. 644	- 46. 031	- 156. 093	0. 883	- 0. 005		
43'	196 154. 796	- 11 594. 437	- 46. 037	- 156. 040	0. 886	- 0. 005		
44'	196 085. 221	- 11 597. 228	- 46. 043	- 155. 986	0. 889	- 0. 005		
45'	196 015. 629	- 11 600. 019	- 46. 048	- 155. 932	0. 891	- 0. 005		
46'	195 946. 020	- 11602. 808	- 46. 054	- 155. 878	0. 894	- 0. 005		
47'	195 876. 395	- 11 605. 597	- 46. 059	- 155. 825	0. 897	- 0 005		
48'	195 806. 754	- 11 608. 385	- 46. 065	- 155. 771	0. 900	- 0. 005		
49'	195 737. 095	- 11 611. 172	- 46. 070	- 155. 717	0. 903	- 0. 005		
50'	195 667 420	- 11 613. 957	- 46. 076.	- 155. 663	0. 905	- 0. 005		
51'	195 597. 729	- 11 616. 742	- 46. 081	- 155. 609	0. 908	- 0. 005		
52'	195 528. 021	- 11 619. 526	- 46. 086	- 155. 556	0. 911	- 0. 005		
53	195 458. 296	- 11 622. 309	- 46. 092	- 155. 502	0. 914	- 0. 005		
54'	195 388. 554	- 11625. 091	- 46. 087	- 155. 448	0. 917	- 0. 005		
55'	195318. 795	- 11627. 872	- 46. 102	- 155. 394	0. 920	- 0. 004		
56'	195 249. 020	- 11630. 652	- 46. 108	- 155. 340	0. 922	- 0. 004		
57'	195 179. 227	- 11633. 431	- 46. 113	- 155. 286	0. 925	- 0 004		
58'	195 109. 417	- 11636. 209	- 46. 118	- 155 232	0. 928	- 0. 004		
59'	195 039. 591	- 11638 986	- 46. 123	- 155. 178	0. 931	- 0. 004		
60'	194 969. 748	- 11641. 762	- 46. 129	- 155. 124	0. 934	- 0. 004		

A.K.

II Iloczyn długości linji geodezyjnej przez COSINUS azymutu X

$x_m = (\Delta\varphi)\Delta\varphi + (\Delta\lambda^2)\Delta\lambda^2 + (\Delta\varphi^3)\Delta\varphi^3 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku

$\varphi = 51°$	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta\lambda^2)$	$(\Delta\lambda^4)$
0'	308 987. 746.	3672. 947	73. 646	- 171. 248	- 0. 470	- 5. 626	- 0. 158
1'	308 988. 630	3672. 496	73. 637	- 171. 387	- 0. 471	- 5. 625	- 0. 159
2'	308 989. 514	3672. 043	73. 628	- 171. 525	- 0. 472	- 5. 625	- 0. 159
3'	308 990. 397	3671. 590	73. 619	- 171. 663	- 0. 474	- 5. 624	- 0. 160
4'	308 991. 280	3671. 135	73. 610	- 171. 802	- 0. 475	- 5. 623	- 0. 160
5'	308 992. 164	3670. 678	73. 602	- 171. 940	- 0. 477	- 5. 623	- 0. 160
6'	308 993. 047	3670. 221	73. 593	- 172. 078	- 0. 478	- 5. 622	- 0. 161
7'	308 993. 930	3669. 762	73. 584	- 172. 217	- 0. 479	- 5. 621	- 0. 161
8'	308 994. 813	3669. 302	73. 575	- 172. 355	- 0. 481	- 5. 621	- 0. 162
9	308 995. 696	3668. 841	73. 566	- 172. 493	- 0. 482	- 5. 620	- 0. 162
10'	308 996. 578	3668. 378	73. 557	- 172. 631	- 0. 483	- 5. 619	- 0. 163
11'	308 997. 461	3667. 914	73. 548	- 172. 770	- 0. 485	- 5. 619	- 0. 163
12'	308 998. 344	3667. 449	73. 539	- 172. 908	- 0. 486	- 5. 618	- 0. 163
13'	308 999. 226	3666. 983	73. 530	- 173. 046	- 0. 488	- 5. 617	- 0. 163
14'	309 000. 108	3666. 516	73. 521	- 173. 184	- 0. 489	- 5. 616	- 0. 164
15'	309 000 990	3666. 047	73. 512	- 173. 323	- 0. 490	- 5. 616	- 0. 164
16'	309 001. 873	3665. 577	73. 502	- 173. 461	- 0. 492	- 5. 615	- 0. 165
17'	309 002. 755	3665. 106	73. 493	- 173. 599	- 0. 493	- 5. 614	- 0. 165
18'	309 003. 636	3664. 633	73. 484	- 173. 737	- 0. 495	- 5. 614	- 0. 165
19'	309 004. 518	3664. 160	73. 475	- 173. 875	- 0. 496	- 5. 613	- 0. 166
20	309 005. 400	3663. 685	73. 466	- 174. 013	- 0. 497	- 5. 612	- 0. 166
21	309 006. 281	3663. 209	73. 456	- 174. 151	- 0 499	- 5. 612	- 0. 167
22'	309 007. 163	3662. 731	73. 447	- 174. 289	- 0. 500	- 5. 611	- 0. 167
23'	309 008. 044	3662. 253	73. 438	- 174. 428	- 0. 502	- 5. 610	- 0. 167
24'	309 008. 925	3661. 773	73. 428	- 174. 566	- 0. 503	- 5. 610	- 0. 168
25'	309 009. 806	3661. 292	73. 419	- 174. 704	- 0. 504	- 5. 609	- 0. 168
26'	309 010. 687	3660. 809	73. 410	- 174. 842	- 0. 506	- 5. 608	- 0. 168
27'	309 011. 568	3660. 325	73 400	- 174. 980	- 0. 507	- 5. 607	- 0. 169
28'	309 012. 449	3659. 841	73. 391	- 175. 118	- 0. 509	- 5. 607	- 0. 169
29'	309 013. 329	3659. 355	73. 381	- 175. 255	- 0. 510	- 5. 606	- 0. 170
30'	309 014. 210	3658. 867	73. 372.	- 175. 393	- 0. 511	- 5. 605	- 0. 170
31'	309 015. 090	3658. 379	73. 362	- 175. 531	- 0. 513	- 5. 605	- 0. 170
32'	309 015. 971	3657. 889	73. 353	- 175. 669	- 0. 514	- 5. 604	- 0. 171
33'	309 016. 851	3657. 398	73. 343	- 175. 807	- 0. 515	- 5. 603	- 0. 171
34'	309 017. 731	3656. 905	73. 334	- 175. 945	- 0. 517	- 5. 602	- 0. 171
35'	309 018. 611	3656. 412	73. 324	- 176. 083	- 0. 518	- 5. 602	- 0. 172
36'	309 019. 491	3655. 917	73. 314	- 176. 221	- 0. 520	- 5. 601	- 0. 172
37'	309 020. 370	3655. 421	73. 305	- 176. 358	- 0. 521	- 5. 600	- 0. 173
38'	309 021. 250	3654. 924	73. 295	- 176. 496	- 0. 522	- 5. 599	- 0. 173
39'	309 022. 130	3654. 425	73. 285	- 176. 634	- 0. 524	- 5. 599	- 0. 173
40'	309 023. 009	3653. 926	73. 275	- 176. 772	- 0. 525	- 5. 598	- 0. 174
41'	309 023. 888	3653. 425	73. 266	- 176. 909	- 0. 527	- 5. 597	- 0. 174
42'	309 024. 767	3652. 922	73. 256	- 177. 047	- 0. 528	- 5. 597	- 0. 175
43'	309 025. 646	3652. 419	73. 246	- 177. 185	- 0. 529	- 5. 596	- 0. 175
44'	309 026. 525	3651. 914	73. 236	- 177. 323	- 0. 531	- 5. 595	- 0. 175
45'	309 027. 404	3651. 408	73. 226	- 177. 460	- 0. 532	- 5. 594	- 0. 176
46'	309 028. 283	3650. 901	73. 216	- 177. 598	- 0. 534	- 5. 594	- 0. 176
47'	309 029. 161	3650. 393	73. 207	- 177. 735	- 0. 535	- 5. 593	- 0. 176
48'	309 030. 039	3649. 883	73. 197	- 177. 873	- 0. 536	- 5. 592	- 0. 177
49'	309 030. 918	3649. 372	73. 187	- 178. 011	- 0 538	- 5. 591	- 0. 177
50	309 031. 796	3648. 860	73. 177	- 178. 148	- 0. 539	- 5. 591	- 0. 178
51'	309 032. 674	3648. 347	73. 167	- 178. 286	- 0. 540	- 5. 590	- 0. 178
52'	309 033. 552	3647. 832	73. 157	- 178. 423	- 0. 542	- 5. 589	- 0. 178
53'	309 034. 430	3647. 316	73. 146	- 178. 561	- 0. 543	- 5. 588	- 0. 179
54'	309 035. 307	3646. 799	73. 136	- 178. 698	- 0. 545	- 5. 588	- 0. 179
55'	309 036. 185	3646. 281	73. 126	- 178. 836	- 0. 546	- 5. 587	- 0. 180
56'	309 037. 063	3645. 762	73. 116	- 178. 973	- 0. 547	- 5. 586	- 0. 180
57'	309 037. 940	3645. 241	73. 106	- 179. 111	- 0. 549	- 5. 585	- 0. 180
58'	309 038. 817	3644. 719	73. 096	- 179. 248	- 0. 550	- 5. 584	- 0. 181
59'	309 039. 694	3644 196	73. 086	- 179. 385	- 0. 552	- 5. 584	- 0. 181
60'	309 040. 571	3643. 671	73. 075.	- 179. 523.	- 0. 553	- 5. 583	- 0. 181

Iloczyn długości linji geodezyjnej przez sinus azymutu Y

$Y_m = (\Delta\lambda)\Delta h + (\Delta\varphi\Delta\lambda)\Delta\varphi\Delta\lambda + (\Delta\lambda^3)\Delta\lambda^2 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku, $\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku

$\varphi = 51°$	$(\Delta\lambda)$	$(\Delta\varphi\Delta\lambda)$	$(\Delta\lambda^3)$	$(\Delta\varphi^2\Delta\lambda)$	$(\Delta\varphi\Delta\lambda^3)$	$(\Delta\varphi^3\Delta\lambda)$	Poprawka interpolacyjna do wyrazu $\Delta\lambda$	
							K'	2
0'	194 909. 748	-11641. 762	- 46. 129	- 155. 124	0. 934	- 0. 004		
1'	194 899. 886	-11644. 537	- 46. 134	- 155. 070	0. 937	- 0. 004		
2'	194 830. 008	-11647. 311	- 46. 139	- 155. 016	0. 939	- 0. 004		
3'	194 760. 114	-11650. 084	- 46. 144	- 154. 962	0. 942	- 0. 004		
4'	194 690. 204	-11652. 856	- 46. 149	- 154. 908	0. 945	- 0. 004		
5'	194 620. 278	-11655. 628	- 46. 154	- 154. 854	0. 948	- 0. 004		
6'	194 550. 335	-11658. 398	- 46. 160	- 154. 800	0. 951	- 0. 004		
7'	194 480. 376	-11661. 167	- 46. 165	- 154. 746	0. 954	- 0. 004		
8'	194 410. 400	-11663. 935	- 46. 170	- 154. 692	0. 957	- 0. 004		
9'	194 340. 409	-11666. 703	- 46. 175	- 154. 638	0. 959	- 0. 003		
10'	194 270. 401	-11669. 469	- 46. 180	- 154. 584	0. 962	- 0. 003		
11'	194 200. 377	-11672. 234	- 46. 185	- 154. 530	0. 965	- 0. 003		
12'	194 130. 337	-11674. 999	- 46. 190	- 154. 476	0. 968	- 0. 003		
13'	194 060. 280	-11677. 762	- 46. 195	- 154 422	0. 971	- 0. 003		
14'	193 990. 206	-11680. 525	- 46. 199	- 154. 367	0. 974	- 0. 003		
15'	193 920. 116	-11683. 286	- 46. 204	- 154. 313	0. 976	- 0. 003		
16'	193 850. 009	-11686. 046	- 46. 209	- 154. 259	0. 979	- 0 003		
17'	193 779. 885	-11688. 806	- 46. 214	- 154. 205	0 982	- 0. 003		
18'	193 709. 745	-11691. 565	- 46. 219	- 154. 151	0. 985	- 0 003		
19'	193 639. 587	-11694. 322	- 46. 224	- 154. 096	0. 988	- 0. 003		
20'	193 569. 414	-11697. 079	- 46. 228	- 154. 042	0. 991	- 0. 003		
21'	193 499. 223	-11699. 834	- 46. 233	- 153. 988	0. 994	- 0. 003		+0001+
22'	193 429. 016	-11702. 589	- 46. 238	- 153. 934	0. 996	- 0. 003		
23'	193 358. 792	-11705. 342	- 46. 243	- 153. 879	0. 999	- 0. 002		
24'	193 288. 551	-11708. 095	- 46. 247	- 153. 825	1. 002	- 0. 002		
25'	193 218. 295	-11710. 847	- 46. 252	- 153. 771	1. 005	- 0. 002	0'1	1
26'	193 148. 021	-11713. 597	- 46. 257	- 153. 716	1. 008	- 0. 002	0'2	1
27'	193 077. 731	-11716. 347	- 46. 261	- 153. 662	1. 011	- 0. 002	0'3	2
28'	193 007. 425	-11719. 096	- 46. 266	- 153. 608	1. 014	- 0. 002	0'4	2
29'	192 937. 102	-11721. 844	- 46. 270	- 153. 553	1. 016	- 0. 002	0'5	2
30'	192 866. 763	-11724. 590	- 46. 275	- 153. 499	1. 019	- 0. 002	0'6	2
31'	192 796. 407	-11727. 336	- 46. 279	- 153. 444	1. 022	- 0 002	0'7	2
32'	192 726. 035	-11730. 081	- 46. 284	- 153. 390	1. 025	- 0. 002	0'8	1
33'	192 655. 646	-11732. 825	- 46. 288	- 153. 336	1. 028	- 0. 002	0'9	1
34'	192 585. 241	-11735. 568	- 46. 293	- 153. 281	1. 031	- 0. 002	1'0	
35'	192 514. 819	-11738. 310	- 46. 297	- 153. 227	1. 034	- 0. 002		
36'	192 444. 381	-11741. 050	- 46. 302	- 153. 172	1. 036	- 0. 002		
37'	192 373. 927	-11743. 790	- 46. 306	- 153. 118	1. 039	- 0. 002		
38'	192 303. 456	-11746. 529	- 46. 310	- 153. 063	1. 042	- 0. 001		
39'	192 232. 968	-11749. 267	- 46. 315	- 153. 009	1. 045	- 0. 001		
40'	192 162. 465	-11752. 004	- 46. 319	- 152. 954	1. 048	- 0. 001		
41'	192 091. 944	-11754. 740	- 46. 323	- 152. 900	1. 051	- 0. 001		
42'	192 021. 408	-11757. 475	- 46. 328	- 152. 845	1. 054	- 0. 001		
43'	191 950. 854	-11760. 209	- 46. 332	- 152. 790	1. 057	- 0. 001		
44'	191 880. 285	-11762. 942	- 46. 336	- 152. 736	1. 059	- 0. 001		
45'	191 809. 699	-11765. 674	- 46. 340	- 152. 681	1 062	- 0. 001		
46'	191 739. 097	-11768. 405	- 46. 345	- 152. 627	1. 065	- 0. 001		
47'	191 668. 478	-11771. 135	- 46. 349	- 152. 572	1. 068	- 0. 001		
48'	191 597. 843	-11773. 864	- 46. 353	- 152. 517	1. 071	- 0. 001		
49'	191 527. 192	-11776. 592	- 46. 357	- 152. 463	1. 074	- 0. 001		
50'	191 456. 524	-11779. 319	- 46. 361	- 152. 408	1. 077	- 0. 001		
51'	191 385. 840	-11782. 046	- 46. 365	- 152. 353	1. 080	0. 000		
52'	191 315. 140	-11784. 771	- 46. 369	- 152. 298	1. 082	0. 000		
53'	191 244. 423	-11787 495	- 46. 373	- 152. 244	1. 085	0. 000		
54'	191 173. 690	-11790. 218	- 46. 377	- 152. 189	1. 088	0. 000		
55'	191 102. 940	-11792. 940	- 46. 381	- 152. 134	1. 091	0. 000		
56'	191 032. 175	-11795. 661	- 46. 385	- 152. 080	1. 094	0. 000		
57'	190 961. 392	-11798. 382	- 46. 389	- 152. 025	1. 097	0. 000		
58	190 890. 594	-11801. 101	- 46. 393	- 151. 970	1. 100	0. 000		
59'	190 819. 779	-11803. 819	- 46. 397	- 151. 915	1. 103	0. 000		
60'	190 748. 948	-11806. 536	- 46. 401	- 151. 860	1. 106	0. 000		

A.K

II Iloczyn długości linji geodezyjnej przez cosinus azymutu X

$x_m = (\Delta\varphi)\Delta\varphi + (\Delta\lambda^2)\Delta\lambda^2 + (\Delta\varphi^3)\Delta\varphi^3 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku. $\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.

$\varphi = 52°$	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^2)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta\lambda^2)$	$(\Delta\lambda^4)$
0′	309040. 571	3643. 671	73. 075	- 179. 523	- 0. 553	- 5. 583	- 0. 181
1′	309041. 448	3643. 145	73. 065	- 179. 660	- 0. 554	- 5. 582	- 0. 182
2′	309042. 325	3642. 618	73. 055	- 179. 798	- 0. 556	- 5. 581	- 0. 182
3′	309043. 201	3642. 090	73. 044	- 179. 935	- 0. 557	- 5. 581	- 0. 183
4′	309044. 078	3641. 561	73. 034	- 180. 072	- 0. 558	- 5. 580	- 0. 183
5′	309044. 954	3641. 030	73. 024	- 180. 209	- 0. 560	- 5. 579	- 0. 183
6′	309045. 830	3640. 498	73. 013	- 180. 347	- 0. 561	- 5. 578	- 0. 184
7′	309046. 706	3639. 965	73. 003	- 180. 484	- 0. 563	- 5. 577	- 0. 184
8′	309047. 582	3639. 431	72. 992	- 180. 621	- 0. 564	- 5. 577	- 0. 184
9′	309048. 458	3638. 895	72. 982	- 180. 758	- 0. 565	- 5. 576	- 0. 185
10′	309049. 334	3638. 359	72. 972	- 180. 895	- 0. 567	- 5. 575	- 0. 185
11′	309050. 209	3637. 821	72. 961	- 181. 033	- 0. 568	- 5. 574	- 0. 186
12′	309051. 085	3637. 281	72. 950	- 181. 170	- 0. 569	- 5. 573	- 0. 186
13′	309051. 960	3636 741	72. 940	- 181 307	- 0. 571	- 5. 573	- 0. 186
14′	309052. 835	3636 199	72 929	- 181. 444	- 0. 572	- 5. 572	- 0. 187
15′	309053. 711	3635. 656.	72. 919	- 181. 581	- 0. 574	- 5. 571	- 0. 187
16′	309054. 586	3635. 112	72. 908	- 181. 718	- 0. 575	- 5. 570	- 0. 187
17′	309055. 460	3634. 567	72. 897	- 181. 855	- 0. 576	- 5. 569	- 0. 188
18′	309056. 335	3634. 020	72. 887	- 181. 992	- 0. 578	- 5. 569	- 0. 188
19′	309057. 210	3633. 472	72. 876	- 182 129	- 0. 579	- 5. 568	- 0. 189
20′	309058. 084	3632. 923	72. 865	- 182. 266	- 0. 581	- 5. 567	- 0. 189
21′	309058. 958	3632. 373	72. 855	- 182. 403	- 0. 582	- 5. 566	- 0. 189
22′	309059. 833	3631. 821	72 844	- 182 540	- 0. 583	- 5. 565	- 0 190
23′	309060. 707	3631 268	72. 833	- 182. 677	- 0 585	- 5. 565	- 0. 190
24′	309061. 581	3630. 714	72. 822	- 182. 814	- 0. 586	- 5. 564	- 0. 190
25′	309062. 454	3630 159	72 811	- 182. 951	- 0 587	- 5. 563	- 0. 191
26′	309063. 328	3629. 602	72 800	- 183. 088	- 0. 589	- 5. 562	- 0. 191
27′	309064. 202	3629. 045	72. 789	- 183. 225	- 0. 590	- 5. 561	- 0. 191
28′	309065. 075	3628 486	72 778	- 183 361	- 0. 592	- 5. 560	- 0. 192
29′	309065. 948	3627. 925	72. 767	- 183. 498	- 0. 593	- 5. 560	- 0. 192
30′	309066. 821	3627. 364	72. 756	- 183. 635	- 0. 594	- 5. 559	- 0. 193
31′	309067. 694	3626. 801	72. 745	- 183. 772	- 0. 596	- 5. 558	- 0. 193
32′	309068. 567	3626. 237	72. 734	- 183. 908	- 0. 597	- 5. 557	- 0. 193
33′	309069. 440	3625. 672	72. 723	- 184. 045	- 0. 598	- 5. 556	- 0. 194
34′	309070. 313	3625. 106	72. 712	- 184. 182	- 0. 600	- 5. 555	- 0. 194
35′	309071. 185	3624. 538	72. 701	- 184. 318	- 0. 601	- 5. 555	- 0. 194
36	309072. 057	3623. 970	72. 690	- 184. 455	- 0 603	- 5. 554	- 0. 195
37′	309072. 930	3623 400	72. 679	- 184. 592	- 0. 604	- 5. 553	- 0. 195
38′	309073. 802	3622. 828	72. 668	- 184. 728	- 0. 605	- 5. 552	- 0. 196
39′	309074. 674.	3622. 256	72. 656	- 184. 865	- 0. 607	- 5. 551	- 0. 196
40′	309075. 545	3621. 682	72. 645	- 185. 002	- 0. 608	- 5. 550	0. 196
41′	309076. 417	3621. 107	72. 634	- 185. 138	- 0 609	- 5. 550	- 0. 197
42′	309077. 289	3620. 531	72. 623	- 185. 275	- 0. 611	- 5. 549	- 0. 197
43′	309078. 160	3619. 954	72. 611	- 185. 411	- 0. 612	- 5. 548	- 0. 197
44′	309079 031	3619. 375	72. 600	- 185. 548	- 0. 614	- 5. 547	- 0. 198
45′	309079. 902	3618. 795	72. 589	- 185. 684	- 0. 615	- 5. 546	- 0. 198
46	309080. 773	3618. 214	72. 577	- 185. 820	- 0. 616	- 5. 545	- 0. 199
47′	309081. 644	3617. 632	72. 566	- 185. 957	- 0. 618	- 5. 544	- 0. 199
48′	309082. 515	3617. 048	72. 554	- 186. 093	- 0. 619	- 5. 544	- 0. 199
49′	309083. 386	3616 464	72. 543	- 186. 230	- 0. 621	- 5. 543	- 0. 200
50′	309084. 256	3615. 878	72. 531	- 186 366	- 0. 622	- 5. 542	- 0. 200
51′	309085. 126	3615. 290	72. 520	- 186. 502	- 0. 623	- 5. 541	- 0. 200
52	309085 996	3614. 702	72. 508	- 186. 639	- 0. 625	- 5. 540	- 0. 201
53′	309086. 866	3614. 112	72. 497	- 186. 775	- 0. 626	- 5. 539	- 0. 201
54′	309087. 736	3613. 521	72. 485	- 186. 911	- 0. 627	- 5. 538	- 0. 201
55′	309088. 606	3612. 929	72. 474	- 187. 047	- 0. 629	- 5. 538	- 0. 202
56′	309089. 476	3612. 336	72. 462	- 187. 184	- 0. 630	- 5. 537	- 0. 202
57′	309090. 345	3611. 741	72. 450	- 187. 320	- 0. 631	- 5. 536	- 0. 202
58′	309091 215	3611. 146	72. 439	- 187. 456	- 0. 633	- 5. 535	- 0. 203
59′	309092. 084	3610. 549	72. 427	- 187. 592	- 0. 634	- 5. 534	- 0. 203
60′	309092 953	3609. 950	72. 415.	- 187. 728	- 0. 636.	- 5. 533	- 0. 204

Jloczyn długości linji geodezyjnej przez SINUS azymutu Y

$y_m = (\Delta\lambda) \Delta\lambda + (\Delta\varphi\Delta\lambda)\Delta\varphi\Delta\lambda + (\Delta\lambda^2)\Delta\lambda^2 + \ldots$ gdzie. $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.

φ. 52°	$(\Delta\lambda)$	$(\Delta\varphi\Delta\lambda)$	$(\Delta\lambda^2)$	$(\Delta\varphi^2\Delta\lambda)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3\Delta\lambda)$	Poprawka interpolacyjna dla wyrazu $\Delta\lambda$.	
							K	L
0'	190 748. 948	- 11 806. 536	- 46. 401	- 151. 860	1. 106	0. 000		
1'	190 678. 101	- 11 809. 253	- 46. 405	- 151. 805	1. 108	0. 000		
2'	190 607. 237	- 11 811. 968	- 46. 408	- 151. 751	1. 111	0. 000		
3'	190 536. 357	- 11 814. 682	- 46. 412	- 151. 696	1. 114	0. 000		
4'	190 465. 461	- 11 817. 395	- 46. 416	- 151. 641	1. 117	0. 000		
5'	190 394. 549	- 11 820. 106	- 46. 420	- 151. 586	1. 120	0. 000		
6'	190 323. 620	- 11 822. 819	- 46. 424	- 151. 531	1. 123	0. 001		
7'	190 252. 675	- 11 825. 529	- 46. 427	- 151. 476	1. 126	0. 001		
8'	190 181. 714	- 11 828. 239	- 46. 431	- 151. 421	1. 129	0. 001		
9'	190 110. 736	- 11 830. 947	- 46. 435	- 151. 366	1. 132	0. 001		
10'	190 039. 742	- 11 833. 654	- 46. 438	- 151. 311	1. 134	0. 001		
11'	189 968. 732	- 11 836. 361	- 46. 442	- 151. 256	1. 137	0. 001		
12'	189 897. 706	- 11 839. 066	- 46. 445	- 151. 201	1. 140	0. 001		
13'	189 826. 663	- 11 841. 770	- 46. 449	- 151. 146	1. 143	0. 001		
14'	189 755. 605	- 11 844. 474	- 46. 453	- 151. 091	1. 146	0. 001		
15'	189 684. 530	- 11 847. 176	- 46. 456	- 151. 036	1. 149	0. 001		
16'	189 613. 439	- 11 849. 877	- 46. 460	- 150. 981	1. 152	0. 001		
17'	189 542. 331	- 11 852. 578	- 46. 463	- 150. 926	1. 155	0. 001		
18'	189 471. 208	- 11 855. 277	- 46. 467	- 150. 871	1. 158	0. 001		
19'	189 400. 068	- 11 857. 976	- 46. 470	- 150. 816	1. 160	0. 001		
20'	189 328. 912	- 11 860. 673	- 46. 473	- 150. 761	1. 163	0. 001		
21'	189 257. 740	- 11 863. 370	- 46. 477	- 150 706	1. 166	0. 002		
22'	189 186. 551	- 11 866. 065	- 46. 480	- 150. 650	1. 169	0. 002		
23'	189 115. 347	- 11 868. 759	- 46. 484	- 150 595	1. 172	0. 002		
24'	189 044. 126	- 11 871. 453	- 46. 487	- 150. 540	1. 175	0. 002		
25'	188 972. 890	- 11 874. 145	- 46. 490	- 150. 485	1. 178	0. 002	0.1	1
26'	188 901. 637	- 11 876. 837	- 46. 493	- 150. 430	1. 181	0. 002	0.2	1
27'	188 830. 368	- 11 879. 527	- 46. 497	- 150. 375	1 184	0. 002	0.3	2
28'	188 759. 082	- 11 882. 217	- 46. 500	- 150. 319	1. 187	0. 002	0.4	2
29'	188 687. 781	- 11 884. 905	- 46. 503	- 150. 264	1. 190	0. 002	0.5	2
30'	188 616. 463	- 11 887. 593	- 46. 506.	- 150. 209	1. 192	0. 002	0.6	2
31'	188 545. 130	- 11 890. 279	- 46. 509	- 150. 154	1. 195	0. 002	0.7	2
32'	188 473. 780	- 11 892. 965	- 46. 513	- 150. 098	1. 198	0. 002	0.8	1
33'	188 402. 414	- 11 895. 649	- 46. 516	- 150. 043	1. 201	0. 002	0.9	1
34'	188 331. 032	- 11 898. 332	- 46. 519	- 149. 988	1. 204	0. 002	1.0	
35'	188 259. 634	- 11 901. 015	- 46. 522	- 149. 932	1. 207	0. 003		
36'	188 188. 220	- 11 903. 696	- 46. 525	- 149. 877	1. 210	0. 003		
37'	188 116. 790	- 11 906. 377	- 46. 528	- 149 822	1. 213	0. 003		
38'	188 045. 344	- 11 909. 056	- 46. 531	- 149. 766	1. 216	0. 003		
39'	187 973. 881	- 11 911. 735	- 46. 534	- 149. 711	1. 219	0 003		
40'	187 902. 403	- 11 914. 412	- 46. 537	- 149. 655	1. 222	0. 003		
41'	187 830. 908	- 11 917. 089	- 46. 540	- 149. 600	1 224	0. 003		
42'	187 759. 398	- 11 919. 764	- 46. 543	- 149 545	1. 227	0. 003		
43'	187 687. 871	- 11 922. 439	- 46. 546	- 149. 489	1. 230	0. 003		
44'	187 616. 328	- 11 925. 112	- 46. 548	- 149. 434	1. 233	0. 003		
45'	187 544. 770	- 11 927. 785	- 46. 551	- 149. 378	1. 236	0. 003		
46'	187 473. 195	- 11 930. 456	- 46. 554	- 149. 323	1. 239	0. 003		
47'	187 401. 604	- 11 933. 127	- 46. 557	- 149 267	1. 242	0. 003		
48'	187 329. 997	- 11 935. 798	- 46. 560	- 149 212	1. 245	0. 003		
49'	187 258. 375	- 11 938 465	- 46. 562	- 149. 156	1. 248	0. 004		
50'	187 186. 736	- 11 941. 132	- 46. 565	- 149. 101	1. 251	0. 004		
51'	187 115. 081	- 11 943. 799	- 46. 568	- 149. 045	1. 254	0. 004		
52'	187 043. 410	- 11 946. 464	- 46. 571	- 148. 990	1. 257	0. 004		
53'	186 971. 723	- 11 949. 129	- 46. 573	- 148. 934	1. 259	0. 004		
54'	186 900. 021	- 11 951. 792	- 46. 576	- 148. 878	1. 262	0. 004		
55'	186 828. 302	- 11 954. 455	- 46. 578	- 148. 823	1. 265	0. 004		
56'	186 756. 567	- 11 957. 116	- 46. 581	- 148 767	1. 268	0. 004		
57'	186 684. 816	- 11 959. 777	- 46. 584	- 148. 712	1. 271	0. 004		
58'	186 613. 050	- 11 962 436	- 46. 586	- 148. 656	1. 274	0. 004		
59'	186 541. 267	- 11 965. 095	- 46. 589	- 148. 600	1. 277	0. 004		
60'	186 469. 469	- 11 967. 752	- 46. 591	- 148. 544.	1. 280	0. 004		

A. K.

II Iloczyn długości linji geodezyjnej przez cosinus azymutu X

$x_m = (\Delta\varphi)\,\Delta\varphi + (\Delta\lambda^2)\,\Delta\lambda^2 + (\Delta\varphi^3)\,\Delta\varphi^3 + \ldots$ gdzie. $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.

φ. 53°	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^3\Delta\lambda^2)$	$(\Delta\lambda^4)$
0'	309 092. 953	3609. 950	72. 415	187. 728	- 0. 636	- 5. 533	- 0. 203
1'	309 093. 822	3608. 351	72. 404	- 187. 864	- 0. 637	- 5. 532	- 0. 204
2'	309 094. 691	3608. 750	72. 392	- 188. 001	- 0. 638	- 5. 531	- 0. 204
3'	309 095. 559	3608. 148	72. 380	- 188. 137	- 0. 640	- 5. 530	- 0. 205
4'	309 096. 428	3607. 545	72. 368	- 188 273	- 0. 641	- 5. 530	- 0. 205
5'	309 097. 296	3606 941	72. 356	- 188. 409	- 0. 642	- 5. 529	- 0. 205
6'	309 098. 164	3606. 335	72. 344	- 188. 545	- 0. 644	- 5. 528	- 0. 206
7'	309 099 032	3605. 729	72. 332	- 188. 681	- 0. 645	- 5. 527	- 0. 206
8'	309 099. 900	3605. 121	72 321	- 188. 817	- 0. 647	- 5. 526	- 0. 206
9'	309 100. 768	3604. 511	72. 309	- 188. 952	- 0. 648	- 5. 525	- 0. 207
10'	309 101. 636	3603 901	72. 297	- 189. 088	- 0. 649	- 5. 524	- 0. 207
11'	309 102. 503	3603. 289	72. 285	- 189. 224	- 0. 651	- 5. 523	- 0. 207
12'	309 103. 371	3602. 676	72. 273	- 189. 360	- 0. 652	- 5. 522	- 0. 208
13'	309 104. 238	3602 062	72. 261	- 189. 496	- 0 653	- 5. 521	- 0. 208
14'	309 105. 105	3601. 447	72. 248	- 189. 632	- 0. 655	- 5. 520	- 0. 209
15'	309 105. 972	3600. 830	72. 236	- 189. 768	- 0. 656	- 5. 520	- 0. 209
16'	309 106. 839	3600 213	72. 224	- 189. 903	- 0. 658	- 5. 519	- 0. 209
17'	309 107. 705	3599. 594	72. 212	- 190. 039	- 0. 659	- 5. 518	- 0. 210
18'	309 108 572	3598. 973	72. 200	- 190. 175	- 0. 660	- 5. 517	- 0. 210
19'	309 109. 438	3598. 352	72 188	- 190. 311	- 0. 662	- 5. 516	- 0. 210
20'	309 110 304	3597. 729	72. 175	- 190. 446	- 0. 663	- 5. 515	- 0. 211
21'	309 111. 170	3597. 105	72. 163	- 190. 582	- 0. 664	- 5. 514	- 0. 211
22'	309 112. 036	3596 480	72. 151	- 190. 717	- 0. 666	- 5. 513	- 0. 211
23'	309 112. 902	3595 854	72. 139	- 190. 853	- 0. 667	- 5. 512	- 0. 212
24'	309 113. 767	3595. 226	72. 126	- 190. 989	- 0. 668	- 5. 511	- 0. 212
25'	309 114. 633	3594. 598	72. 114	- 191. 124	- 0. 670	- 5. 510	- 0. 212
26'	309 115 498	3593. 968	72. 102	- 191. 260	- 0. 671	- 5. 509	- 0. 213
27'	309 116. 363	3593. 336	72. 089	- 191. 395	- 0. 673	- 5. 508	- 0. 213
28'	309 117. 228	3592. 704	72. 077	- 191. 531	- 0. 674	- 5. 507	- 0. 214
29'	309 118. 093	3592. 070	72. 064	- 191 666	- 0. 675	- 5. 507	- 0. 214
30'	309 118. 958	3591. 436	72. 052	- 191. 802	- 0. 677	- 5. 506	- 0. 214
31'	309 119. 822	3590. 800	72. 039	- 191. 937	- 0. 678	- 5. 505	- 0. 215
32'	309 120 687	3590 162	72. 027	- 192. 073	- 0. 679	- 5. 504	- 0. 215
33'	309 121. 551	3589. 524	72. 014	- 192. 208	- 0. 681	- 5. 503	- 0. 215
34'	309 122. 415	3588. 884	72. 002	- 192. 343	- 0. 682	- 5. 502	- 0. 216
35'	309 123. 279	3588. 243	71 989	- 192. 479	- 0. 684	- 5. 501	- 0. 216
36'	309 124. 143	3587. 601	71 977	- 192. 614	- 0. 685	- 5. 500	- 0. 216
37'	309 125. 006	3586. 958	71. 964	- 192. 749	- 0. 686	- 5. 499	- 0. 217
38'	309 125. 870	3586. 313	71 951	- 192. 884	- 0. 688	- 5. 498	- 0 217
39	309 126. 733	3585. 667	71. 939	- 193. 020	- 0. 690	- 5. 497	- 0. 217
40'	309 127. 596	3585 020	71. 926	- 193. 155	- 0. 690	- 5. 496	- 0. 218
41'	309 128. 459	3584. 372	71. 913	- 193. 290	- 0. 692	- 5. 495	- 0. 218
42'	309 129. 322	3583. 723	71. 900	- 193. 425	- 0. 693	- 5 494	- 0. 218
43'	309 130 185	3583. 072	71. 888	- 193. 560	- 0. 694	- 5. 493	- 0. 219
44'	309 131. 048	3582. 420	71. 875	- 193. 696	- 0. 696	- 5. 492	- 0. 219
45'	309 131. 910	3581. 767	71. 862	- 193. 831	- 0. 697	- 5. 491	- 0. 219
46'	309 132. 772	3581. 113	71. 849	- 193. 966	- 0. 699	- 5. 490	- 0. 220
47'	309 133. 634	3580. 457	71. 836	- 194. 101	- 0. 700	- 5. 489	- 0. 220
48'	309 134. 496	3579. 800	71. 823	- 194. 236	- 0. 701	- 5. 488	- 0. 220
49'	309 135. 358	3579 142	71. 810	- 194. 371	- 0. 703	- 5. 487	- 0. 221
50'	309 136. 220	3578. 483	71. 797	- 194. 506	- 0. 704	- 5. 486	- 0. 221
51'	309 137. 081	3577. 823	71. 784	- 194. 641	- 0. 705	- 5. 485	- 0. 222
52'	309 137. 943	3577. 161	71. 771	- 194. 776	- 0. 707	- 5. 484	- 0. 222
53'	309 138. 804	3576. 499	71. 758	- 194. 910	- 0. 708	- 5. 483	- 0. 222
54	309 139. 665	3575. 835	71. 745	- 195. 045	- 0. 709	- 5. 482	- 0. 223
55'	309 140. 526	3575. 169	71. 732	- 195. 180	- 0. 711	- 5. 481	- 0. 223
56'	309 141. 386	3574. 503	71. 719	- 195. 315	- 0. 712	- 5. 480	- 0. 223
57'	309 142. 247	3573. 835	71. 706	- 195. 450	- 0. 714	- 5. 479	- 0. 224
58'	309 143. 107	3573. 166	71. 693	- 195. 585	- 0 715	- 5. 478	- 0. 224
59'	309 143. 968	3572. 496	71. 680	- 195. 719	- 0. 716	- 5. 477	- 0. 224
60'	309 144. 828	3571. 825.	71. 666.	- 195. 854.	- 0. 718	- 5. 476.	- 0. 225.

Iloczyn długości linji geodezyjnej przez SINUS azymutu Y

$Y_m = (\Delta\lambda)\,\Delta\lambda + (\Delta\varphi\Delta\lambda)\,\Delta\varphi\Delta\lambda + (\Delta\lambda^3)\,\Delta\lambda^3 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziątkach tysięcy sek. łuku.

$\varphi = 53°$	$(\Delta\lambda)$	$(\Delta\varphi\Delta\lambda)$	$(\Delta\lambda^3)$	$(\Delta\varphi^2\Delta\lambda)$	$(\Delta\varphi\Delta\lambda^3)$	$\Delta\varphi^3\Delta\lambda$	Poprawka interpolacyjna dla wyrazu $\Delta\lambda$.	
							K'	2.
0'	186 469. 469	- 11 967. 752	- 46. 591	- 148. 544	1. 280	0. 004		
1'	186 397. 654	- 11 970. 408	- 46. 594	- 148. 489	1. 283	0. 004		
2'	186 325. 824	- 11 973. 064	- 46. 596	- 148. 433	1. 286	0. 004		
3'	186 253. 977	- 11 975 719	- 46. 599	- 148. 377	1. 289	0. 005		
4'	186 182. 115	- 11 978. 372	- 46. 601	- 148. 322	1. 292	0. 005		
5	186 110. 237	- 11 981. 025	- 46. 603	- 148. 266	1. 295	0. 005		
6'	186 038. 343	- 11983. 676	- 46. 606	- 148. 210	1. 297	0. 005		
7'	185 966. 434	- 11 986. 327	- 46. 608	- 148. 154	1. 300	0. 005		
8'	185 894. 507	- 11 988. 976	- 46. 610	- 148. 099	1. 303	0. 005		
9'	185 822. 565	- 11 991. 624	- 46. 613	- 148. 043	1. 306	0. 005		
10'	185 750. 607	- 11 994. 272	- 46. 615	- 147. 987	1. 309	0. 005		
11'	185 678. 634	- 11 996. 918	- 46 617	- 147. 931	1. 312	0. 005		
12'	185 606. 644	- 11 999 564	- 46 619	- 147. 875	1. 315	0. 005		
13'	185 534. 639	- 12002. 208	- 46. 622	- 147. 819	1 318	0 005		
14'	185 462. 618	- 12004. 852	- 46. 624	- 147. 763	1. 321	0. 005		
15'	185 390. 581	- 12007. 494	- 46. 626	- 147. 708	1. 324	0. 005		
16'	185 318. 528	- 12010. 135	- 46 628	- 147. 652	1. 327	0 005		
17'	185 246. 459	- 12012. 776	- 46. 630	- 147. 596	1 330	0. 005		
18'	185 174. 375	- 12015. 415	- 46. 632	- 147. 540	1. 333	0. 006		
19'	185 102. 274	- 12018. 053	- 46. 634	- 147. 484	1. 336	0. 006		
20'	185 030. 158	- 12020. 691	- 46 636	- 147. 428	1. 339	0. 006		
21'	184 958. 026	- 12023. 327	- 46. 638	- 147. 372	1. 341	0. 006		+ 1000
22'	184 885. 878	- 12025. 963	- 46. 640	- 147. 316	1. 344	0. 006		
23'	184 813. 714	- 12028. 597	- 46. 642	- 147. 260	1. 347	0. 006		
24'	184 741. 535	- 12031. 230	- 46. 644	- 147. 204	1. 350	0 006		
25'	184 669. 340	- 12033. 862	- 46. 646	- 147. 148	1. 353	0. 006	0.1	1
26	184 597. 129	- 12036. 494	- 46. 648	- 147. 092	1 356	0. 006	0.2	1
27'	184 524. 902	- 12039 124	- 46. 650	- 147. 036	1. 359	0. 006	0.3	2
28'	184 452 659	- 12041. 753	- 46. 652	- 146. 980	1. 362	0 006	0.4	2
29'	184 380. 401	- 12044. 382	- 46 653	- 146. 924	1. 365	0. 006	0.5	2
30'	184 308. 127	- 12047. 009	- 46. 655.	- 146. 868	1. 368	0. 006	0.6	2
31'	184 235. 837	- 12049. 635	- 46. 657	- 146. 811	1. 371	0. 006	0.7	2
32'	184 163. 531	- 12052. 260	- 46 659	- 146. 755	1. 374	0. 007	0.8	1
33'	184 091. 210	- 12054. 885	- 46. 660	- 146. 699	1. 377	0. 007	0.9	1
34'	184 018. 872	- 12057. 508	- 46. 662	- 146. 643	1. 380	0. 007	1.0	
35'	183 946. 520	- 12060. 130	- 46 664	- 146. 587	1 383	0. 007		
36'	183 874. 151	- 12062. 751	- 46. 665	- 146. 531	1. 386	0. 007		
37'	183 801. 766	- 12065. 371	- 46. 667	- 146. 474	1. 389	0. 007		
38'	183 729. 366	- 12067. 991	- 46 669	- 146. 418	1. 392	0. 007		
39'	183 656. 951	- 12070. 609	- 46. 670	- 146. 362	1. 394	0. 007		
40'	183 584 519	- 12073. 226	- 46. 672	- 146. 306	1. 397	0. 007		
41'	183 512. 072	- 12075. 842	- 46 673	- 146. 249	1. 400	0. 007		
42	183 439. 609	- 12078. 457	- 46. 675	- 146 193	1. 403	0. 007		
43'	183 367. 130	- 12081. 071	- 46. 676	- 146. 137	1. 406	0. 007		
44'	183 294. 636	- 12083. 684	- 46. 678	- 146. 081	1. 409	0. 007		
45'	183 222. 126	- 12086. 296	- 46. 679	- 146. 024	1. 412	0. 008		
46'	183 149 601	- 12088. 908	- 46. 681	- 145. 968	1 415	0. 008		
47'	183 077. 059	- 12091. 518	- 46. 682	- 145. 912	1. 418	0. 008		
48'	183 004. 502	- 12094. 127	- 46. 684	- 145. 855	1. 421	0. 008		
49'	182 931. 930	- 12096 735	- 46. 685	- 145. 799	1. 424	0. 008		
50'	182 859. 342	- 12099. 342	- 46. 686	- 145. 742	1. 427	0. 008		
51'	182 786. 738	- 12101. 948	- 46. 688	- 145. 686	1. 430	0. 008		
52'	182 714. 118	- 12104. 553	- 46. 689	- 145 630	1. 433	0. 008		
53'	182 641. 483	- 12107. 157	- 46. 690	- 145. 573	1. 436	0. 008		
54'	182 568. 832	- 12109. 760	- 46. 691	- 145. 517	1. 439	0. 008		
55'	182 496. 166	- 12112. 362	- 46. 693	- 145 460	1. 442	0. 008		
56'	182. 423. 484	- 12114. 962	- 46. 694	- 145. 404	1. 445	0. 008		
57'	182 350. 786	- 12117. 562	- 46. 695	- 145. 347	1. 448	0. 008		
58	182 278 073	- 12120. 161	- 46. 696	- 145. 291	1. 450	0. 008		
59'	182 205. 344	- 12122. 759	- 46. 697	- 145. 234	1. 453	0. 009		
60'	182 132. 600.	- 12125. 356.	- 46. 698	- 145. 178	1. 456.	0. 009		

A.K.

II Iloczyn długości linji geodezyjnej przez COSINUS azymutu X

$x_m = (\Delta\varphi)\,\Delta\varphi\cdot(\Delta\lambda^2)\,\Delta\lambda^2\cdot(\Delta\varphi^3)\,\Delta\varphi^3 = \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.

φ. 54°	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^2)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta\lambda^2)$	$(\Delta\lambda^4)$
0'	309 144. 828	3571. 825	71. 666	- 195. 854	- 0. 718	- 5. 476	- 0. 225
1'	309 145. 888	3571. 153	71. 653	- 195. 989	- 0. 719	- 5. 475	- 0. 225
2'	309 146. 547	3570. 479	71. 640	- 196. 123	- 0. 720	- 5. 474	- 0. 225
3'	309 147. 407	3569. 804	71. 627	- 196. 258	- 0. 722	- 5. 473	- 0. 226
4'	309 148. 266	3569. 128	71. 613	- 196. 393	- 0. 723	- 5. 472	- 0. 226
5'	309 149. 126	3568. 451	71. 600	- 196. 527	- 0. 724	- 5. 471	- 0. 226
6'	309 149. 985	3567. 772	71. 587	- 196. 662	- 0. 726	- 5. 470	- 0. 227
7'	309 150. 844	3567. 093	71. 573	- 196. 797	- 0. 727	- 5. 469	- 0. 227
8'	309 151. 703	3566. 412	71. 560	- 196. 931	- 0. 728	- 5. 468	- 0. 227
9'	309 152. 561	3565. 729	71. 546	- 197. 066	- 0. 730	- 5. 467	- 0. 228
10'	309 153. 420	3565. 046	71 533	- 197. 200	- 0. 731	- 5. 466	- 0. 228
11'	309 154 278	3564. 362	71. 519	- 197. 334	- 0. 733	- 5. 465	- 0. 228
12'	309 155. 136	3563. 676	71. 506	- 197. 469	- 0. 734	- 5. 464	- 0. 229
13'	309 155. 994	3562. 989	71. 492	- 197. 603	- 0. 735	- 5. 463	- 0. 229
14'	309 156. 852	3562. 301	71. 479	- 197. 738	- 0. 737	- 5. 462	- 0. 229
15'	309 157. 710	3561. 611	71. 465	- 197. 872	- 0. 738	- 5. 461	- 0. 230
16'	309 158. 567	3560. 921	71. 452	- 198. 006	- 0. 739	- 5. 460	- 0. 230
17'	309 159. 425	3560. 229	71. 438	- 198. 141	- 0. 741	- 5. 459	- 0. 230
18'	309 160. 282	3559. 536	71. 424	- 198 275	- 0. 742	- 5. 458	- 0 231
19'	309 161 138	3558. 842	71. 411	- 198. 409	- 0. 743	- 5. 457	- 0. 231
20'	309 161 996	3558. 146	71. 397	- 198 543	- 0. 745	- 5. 456	- 0. 231
21'	309 162. 852	3557. 447	71. 383	- 198. 678	- 0. 746	- 5. 455	- 0. 232
22'	309 163. 709	3556 752	71 370	- 198. 812	- 0. 748	- 5. 454	- 0 232
23'	309 164. 566	3556 053	71. 356	- 198. 946	- 0. 749	- 5. 453	- 0. 232
24'	309 165. 421	3555. 352	71. 342	- 199. 080	- 0. 750	- 5, 452	- 0. 233
25'	309 166. 277	3554. 651	71. 328	- 199. 214	- 0. 752	- 5. 451	- 0. 233
26'	309 167. 133	3553. 948	71. 314	- 199. 348	- 0. 753	- 5. 450	- 0. 233
27'	309 167 989	3553. 244	71. 301	- 199. 482	- 0. 754	- 5. 449	- 0 234
28'	309 168. 844	3552. 539	71. 287	- 199. 616	- 0. 756	- 5. 448	- 0. 234
29'	309 169. 700	3551. 833	71. 273	- 199. 750	- 0. 757	- 5. 447	- 0. 234
30'	309 170. 555	3551. 125	71. 259	- 199. 884	- 0. 758	- 5. 446	- 0. 235
31'	309 171. 410	3550. 417	71. 245	- 200. 018	- 0. 760	- 5. 445	- 0. 235
32'	309 172. 265	3549 707	71. 231	- 200. 152	- 0. 761	- 5. 443	- 0. 235
33'	309 173 120	3548. 996	71. 217	- 200. 286	- 0 762	- 5. 442	- 0. 236
34'	309 173. 974	3548 283	71. 203	- 200. 420	- 0. 764	- 5. 441	- 0. 236
35'	309 174. 828	3547. 570	71. 189	- 200. 554	- 0 765	- 5. 440	- 0. 236
36'	309 175. 683	3546. 855	71. 175	- 200. 687	- 0 766	- 5. 439	- 0. 237
37'	309 176. 537	3546. 139	71 161	- 200. 821	- 0 768	- 5. 438	- 0 237
38'	309 177. 391	3545. 422	71. 146	- 200. 955	- 0. 769	- 5. 437	- 0. 237
39'	309 178 244	3544. 704	71. 132	- 201. 089	- 0. 771	- 5. 436	- 0. 238
40'	309 179. 098	3543 984	71. 118	- 201. 222	- 0. 772	- 5. 435	- 0. 238
41'	309 179. 951	3543. 263	71. 104	- 201. 356	- 0. 773	- 5. 434	- 0. 238
42'	309 180. 804	3542. 542	71. 090	- 201. 490	- 0. 775	- 5. 433	- 0. 239
43'	309 181. 657	3541 818	71. 075	- 201. 623	- 0. 776	- 5. 432	- 0. 239
44'	309 182. 510	3541. 094	71 061	- 201. 757	- 0. 777	- 5. 431	- 0. 239
45'	309 183. 363	3540. 369	71. 047	- 201. 890	- 0. 779	- 5. 430	- 0. 240
46'	309 184. 215	3539. 642	71. 033	- 202. 024	- 0. 780	- 5. 428	- 0. 240
47'	309 185. 067	3538 914	71. 018	- 202. 158	- 0. 781	- 5. 427	- 0. 240
48	309 185. 920	3538. 185	71. 004	- 202. 291	- 0. 783	- 5. 426	- 0. 241
49'	309 186. 772	3537 455	70. 989	- 202. 424	- 0. 784	- 5. 425	- 0. 241
50'	309 187. 623	3536. 723	70. 975	- 202. 558	- 0. 785	- 5. 424	- 0. 241
51	309 188. 475	3535. 990	70. 961	- 202. 691	- 0. 787	- 5. 423	- 0. 242
52'	309 189. 326	3535. 256	70. 946	- 202. 825	- 0. 788	- 5. 422	- 0 242
53'	309 190. 178	3534. 521	70. 932	- 202. 958	- 0. 789	- 5. 421	- 0 242
54'	309 191. 029	3533. 785	70. 917	- 203. 091	- 0. 791	- 5. 420	- 0. 243
55'	309 191. 880	3533. 047	70. 903	- 203. 225	- 0. 792	- 5. 419	- 0. 243
56'	309 192. 730	3532. 309	70. 888	- 203. 358	- 0. 794	- 5. 418	- 0. 243
57'	309 193. 581	3531. 569	70. 873	- 203. 491	- 0. 795	- 5. 416	- 0. 244
58'	309 194. 431	3530. 828	70. 859	- 203. 624	- 0. 796	- 5. 415	- 0. 244
59'	309 195. 282	3530. 085	70. 844	- 203. 758	- 0 798	- 5. 414	- 0. 244
60'	309 196. 132	3529. 342	70 830	- 203. 891	- 0. 799	- 5. 413	- 0. 245

Iloczyn długości linji geodezyjnej przez sinus azymutu Y

$Y_m = (\Delta\lambda)\Delta\lambda + (\Delta\varphi\Delta\lambda)\Delta\varphi\Delta\lambda + (\Delta\lambda^3)\Delta\lambda^2 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.
$\Delta\lambda$ przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek. łuku.

$\varphi = 54°$	$\Delta\lambda$	$\Delta\varphi\Delta\lambda$	$\Delta\lambda^3$	$\Delta\varphi^2\Delta\lambda$	$\Delta\varphi\Delta\lambda^3$	$\Delta\varphi^3\Delta\lambda$	Poprawka interpolacyjna dla wyrazu $\Delta\lambda$	
							K'	g'
0'	182 132. 600	- 12123. 356	- 46. 698	- 145. 178	1. 456	0. 009		
1'	182 089. 840	- 12127. 952	- 46. 699	- 145. 121	1. 459	0. 009		
2'	181 987. 065	- 12130. 547	- 46. 700	- 145. 065	1. 462	0. 009		
3'	181 914. 274	- 12133. 140	- 46. 701	- 145. 008	1. 465	0. 009		
4'	181 841. 467	- 12135. 733	- 46. 702	- 144. 952	1. 468	0. 009		
5'	181 768. 645	- 12138. 325	- 46. 703	- 144. 895	1. 471	0. 009		
6'	181 695. 807	- 12140. 916	- 46. 704	- 144. 838	1. 474	0. 009		
7'	181 622. 954	- 12143. 505	- 46. 705	- 144. 782	1. 477	0. 009		
8'	181 550. 085	- 12146. 094	- 46. 706	- 144. 725	1. 480	0. 009		
9'	181 477. 201	- 12148. 682	- 46. 707	- 144. 669	1. 483	0. 009		
10'	181 404. 301	- 12151. 268	- 46. 708	- 144. 612	1. 486	0. 009		
11'	181 331. 385	- 12153. 854	- 46. 709	- 144. 555	1. 489	0. 009		
12'	181 258. 454	- 12156. 439	- 46. 710	- 144. 499	1. 492	0. 009		
13'	181 185. 508	- 12159. 022	- 46. 710	- 144. 442	1. 495	0. 010		
14'	181 112. 546	- 12161. 605	- 46. 711	- 144. 385	1. 498	0. 010		
15'	181 039. 589	- 12164. 186	- 46. 712	- 144. 328	1. 501	0. 010		
16'	180 966. 576	- 12166. 767	- 46. 713	- 144. 272	1. 504	0. 010		
17'	180 893. 568	- 12169. 346	- 46. 713	- 144. 215	1. 507	0. 010		
18'	180 820. 544	- 12171. 925	- 46 714	- 144. 158	1 510	0. 010		
19'	180 747. 505	- 12174. 502	- 46. 715	- 144. 101	1. 513	0. 010		
20'	180 674. 450	- 12177. 079	- 46. 715	- 144. 045	1. 516	0. 010		
21'	180 601. 380	- 12179. 654	- 46. 716	- 143. 988	1. 519	0. 010		+0.001
22'	180 528. 294	- 12182. 229	- 46. 716	- 143. 931	1. 522	0. 010		
23'	180 455. 193	- 12184. 802	- 46. 717	- 143. 874	1 525	0. 010		
24'	180 382. 076	- 12187. 374	- 46. 718	- 143 817	1. 527	0. 010		
25'	180 308. 944	- 12189. 946	- 46. 718	- 143 760	1. 530	0. 010	0.1	1
26'	180 235 797	- 12192. 516	- 46. 719	- 143. 703	1. 533	0. 011	0.2	1
27'	180 162. 634	- 12195. 085	- 46. 719	- 143. 647	1. 536	0. 011	0.3	2
28'	180 089. 456	- 12197. 653	- 46 719	- 143. 590	1. 539	0. 011	0.4	2
29'	180 016. 262	- 12200. 221	- 46. 720	- 143. 533	1. 542	0. 011	0.5	2
30'	179 943. 053	- 12202. 787	- 46. 720	- 143. 476	1. 545	0. 011	0.6	2
31'	179 869. 829	- 12205. 352	- 46 721	- 143. 419	1. 548	0. 011	0.7	2
32'	179 796. 589	- 12207. 916	- 46. 721	- 143. 362	1. 551	0. 011	0.8	1
33'	179 723. 334	- 12210. 479	- 46. 721	- 143. 305	1 554	0. 011	0.9	1
34'	179 650. 063	- 12213. 041	- 46. 722	- 143. 248	1. 557	0. 011	1.0	
35'	179 576. 778	- 12215. 602	- 46. 722	- 143 191	1. 560	0. 011		
36'	179 503. 476	- 12218. 162	- 46. 722	- 143. 134	1. 563	0. 011		
37'	179 430. 160	- 12220. 722	- 46. 722	- 143. 077	1. 566	0. 011		
38'	179. 356. 828	- 12223. 280	- 46 723	- 143. 020	1 569	0 011		
39'	179. 283. 480	- 12225 836	- 46. 723	- 142. 963	1. 572	0. 012		
40'	179 210. 118	- 12228. 392	- 46. 723	- 142. 906	1. 575	0. 012		
41'	179 136. 740	- 12230. 947	- 46. 723	- 142 849	1 578	0. 012		
42'	179 063. 346	- 12233. 501	- 46. 723	- 142. 792	1. 581	0. 012		
43'	178 989 938	- 12236. 054	- 46 723	- 142. 734	1. 584	0 012		
44'	178 916. 514	- 12238 606	- 46. 723	- 142. 677	1. 587	0. 012		
45'	178 843. 074	- 12241. 157	- 46. 723	- 142 620	1. 590	0. 012		
46'	178 769. 620	- 12243. 708	- 46. 723	- 142. 563	1. 593	0. 012		
47'	178 696 150	- 12246. 255	- 46. 723	- 142. 506	1 596	0. 012		
48'	178 622. 665	- 12248. 803	- 46. 723	- 142. 449	1. 599	0. 012		
49'	178 549. 164	- 12251. 350	- 46. 723	- 142. 391	1. 602	0 012		
50'	178 475 648	- 12253. 895	- 46. 723	- 142. 334	1. 605	0. 012		
51'	178 402. 117	- 12256. 440	- 46. 723	- 142 277	1 608	0 012		
52'	178 328. 571	- 12258. 983	- 46. 723	- 142. 220	1. 611	0. 012		
53'	178 255. 010	- 12261. 526	- 46. 723	- 142. 163	1 614	0. 013		
54'	178 181. 433	- 12264. 068	- 46. 723	- 142. 105	1. 617	0. 013		
55'	178 107. 841	- 12266. 608	- 46. 722	- 142. 048	1 620	0. 013		
56'	178 034. 234	- 12269. 147	- 46. 722	- 141. 991	1. 623	0. 013		
57'	177 960 611	- 12271. 686	- 46. 722	- 141. 933	1 626	0. 013		
58'	177 886. 973	- 12274. 223	- 46. 722	- 141 876	1 629	0. 013		
59'	177 813. 320	- 12276. 760	- 46. 721	- 141. 819	1 632	0 013		
60'	177 739. 652	- 12279 295	- 46. 721	- 141. 761	1 635	0. 013		

A.K.

Iloczyn długości linji geodezyjnej przez COSINUS azymutu X

$x_m = (\Delta\varphi)\,\Delta\varphi + (\Delta\lambda^2)\,\Delta\lambda^2 + (\Delta\varphi^2)\,\Delta\varphi^2 \ldots\ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek. łuku
$\Delta\lambda$ przyrost długości geogr wyrażony w dziesiątkach tysięcy sek. łuku.

$\varphi = 55^\circ$	$(\Delta\varphi)$	$(\Delta\lambda^2)$	$(\Delta\varphi^2)$	$(\Delta\varphi\Delta\lambda^2)$	$(\Delta\varphi^3)$	$(\Delta\varphi^2\Delta\lambda^2)$	$(\Delta\lambda^4)$
0'	309 196. 132	3529. 342	70. 630	- 203. 891	- 0. 799	- 5. 413	- 0. 245
1'	309 196. 981	3528. 597	70. 815	- 204. 024	- 0. 800	- 5. 412	- 0. 245
2'	309 197. 831	3527. 851	70. 800	- 204. 157	- 0. 802	- 5. 411	- 0. 245
3'	309 198. 681	3527. 104	70. 785	- 204. 290	- 0. 803	- 5. 410	- 0. 246
4'	309 199. 530	3526. 356	70. 771	- 204. 423	- 0. 804	- 5. 409	- 0. 246
5'	309 200. 379	3525. 606	70 756	- 204. 556	- 0. 806	- 5. 408	- 0. 246
6'	309 201. 228	3524. 856	70. 741	- 204. 689	- 0. 807	- 5. 406	- 0. 247
7'	309 202 077	3524. 104	70. 726	- 204 822	- 0. 808	- 5. 405	- 0. 247
8'	309 202. 926	3523. 351	70. 711	- 204. 955	- 0. 810	- 5. 404	- 0 247
9'	309 203. 774	3522. 597	70. 697	- 205. 088	- 0. 811	- 5. 403	- 0. 247
10'	309 204. 622	3521. 841	70. 682	- 205. 221	- 0. 812	- 5. 402	- 0. 248
11'	309 205. 470	3521. 084	70. 667	- 205. 354	- 0. 814	- 5. 401	- 0. 248
12'	309 206. 318	3520. 327	70. 652	- 205. 486	- 0. 815	- 5. 400	- 0. 248
13'	309 207. 166	3519. 568	70. 637	- 205. 619	- 0. 816	- 5. 398	- 0. 249
14'	309 208. 014	3518. 807	70. 622	- 205. 752	- 0. 818	- 5. 397	- 0. 249
15	309 208. 861	3518. 046	70. 607	- 205. 885	- 0. 819	- 5. 396	- 0. 249
16'	309 209. 708	3517. 283	70. 592	- 206. 017	- 0. 820	- 5. 395	- 0. 250
17'	309 210. 555	3516. 519	70. 577	- 206. 150	- 0. 822	- 5. 394	- 0. 250
18'	309 211. 402	3515. 754	70. 562	- 206. 283	- 0. 823	- 5. 393	- 0. 250
19'	309 212 249	3514. 988	70. 547	- 206. 415	- 0. 824	- 5. 392	- 0. 251
20'	309 213. 095	3514. 221	70. 531	- 206. 548	- 0. 826	- 5. 390	- 0. 251
21'	309 213. 941	3513. 452	70. 516	- 206. 681	- 0. 827	- 5. 389	- 0. 251
22'	309 214. 787	3512. 683	70. 501	- 206. 813	- 0. 828	- 5. 388	- 0. 252
23'	309 215. 633	3511. 912	70. 486	- 206. 945	- 0. 830	- 5. 387	- 0. 252
24'	309 216. 479	3511. 139	70 471	- 207. 078	- 0. 831	- 5. 386	- 0. 252
25'	309 217 325	3510. 366	70. 455	- 207. 211	- 0 832	- 5. 385	- 0. 253
26'	309 218. 170	3509. 592	70. 440	- 207. 343	- 0. 834	- 5. 384	- 0. 253
27'	309 219. 015	3508. 816	70. 425	- 207. 475	- 0. 835	- 5. 382	- 0. 253
28'	309 219. 860	3508. 039	70. 409	- 207. 608	- 0. 837	- 5. 381	- 0. 254
29'	309 220. 705	3507. 261	70. 394	- 207. 740	- 0. 838	- 5. 380	- 0. 254
30'	309 221 550	3506. 482	70 379	- 207 872	- 0. 839	- 5. 379	- 0. 254
31'	309 222. 394	3505. 701	70. 363	- 208. 005	- 0. 841	- 5. 378	- 0. 255
32'	309 223. 238	3504. 919	70. 348	- 208. 137	- 0. 842	- 5. 377	- 0. 255
33'	309 224. 083	3504. 137	70. 332	- 208. 269	- 0. 843	- 5. 375	- 0. 255
34'	309 224. 926	3503. 352	70. 317	- 208. 401	- 0. 845	- 5. 374	- 0. 255
35'	309 225. 770	3502. 567	70. 301	- 208. 534	- 0. 846	- 5. 373	- 0. 256
36'	309 226. 614	3501 781	70. 286	- 208. 666	- 0. 847	- 5. 372	- 0. 256
37'	309 227. 457	3500. 993	70. 270	- 208. 798	- 0. 849	- 5. 371	- 0. 256
38	309 228. 300	3500. 204	70 255	- 208. 930	- 0. 850	- 5. 369	- 0. 257
39'	309 229. 143	3499 414	70. 239	- 209. 062	- 0. 851	- 5. 368	- 0. 257
40'	309 229. 986	3498. 623	70 224	- 209 194	- 0. 853	- 5. 367	- 0. 257
41'	309 230. 829	3497. 831	70. 208	- 209. 326	- 0. 854	- 5. 366	- 0. 258
42'	309 231. 671	3497. 037	70 192	- 209. 458	- 0 855	- 5. 365	- 0. 258
43'	309 232. 513	3496. 243	70 177	- 209. 590	- 0. 857	- 5. 364	- 0. 258
44'	309 233. 355	3495. 447	70. 161	- 209. 722	- 0. 858	- 5. 362	- 0. 259
45'	309 234. 197	3494. 650	70. 145	- 209. 854	- 0. 859	- 5. 361	- 0. 259
46'	309 235. 039	3493. 851	70. 129	- 209. 985	- 0. 861	- 5. 360	- 0. 259
47'	309 235. 880	3493. 052	70. 114	- 210. 117	- 0. 862	- 5. 359	- 0. 259
48'	309 236. 721	3492. 251	70 098	- 210. 249	- 0. 863	- 5. 358	- 0. 260
49'	309 237. 562	3491. 449	70. 082	- 210. 381	- 0. 865	- 5. 356	- 0. 260
60'	309 238. 403	3490. 646	70. 066	- 210. 512	- 0. 866	- 5. 355	- 0. 260
51'	309 239. 244	3489. 842	70. 050	- 210. 644	- 0. 867	- 5. 354	- 0. 261
52	309 240 085	3489. 037	70. 034	- 210. 776	- 0. 869	- 5. 353	- 0. 261
53'	309 240. 925	3488. 230	70. 018	- 210. 907	- 0. 870	- 5. 351	- 0. 261
54'	309 241. 765	3487 422	70. 002	- 211. 039	- 0. 871	- 5. 350	- 0. 262
55'	309 242. 605	3486. 613	69. 986	- 211. 171	- 0. 873	- 5. 349	- 0. 262
56	309 243. 445	3485. 803	69 970	- 211. 302	- 0. 874	- 5. 348	- 0. 262
57'	309 244 284	3484. 992	69. 954	- 211. 434	- 0. 875	- 5. 347	- 0. 263
58'	309 245. 123	3484. 180	69 938	- 211. 565	- 0. 877	- 5. 345	- 0. 263
59'	309 245. 963	3483. 366	69. 922	- 211. 697	- 0. 878	- 5 344	- 0. 263
60'	309 246. 802	3482 551	69. 906	- 211. 828.	- 0. 879.	- 5. 343	- 0. 264.

Iloczyn długości linji geodezyjnej przez sinus azymutu Y

$y_m = (\Delta l)\,\Delta l + (\Delta\varphi\Delta l)\,\Delta\varphi\Delta l + (\Delta l^3)\,\Delta l^3 + \ldots$ gdzie $\Delta\varphi$ przyrost szerokości geogr. wyrażony w dziesiątkach tysięcy sek łuku
Δl przyrost długości geogr. wyrażony w dziesiątkach tysięcy sek łuku

$\varphi = 55°$	(Δl)	$(\Delta\varphi\Delta l)$	(Δl^3)	$(\Delta\varphi^2\Delta l)$	$(\Delta\varphi\Delta l^3)$	$(\Delta\varphi^3\Delta l)$	Poprawka interpolacyjna dla wyrazu Δl.	
							K.	2.
0'	177 739. 652	- 12 279. 295	- 46. 721	- 141 761	1. 635	0. 013		
1'	177 665. 969	- 12 281. 829	- 46. 721	- 141 704	1. 638	0. 013		
2'	177 592 270	- 12 284 363	- 46. 720	- 141. 647	1. 641	0. 013		
3'	177 518. 557	- 12 286. 895	- 46. 720	- 141. 589	1. 644	0 013		
4'	177 444. 828	- 12 289. 426	- 46 720	- 141. 532	1. 647	0. 013		
5'	177 371. 083	- 12 291. 956	- 46. 719	- 141. 474	1. 650	0. 014		
6'	177 297 324	- 12 294. 485	- 46. 719	- 141. 417	1. 653	0 014		
7'	177 223. 550	- 12 297. 013	- 46 718	- 141. 360	1. 656	0 014		
8'	177 149. 760	- 12 299. 540	- 46. 718	- 141. 302	1 659	0. 014		
9'	177 075. 955	- 12 302. 067	- 46. 717	- 141. 245	1. 662	0. 014		
10'	177 002 135	- 12 304. 592	- 46. 716	- 141 187	1 665	0 014		
11'	176. 928. 300	- 12 307. 115	- 46. 716	- 141. 130	1. 668	0 014		
12'	176 854. 450	- 12 309. 638	- 46. 715	- 141. 072	1. 671	0. 014		
13'	176 780 584	- 12 312. 160	- 46. 715	- 141. 015	1 674	0. 014		
14'	176 706. 704	- 12 314. 681	- 46. 714	- 140. 957	1. 677	0. 014		
15'	176 632. 808	- 12 317. 201	- 46. 713	- 140. 900	1. 680	0. 014		
16'	176 558 898	- 12 319. 720	- 46. 713	- 140. 842	1. 683	0. 014		
17'	176 484. 972	- 12 322. 238	- 46 712	- 140. 784	1. 686	0. 014		
18'	176 441. 031	- 12 324. 754	- 46. 711	- 140. 727	1. 688	0. 014		
19'	176 337. 075	- 12 327. 270	- 46. 710	- 140. 669	1. 691	0. 015		
20'	176 263. 103	- 12 329. 785	- 46. 710	- 140 612	1. 694	0. 015		
21'	176 189. 117	- 12 332 298	- 46 709	- 140. 554	1. 697	0. 015		+0001
22'	176 115. 116	- 12 334. 811	- 46 708	- 140 496	1. 700	0. 015		
23'	176 041. 099	- 12 337. 322	- 46. 707	- 140. 439	1. 703	0. 015		
24'	175 967. 068	- 12 339. 833	- 46 706	- 140. 381	1. 706	0 015		
25'	175 893. 021	- 12 342. 342	- 46 705	- 140. 323	1. 709	0. 015	0 1	1
26'	175 818. 960	- 12 344. 851	- 46. 704	- 140. 266	1. 712	0. 015	0. 2	1
27'	175 744. 883	- 12 347. 358	- 46 703	- 140. 208	1. 715	0. 015	0. 3	2
28'	175 670. 791	- 12 349. 865	- 46. 702	- 140 150	1. 718	0. 015	0. 4	2
29'	175 596 685	- 12 352. 370	- 46. 701	- 140. 093	1 721	0 015	0. 5	2
30'	175 522. 563	- 12 354. 874	- 46 700	- 140. 035	1 724	0. 015	0. 6	2
31'	175 448. 426	- 12 357. 377	- 46. 699	- 139 977	1 727	0. 015	0. 7	2
32'	175 374. 274	- 12 359 880	- 46. 698	- 139. 919	1. 730	0. 016	0. 8	1
33'	175 300. 108	- 12 362. 381	- 46. 697	- 139. 861	1 733	0 016	0. 9	1
34'	175 225. 926	- 12 364. 881	- 46 695	- 139. 804	1. 736	0 016	1. 0	
35'	175 151 729	- 12 367. 380	- 46. 694	- 139. 746	1. 739	0 016		
36'	175 077 517	- 12 369 878	- 46. 693	- 139. 688	1 742	0. 016		
37'	175 003. 291	- 12 372. 375	- 46 692	- 139. 630	1. 745	0. 016		
38'	174 929. 049	- 12 374. 871	- 46. 691	- 139 572	1. 748	0 016		
39'	174 854. 792	- 12 377. 366	- 46. 690	- 139. 514	1 751	0. 016		
40'	174 780 520	- 12 379. 860	- 46 689	- 139. 457	1. 754	0 016		
41'	174 706. 234	- 12 382 353	- 46. 688	- 139. 399	1. 757	0. 016		
42'	174 631 932	- 12 384. 844	- 46. 687	- 139. 341	1. 760	0. 016		
43	174 557. 616	- 12 387. 335	- 46. 685	- 139. 283	1. 763	0. 016		
44'	174 483 284	- 12 389. 825	- 46. 683	- 139. 225	1. 766	0. 016		
45'	174 408. 938	- 12 392. 313	- 46. 682	- 139. 167	1. 769	0. 016		
46'	174 334. 576	- 12 394. 801	- 46. 680	- 139. 109	1 772	0 017		
47'	174 260. 200	- 12 397. 288	- 46. 679	- 139. 051	1. 775	0. 017		
48'	174 185. 809	- 12 399. 773	- 46. 677	- 138. 993	1. 778	0. 017		
49'	174 111. 403	- 12 402. 258	- 46 676	- 138. 935	1. 781	0. 017		
50'	174 036 982	- 12 404. 741	- 46 674	- 138 877	1. 784	0. 017		
51'	173 962. 546	- 12 407. 224	- 46 673	- 138. 819	1. 787	0 017		
52	173 888. 095	- 12 409. 705	- 46. 671	- 138. 761	1. 790	0. 017		
53	173 813 630	- 12 412. 185	- 46. 670	- 138. 703	1. 793	0. 017		
54'	173 739. 149	- 12 414. 664	- 46. 668	- 138. 645	1. 796	0 017		
55	173 664. 654	- 12 417. 143	- 46. 666	- 138. 587	1 799	0 017		
56'	173 590 143	- 12 419. 620	- 46 665	- 138. 529	1. 802	0. 017		
57'	173 5 5 618	- 12 422. 096	- 46. 663	- 138. 470	1. 805	0. 017		
58'	173 441. 078	- 12 424. 571	- 46. 661	- 138. 412	1. 808	0 017		
59'	173 366 523	- 12 427. 045	- 46 660	- 138. 354	1. 811	0. 018		
60'	173 291. 954.	- 12 429. 518.	- 46. 658	- 138. 296	1. 814	0. 018		

A. K.